# Micrel's Guide to

# Designing With Low-Dropout Voltage Regulators

Bob Wolbert Applications Engineering Manager

Revised Edition, December 1998

Micrel Semiconductor 1849 Fortune Drive San Jose, CA 95131 Phone: +1 (408) 944-0800 Fax: +1 (408) 944-0970

### Micrel, The High Performance Analog Power IC Company

Micrel Semiconductor designs, develops, manufactures, and markets high performance analog power integrated circuits on a worldwide basis. These circuits are used in a wide variety of electronic products, including those in cellular communications, portable and desktop computers, and in industrial electronics.

#### **Micrel History**

Since its founding in 1978 as an independent test facility of integrated circuits, Micrel has maintained a reputation for excellence, quality and customer responsiveness that is second to none.

In 1981 Micrel acquired its first independent semiconductor processing facility. Initially focusing on custom and specialty fabrication for other IC manufacturers, Micrel eventually expanded to develop its own line of semicustom and standard product Intelligent Power integrated circuits. In 1993, with the continued success of these ventures, Micrel acquired a new 57,000 sq. ft. facility and in 1995 expanded the campus into a 120,000 sq. ft. facility. The new Class 10 facility has allowed Micrel to extend its process and foundry capabilities with a full complement of CMOS/DMOS/Bipolar/NMOS/PMOS processes. Incorporating metal gate, silicon gate, dual metal, dual poly and feature sizes down to 1.5 micron, Micrel is able to offer its customers unique design and fabrication tools.



#### Micrel Today and Beyond

Building on its strength as an innovator in process and test technology, Micrel has expanded and diversified its business by becoming a recognized leader in the high performance analog power control and management markets.

The company's initial public offering in December of 1994 and recent ISO9001 compliance are just two more steps in Micrel's long range strategy to become the preeminent supplier of high performance analog power management and control ICs. By staying close to the customer and the markets they serve, Micrel will continue to remain focused on cost effective standard product solutions for an ever changing world.

The niche Micrel has carved for itself involves:

- High Performance.....precision voltages, high technology (Super βeta PNP<sup>™</sup> process, patented circuit techniques, etc.) combined with the new safety features of overcurrent, overvoltage, and overtemperature protection
- Analog.....we control continuously varying outputs of voltage or current as opposed to digital ones and zeros (although we often throw in "mixed signal" i.e. analog with digital controls to bring out the best of both worlds)
- **Power ICs**....our products involve high voltage, high current, or both

We use this expertise to address the following growing market segments:

- 1. Power supplies
- 2. Battery powered computer, cellular phone, and handheld instruments
- 3. Industrial & display systems
- 4. Desktop computers
- 5. Aftermarket automotive
- 6. Avionics
- 7. Plus many others

Copyright © 1998 Micrel, Inc.

All rights reserved. No part of this publication may be reproduced or used in any form or by any means without written permission of Micrel, Incorporated.

Some products in this book are protected by one or more of the following patents: 4,914,546; 4,951,101; 4,979,001; 5,034,346; 5,045,966; 5,047,820; 5,254,486; and 5,355,008. Additional patents are pending.

