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Renesas Electronics Corporation

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HOW TO USE ZERO VOLTAGE SWITCHING

" μ PC1701C"

1. INTRODUCTION

Zero Voltage Switch " μ PC1701C" is a bipolar analog integrated circuit to provide zero voltage switching control of resistance loads when used with triacs.

Zero Voltage Switching is a method of switching ON and OFF only at the zero crossing points of the sinusoidal, 50 or 60 Hz waveform.

This largely eliminates the radio frequency interference (RFI) problem.

The μ PC1701C is suitable for mains-on-line operation and requires minimal external components, therefore allow simplification of circuitry and improvement in performance of control circuit.

The device is particularly suited for use in such applications as electric heating, range oven controls, hair dryers, oven in general, and industrial temperature control equipments.

Here we present a outline of zero voltage switching designs using Zero Voltage Switch (ZVS) " μ PC1701C".

2. THE NECESSITY OF ZVS

AC power controller using triac is generally constructed as shown in Fig. 1. There are two ways which control AC power. One of the way is phase control shown in Fig. 2 (a) which is controlled by varying phase angle.

The other one is zero voltage switching shown in Fig. 2 (b) which is controlled by varying ON-OFF frequency with triggering triac at zero voltage point.

Phase control is possible to vary AC power continuously 0~100 % in half cycle of AC power supply, therefore, precision and response are well.

This is using in such applications as light dimmer, motor speed control and electric heating control.

However, abrupt current produces electromagnetic interference (EMI), when the triac turn on, and cause high frequency interference at specially radio frequency band.

Phase control will require adequate filtering in order to hold EMI within acceptable limits.

Such filters can become rather large and expensive and since it is anticipated that the allowed limits on EMI will decrease.

On the contrary, Zero Voltage switching, load current varies gradually following AC supply voltage waveforms, therefore it is possible to control AC power without RFI.

However this is not suitable for use in light dimmer, because this is ON-OFF control.

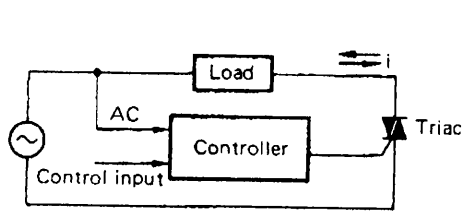


Fig. 1 AC Power Controller by Triac

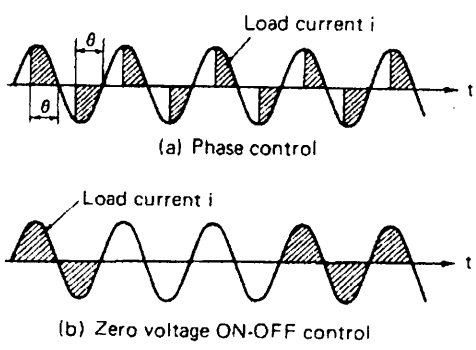


Fig. 2 Phase Control and Zero Voltage ON-OFF Control

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3. OUTLINE OF ZVS "μPC1701C"

Fig. 3 shows a block diagram of μPC1701C, Fig. 4 shows a pin connections and the equivalent circuit is shown in Fig. 5. The features are as follows:

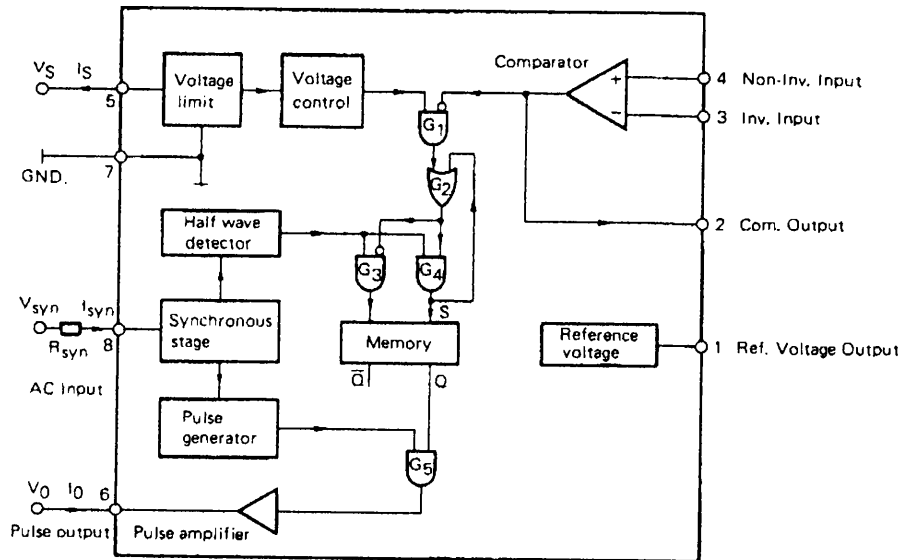
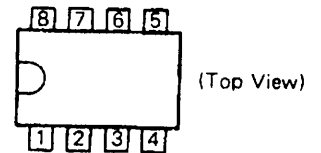


Fig. 3 Block Diagram



Pin No.	Function
1	Ref. Voltage Output
2	Com. Output
3	Inv. Input
4	Non-Inv. Input
5	VS
6	Pulse Output
7	GND.
8	AC Input

Fig. 4 Pin Connections

- Symmetrical burst control
Symmetrical burst control (each one cycle control, not half-cycle) – no DC current components in the load circuit.
 - Enough output trigger pulse for triacs
Negative output current pulse up to 250 mA with short circuit protection, and pulse widths is a few 100 μs.
 - Prevention function of mistrigger
Including low voltage detector – never generate mistrigger pulse, when the supply voltage for IC is low (ex. just after switched ON).
 - Wide input common-mode range
Comparator input constructed by PNP Transistors – wide input common-mode range.
With output terminal of open collector – it is possible to adjust hysteresis.
 - For resistive load
μPC1701C is only for resistive load, because this IC is zero voltage detective type of AC supply voltage.
- And absolute maximum ratings and electrical characteristics are shown in Table 1, 2.