### Contents

Contributors:	
Section 1. Introduction:	
Low-Dropout Linear Regulators	
What is a Linear Regulator?	
Why Use Regulators?	
Basic Design Issues	
What is a "Low-Dropout" Linear Regulator?	
Linear Regulators vs. Switching Regulators Who Prefers Linear Low Dropout Regulators?	
Section 2. Low-Dropout Regulator	
Design Charts	
Regulator Selection Charts	
Regulator Selection Table	
Maximum Power Dissipation by Package Type	
Typical Thermal Characteristics	
Output Current vs. Junction Temperature and Voltage Different	
Junction Temperature Rise vs. Available Output Current	
and Differential Voltage	
Section 3. Using LDO Linear Regulators	
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations	
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors	
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor	<b></b>
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout	<b></b>
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly	25 
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending	<b>25 25 25 25 25 25 26 26 26 26 27</b>
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment	<b>25</b> <b>25</b> <b>25</b> <b>25</b> <b>25</b> <b>25</b> <b>25</b> <b>26</b> <b>26</b> <b>26</b> <b>26</b> <b>27</b> <b>27</b> <b>27</b>
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment Output Voltage Accuracy	25 25 25 25 25 25 26 26 26 26 27 27 27 28
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment Output Voltage Accuracy Adjustable Regulator Accuracy Analysis	25 
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout	25 25 25 25 25 26 26 26 26 27 27 27 27 27 27 28 28 28 29
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment Output Voltage Accuracy Adjustable Regulator Accuracy Analysis Improving Regulator Accuracy Regulator & Reference Circuit Performance	25 
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout	25 25 25 25 25 25 26 26 26 26 27 27 27 27 27 28 28 28 29 30 32
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment Output Voltage Accuracy Adjustable Regulator Accuracy Analysis Improving Regulator Accuracy Regulator & Reference Circuit Performance Design Issues and General Applications	25 25 25 25 25 26 26 26 26 27 27 28 28 29 30 32 32
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout	25 25 25 25 25 25 26 26 26 27 27 27 28 28 29 30 32 32 32 32
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment Output Voltage Accuracy Adjustable Regulator Accuracy Analysis Improving Regulator Accuracy Regulator & Reference Circuit Performance Design Issues and General Applications Noise and Noise Reduction Stability LDO Efficiency Building an Adjustable Regulator Allowing 0V Output	25 25 25 25 25 26 26 26 26 27 27 28 28 29 30 32 32 32 32 32 32
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout	25 25 25 25 25 25 26 26 26 27 27 27 28 28 29 30 32 32 32 32 32 32 32 32
Section 3. Using LDO Linear Regulators General Layout and Construction Considerations Layout Bypass Capacitors Output Capacitor Circuit Board Layout Assembly Lead Bending Heat Sink Attachment Output Voltage Accuracy Adjustable Regulator Accuracy Analysis Improving Regulator Accuracy Regulator & Reference Circuit Performance Design Issues and General Applications Noise and Noise Reduction Stability LDO Efficiency Building an Adjustable Regulator Allowing 0V Output	25 25 25 25 25 26 26 26 27 27 27 28 28 29 30 32 32 32 32 32 32 32 32 32 32

High Input Voltages	
Controlling Voltage Regulator Turn-On Surges	
The Simplest Approach	
Improving the Simple Approach	
Eliminating Initial Start-Up Pedestal	
Current Sources	
Simple Current Source	
The Super LDO Current Source	
Accurate Current Source Using Op Amps	
A Low-Cost 12V & 5V Power Supply 37	
Computer Power Supplies	9
Dropout Requirements	-
5V to 3.xV Conversion Circuits	
Method 1: Use a Monolithic LDO	
Method 2: The MIC5156 "Super LDO"	
Method 3: The MIC5158 "Super LDO"	
Method 4: Current Boost a MIC2951	
Adjust Resistor Values	
3.3V to 2.xV Conversion	
Improving Transient Response	
Accuracy Requirements	
Multiple Output Voltages	
Multiple Supply Sequencing	
Thermal Design	
Portable Devices	6
Portable Devices	6
Design Considerations	6
	6
Design Considerations       46         Small Package Needed       46         Self Contained Power       46	6
<b>Design Considerations</b>	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47	6
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Parameters48	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Primer48Thermal Parameters48	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Primer48Thermal Primer48Thermal Primer48Thermal Primer48Thermal Primer49	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Primer48Thermal Primer48Calculating Thermal Parameters49Calculating Maximum Allowable Thermal Resistance50	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Thermal Management48Thermal Primer48Thermal Primer48Calculating Thermal Parameters49Calculating Maximum Allowable Thermal Resistance50Why A Maximum Junction Temperature?50	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Primer48Thermal Primer48Calculating Thermal Parameters49Calculating Maximum Allowable Thermal Resistance50Why A Maximum Junction Temperature?50Heat Sink Charts for High Current Regulators51	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Parameters48Thermal Parameters48Calculating Thermal Parameters49Calculating Maximum Allowable Thermal Resistance50Why A Maximum Junction Temperature?50Heat Sink Charts for High Current Regulators51Thermal Examples52	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Parameters48Thermal Parameters49Calculating Thermal Parameters49Calculating Maximum Allowable Thermal Resistance50Why A Maximum Junction Temperature?50Heat Sink Charts for High Current Regulators51Thermal Examples52Heat Sink Selection53	
Design Considerations46Small Package Needed46Self Contained Power46Low Current (And Low Voltage)46Low Output Noise Requirement46Dropout and Battery Life47Ground Current and Battery Life47Battery Stretching Techniques47Sleep Mode Switching47Power Sequencing47Multiple Regulators Provide Isolation47Thermal Management48Thermal Parameters48Thermal Parameters48Calculating Thermal Parameters49Calculating Maximum Allowable Thermal Resistance50Why A Maximum Junction Temperature?50Heat Sink Charts for High Current Regulators51Thermal Examples52	