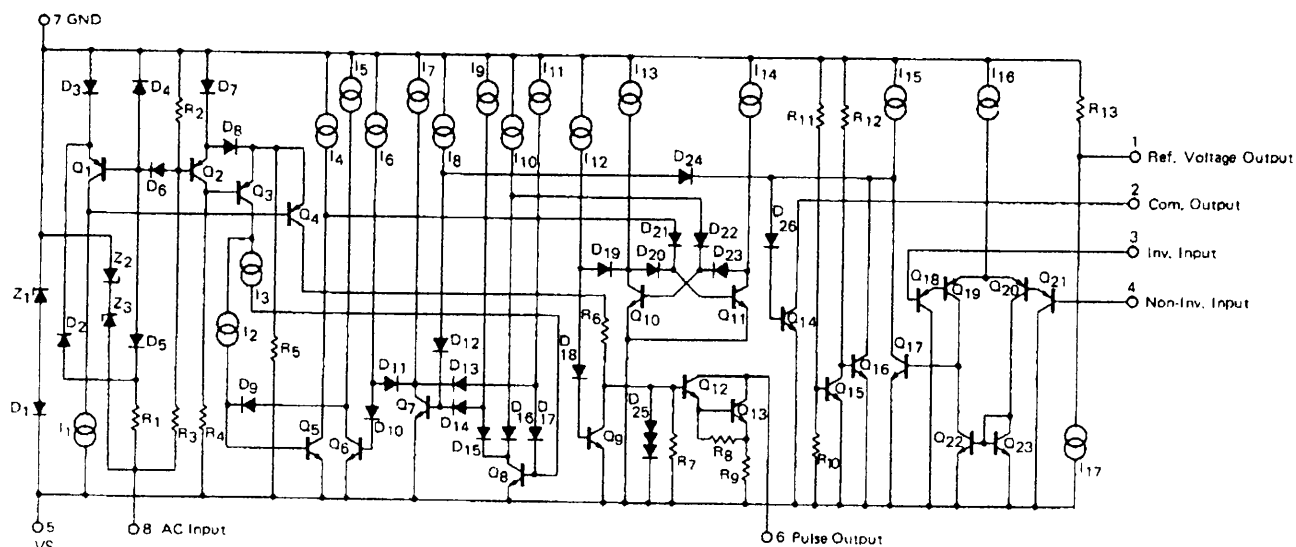


Fig. 5 Equivalent Circuit "μPC1701C"

Table 1 Absolute Maximum Ratings ($T_a=25^\circ\text{C}$)

ITEMS	SYMBOL	CONDITIONS	RATINGS	UNIT
Supply Voltage	V_s	External DC power supply terminal 7 – 5	–8.0	V
Average Supply Current	I_s	External power supply	–40	mA
RMS Synchronous Current	I_{syn}	Commercial frequency power supply terminal 7 – 8	5.0	mA
Input Voltage	V_i	Terminal 7 – 1, 7 – 3, 7 – 4, 7 – 8	$\leq V_s $	V
Junction Temperature	T_j	–	125	$^\circ\text{C}$
Operating Ambient Temperature	T_{opt}	–	–20 ~ 70	$^\circ\text{C}$
Storage Temperature	T_{stg}	–	–40 ~ 125	$^\circ\text{C}$
Power Dissipation	P	–	350	mW

Table 2 Electrical Characteristics ($T_a=25^\circ\text{C}$, $V_s=8\text{ V}$, $V_{syn}=100\text{ V}_{RMS}$, $f=50\sim 60\text{ Hz}$)

ITEMS	PIN. NO.	SYMBOL	MIN.	TYP.	MAX.	UNIT	TEST CONDITIONS
Circuit Current	Pin 5	$-I_S$	–	2.0	2.5	mA	$R_{syn}=56\text{ k}\Omega$
Supply Voltage 1	Pin 5	$-V_{S1}$	8.3	–	9.5	V	$I_S=2.5\text{ mA}$, $R_{syn}=56\text{ k}\Omega$
Supply Voltage 2	Pin 5	$-V_{S2}$	8.2	–	9.6	V	$I_S=20\text{ mA}$, $R_{syn}=56\text{ k}\Omega$
Synchronous Current	Pin 8	I_{syn}	0.3	–	–	mA	
Output Pulse Width	Pin 6	t_p	–	200	–	μs	$R_{syn}=56\text{ k}\Omega$
Output Voltage	Pin 6	V_o	5.0	6.0	–	V	$I_o \leq 200\text{ mA}$
Output Current	Pin 6	I_o	200	250	–	mA	$R_o \leq 25\text{ }\Omega$
Output Leakage Current	Pin 6	I_{LO}	–	–	2.0	μA	
Input Offset Voltage	Pin 3, 4	V_{IO}	–	2.0	5.0	mV	
Input Bias Current	Pin 3, 4	I_i	–	0.5	1.0	μA	
Common Mode Input Voltage Range	Pin 3, 4	$-V_{ICM}$	0	–	6.5	V	
Output Leakage Current	Pin 2	I_{LC}	–	–	0.2	μA	
Reference Voltage	Pin 1	$-V_R$	3.7	4.0	4.2	V	$I_R \leq 1\text{ }\mu\text{A}$

4. ZERO VOLTAGE ON-OFF CONTROL CIRCUIT AND $\mu\text{PC1701C}$

Basic constitution of zero voltage control circuit using ZVS " $\mu\text{PC1701C}$ " is shown in Fig. 6.

ZVS is connected to AC line directly, so this circuit requires minimal external components.

Basically the circuit operation is as follows: (see Fig. 3)

Near the zero point of AC supply voltage, Amplifier Q_1 supplies the triac triggering current (negative gate drive) from zero voltage detector which is composed of the synchronous stage and the pulse generator, and also the triac triggering current is controlled ON or OFF by output signal of the Comparator.

More detail of circuit operation is as follows:

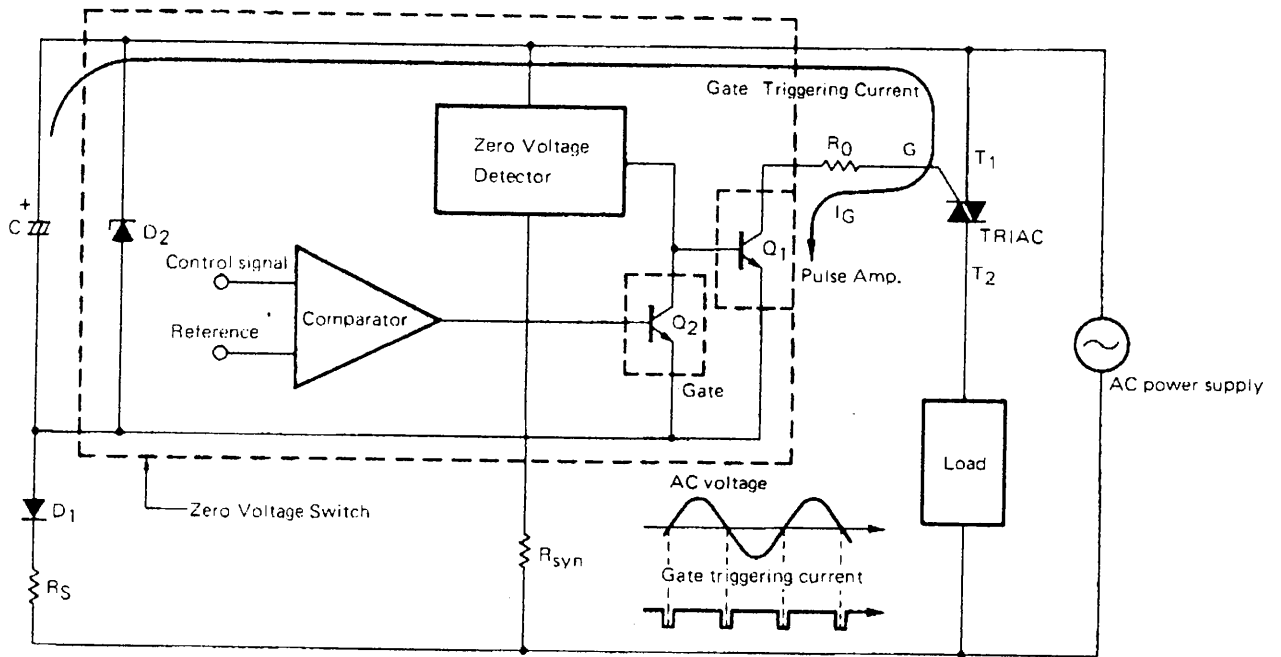


Fig. 6 Zero Voltage ON-OFF Control Circuit

— Application Example —

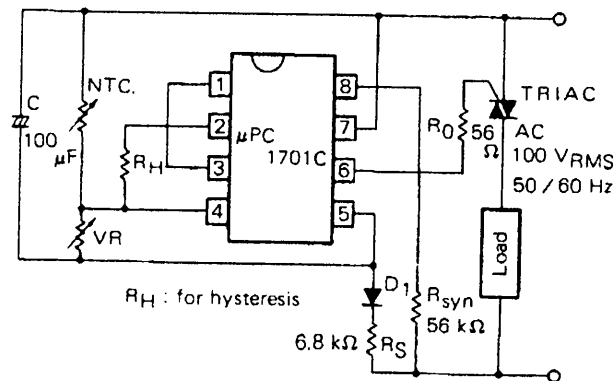


Fig. 7 ON-OFF Temperature Control Circuit

1) Power supply of ZVS

In Fig. 6, the power supply capacitor C is charged up to the zener voltage (V_Z) of D₂ through diode D₁ and R_s, typically 8.5~9.0 V.

The circuit current (I_{cc}) of one cycle controlled logic, comparator, etc. connected in parallel to D₂ is max. 2.5 mA at 8.0 V. Supply voltage V_s of absolute maximum rating in Table 1 is specified only by using external DC power supply with over 40 mA power supply current (I_s), because over 40 mA current destroy the D₂.

Average DC voltage of half wave rectifier circuit is 45 % of R.M.S. AC power supply voltage (V_{RMS}), therefore the current (I_s) flowing into ZVS is;

$$I_s = (0.45 V_{RMS} - V_Z) / R_s \quad \dots\dots\dots (1)$$

Example, $R_s = 20 \text{ k}\Omega$ ($V_{RMS} = 100 \text{ V}$, $V_Z = 9 \text{ V}$), $I_s = 1.8 \text{ mA}$

But I_s is lower than the circuit current (2.5 mA), so it is necessary to decrease R_s value in the range of max. 40 mA I_s , because no current flow into zener diode D₂ and it is impossible to get normal circuit conduct.

R_s is determined by thinking about a sensor current and gate triggering average current (will be discussed later).

2) Zero point detect and triac trigger

The zero voltage detector (in Fig. 6) is in the biased state wherein the AC voltage across the R_{syn} is applied.

Only at point near the zero voltage, output signal of the zero voltage detector turns on Q₂.

Triac gate triggering current supply from capacitor C through T₁ terminal, G terminal, R₀, and Q₁.

Regarding Fig. 7 (one of the application circuit), Zero point is detected by AC voltage applied ZVS terminals between 8 and 7, and equivalent transistor which is shown in Fig. 6, Q₁ is included in terminal between 6 and 5.

This transistor switch has a constant current characteristic and can flow the current minimum 200 mA.

R₀ is determined by thinking about triac gate sensitivity and power consumption of R₀.

3) Comparator

Another important function is comparator which controls triggering pulse ON-OFF.

When output of comparator is low level in Fig. 6, Q₂ is off and triggering pulse flows through R₀ and Q₁ by output signal of zero voltage detector.

In real circuit, as shown in Fig. 3, there is one cycle control function which is composed of memorys G₁~G₄ after output of the comparator.

In Fig. 7 the comparator in $\mu\text{PC1701C}$ compares the reference voltage of the inverting input terminal 3 with the voltage of the noninverting input terminal 4 which is divided by variable resistance V_R and temperature sensor NTC (negative temperature coefficient thermistor).

4) R_{syn} , R_s , R_0 and C design in Fig. 6, 7

(1) R_{syn} value

Triac gate triggering pulse width t_p is changed by R_{syn} value.

Example, at $V_{RMS} = 100 \text{ V}$,

$R_{syn} = 20 \text{ k}\Omega$ — $t_p \approx 150 \mu\text{s}$

$R_{syn} = 56 \text{ k}\Omega$ — $t_p \approx 200 \mu\text{s}$

$R_{syn} = 100 \text{ k}\Omega$ — $t_p \approx 300 \mu\text{s}$,

But the t_p is produced at zero point of AC voltage as a center, so $1/2 t_p$ is efficiency for triggering the triac. R_{syn} is designed so that $1/2 t_p > t_L$ (latching time of the triac). Latching time t_L is determined employing equation (2).

$$I_{LOAD} = (\sqrt{2} V_{RMS} / R_L) \sin \omega t \geq I_{Latch} \quad \dots\dots\dots (2)$$

(R_L : Load resistance, I_{Latch} : triac latching current)

The other way making t_p wider is a capacitor C_{syn} connection between terminal 7 and 8.
(C_{syn} ; 1000 pF~20000 pF, 25 V)

(2) R_0 value

R_0 is determined employing equation (3).

$$I_{GT} < I_G = \{8.5 - (V_{GT} + V_{6-5})\} / R_0 \quad (3)$$

I_{GT} ; triac gate trigger current (thinking about temperature characteristic)
 I_G ; triggering current for triac (Peak value)
 8.5 ; charging voltage of C
 V_{GT} ; triac gate trigger voltage
 V_{6-5} ; voltage between terminal 6 and 5, about 1 V

(3) R_s value

R_s is determined employing equation (4), (5), (6)

$$I_{G(AV)} = 2 \times I_G \times t_p \times f \quad (4)$$

f ; frequency of AC supply

$$I_s = I_{cc} + I_{G(AV)} + I(\text{sensor}) \quad (5)$$

I_{cc} ; circuit current of ZVS, 2.5 mA max.
 $I(\text{sensor})$; sensor current

$$R_s \leq (0.45 V_{RMS} - 9) / I_s \quad (6)$$

R_s consumption power is shown as equation (7)

$$P_s = (V_{RMS} - 9)^2 / 2R_s \quad (7)$$

(4) C value

It is possible to use 100 μF until I_s is about 4 mA. But we recommend using 220 μF and the capacitor voltage is enough to be 15 V.

(5) Reference voltage

The circuit shown in Fig. 7 is using a included reference voltage in ZVS (connected terminal 1 and 3).
 If it is necessary to control more precision, it is better to connect the terminal 3 to divided resistor between terminal 7 and 5.

(6) Hysteresis design

Hysteresis is set up by R_H which is connecting to output terminal 2 (open collector) as shown in Fig. 8.
 When a resistance of the thermistor is high in low temperature, transistor Q14 is On, V_R and R_H is connected in parallel. As temperature increase, voltage of terminal 4 becomes to be higher than voltage of terminal 3 and Q14 to be OFF.
 Therefore, the voltage of terminal 4 is higher than the parallel voltage of V_R and R_H .

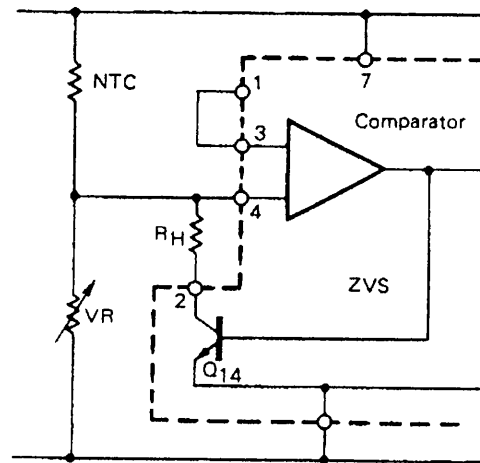


Fig. 8 Hysteresis Circuit

5. TIME PROPORTIONAL CONTROL WITH ZERO VOLTAGE SWITCHING

Fig. 9 is an example of time proportional control using "μPC1701C".

In this circuit the modulation generator is a relaxation oscillator, using the N13TI Programmable Unijunction Transistor (PUT), which produces a sawtooth waveform with a period determined by $R_T C_T$.

The gate voltage of PUT is determined by R_R between terminal 1 and 7, which is reference voltage at open (∞) and 2 V at 39 kΩ.

This resistor is used for setting limits to voltage terminal 3 (comparator input terminal) and terminal 4, because common mode input voltage range of comparator is from a voltage terminal 5 to 1.5 V under voltage terminal 7. Capacitor 0.1 μF between terminal 3 and 4 is used for prevention of wrong operation which repeat ON-OFF every one cycle, when OFF change to ON.

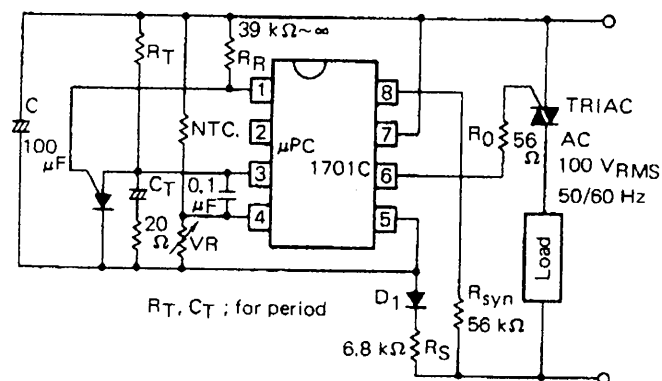


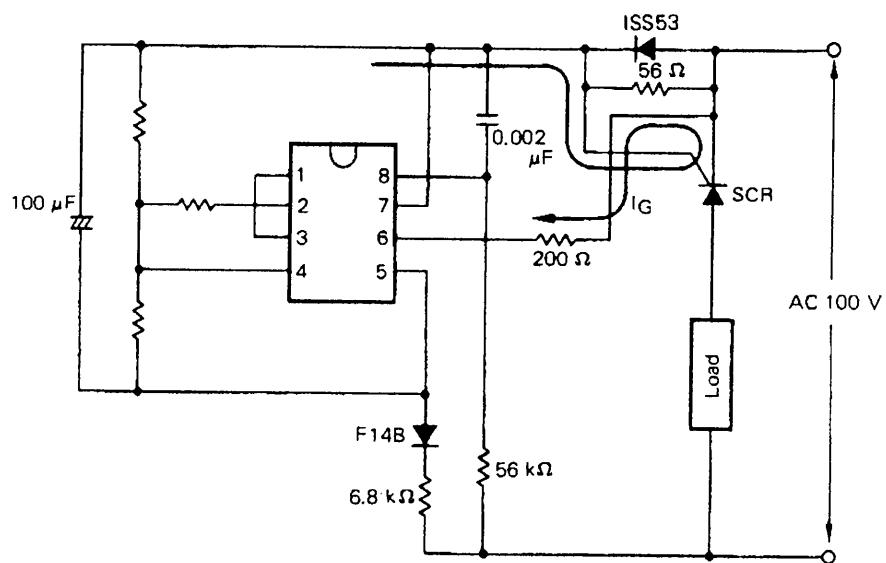
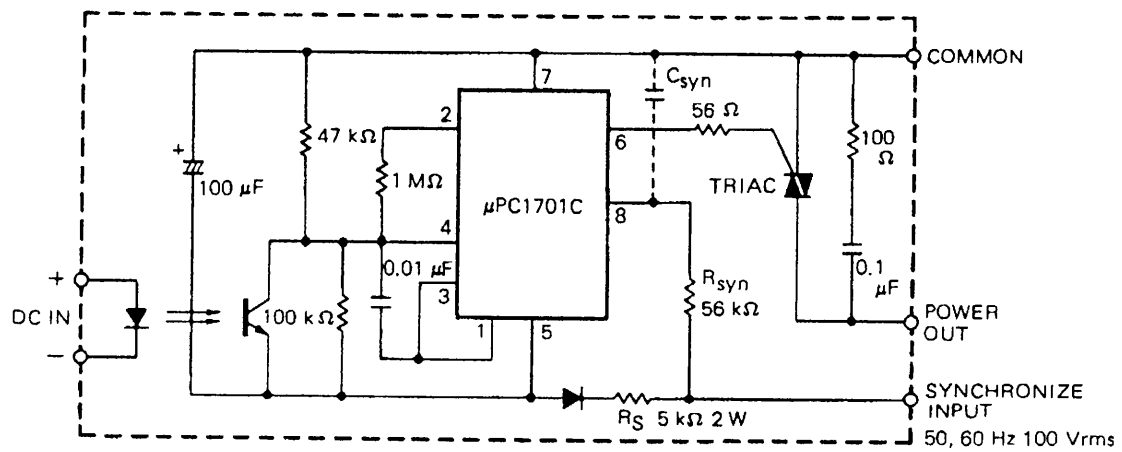
Fig. 9 Time Proportional Temperature Control Circuit

6. OTHER APPLICATION

Fig. 10 is an example of solid state relay application. One more terminal (synchronize input) is necessary, but it is possible to set up hysteresis by comparator, so that ON-OFF operation will be smooth as compared with analogue variation of photo diode.

Fig. 11 is an application for SCR. Fig. 12 is also for SCR, triggering pulse is only generated in half cycle, SCR anode positive.

Fig. 13 is triac triggering circuit which terminal 5 is connected directly to AC line. Triggering pulse is only generated in half cycle, triac T2 positive, so that it is necessary to delay triggering pulse by connection C_1 or C_2 . Be careful with noise, because this circuit is not complete zero voltage switch.



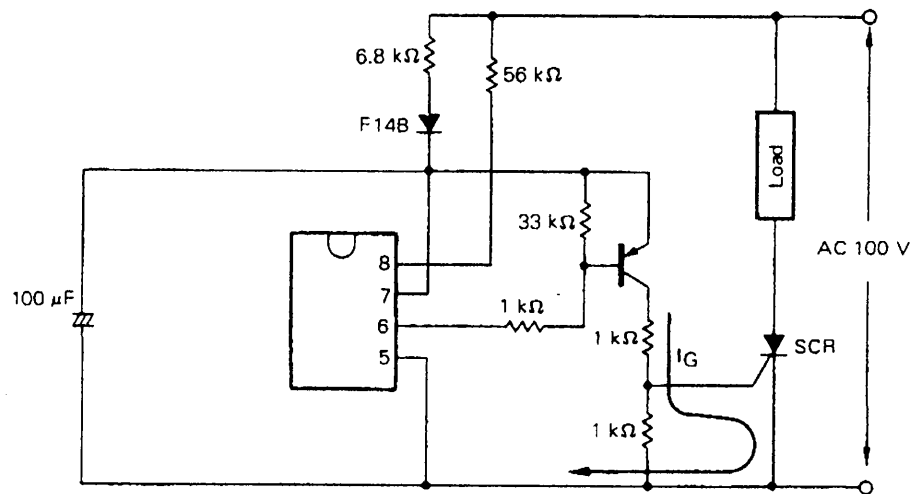


Fig. 12 SCR Triggering Circuit with Direct Connection Terminal 5 on Line

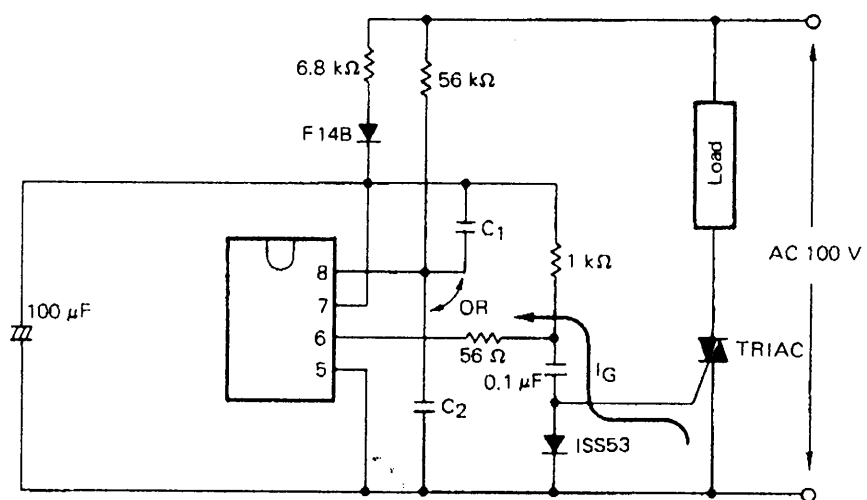


Fig. 13 Triac Triggering Circuit with Direct Connection Terminal 5 on Line

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