Multiple Packages on One Heat Sink	
Paralleled Devices on a Heat Sink Example	
Heat Sinking Surface Mount Packages	
Determining Heat Sink Dimensions	
SO-8 Calculations:	
Comments	
Linear Regulator Troubleshooting Guide	60
Section 4. Linear Regulator Solutions	
Super βeta PNP <sup>™</sup> Regulators	
Super beta PNP Circuitry	
Dropout Voltage Ground Current	
Fully Protected	
Current Limiting	
Overtemperature Shutdown Reversed Input Polarity	
Overvoltage Shutdown	
0	
Variety of Packages Why Choose First Terminal Pagulators?	
Why Choose Five Terminal Regulators?	
Compatible Pinouts	
Stability Issues	
Paralleling Bipolar Regulators	
Micrel's Unique "Super LDO <sup>TM</sup> "	<b> 6</b> 7
Micrel's Super LDO Family	
The MIC5156	
The MIC5157 and MIC5158	
3.3V, 10A Regulator Application	
Comparison With Monolithics	
Similarities to Monolithics	
Differences from Monolithics	
Unique Super LDO Applications	
Super High-Current Regulator	
Selecting the Current Limit Threshold	
Sense Resistor Power Dissipation	
Kelvin Sensing	
Alternative Current Sense Resistors	
<b>Overcurrent Sense Resistors from PC Board Traces</b>	
Resistor Design Method	
Design Example	
Calculate Sheet Resistance	
Calculate Minimum Trace Width	
Calculate Required Trace Length	
Resistor Layout	
Thermal Considerations	
Design Aids	
Highly Accurate Current Limiting	
Protecting the Super LDO from Long-Term Short Circuits	

Section 5. Micrel Low-Dropout Regulator Data Sheets	
Monolithic Regulators	
MIC2920A/29201/29202/29204 400mA Low-Dropout Voltage Regulator	
MIC2937A/29371/29372 750mA Low-Dropout Voltage Regulator	
MIC2940A/2941A 1.25A Low-Dropout Voltage Regulator	
LP2950/LP2951 100mA Low-Dropout Voltage Regulator	
MIC2950/2951 150mA Low-Dropout Voltage Regulator	
MIC2954 250mA Low-Dropout Voltage Regulator	
MIC29150/29300/29500/29750-Series	
High-Current Low-Dropout Regulators	
MIC29310/29312 3A Fast-Response LDO Regulator	155
MIC29510/29512 5A Fast-Response LDO Regulator	
MIC29710/29712 7.5A Fast-Response LDO Regulator	
MIC39150/39151 1.5A Low-Voltage Low-Dropout Regulator	
MIC39300/39301 3A Low-Voltage Low-Dropout Regulator	
MIC5200 100mA Low-Dropout Voltage Regulator	
MIC5201 200mA Low-Dropout Voltage Regulator	
MIC5202 Dual 100mA Low-Dropout Voltage Regulator	
MIC5203 80mA Low-Dropout Voltage Regulator	
MIC5205 150mA Low-Noise LDO Voltage Regulator	
MIC5206 150mA Low-Noise LDO Voltage Regulator	
MIC5207 180mA Low-Noise LDO Voltage Regulator	
MIC5208 Dual 50mA LDO Voltage Regulator	
MIC5209 500mA Low-Noise LDO Voltage Regulator	
MIC5210 Dual 150mA LDO Regulator	
MIC5211 Dual $\mu$ Cap <sup>TM</sup> 50mA LDO Voltage Regulator	
MIC5216 500mA-Peak Output LDO Voltage Regulator	
MIC5219 500mA-Peak Output LDO Voltage Regulator	
MIC5237 500mA Low-Dropout Voltage Regulator	
LDO Regulator Controller ICs	
MIC5156/5157/5158 Super LDO™ Regulator Controller	
Section 6. Package Information	321
Packaging for Automatic Handling	322
Tape & Reel	
Ammo Pack	
Pricing	
Tape & Reel Standards	322
Packages Available in Tape & Reel	
Package Orientation	323
Linear Regulator Packages	
8-Pin Plastic DIP (N)	
14-Pin Plastic DIP (N)	
8-Pin SOIC (M)	
14-Pin SOIC (M)	
TO-92 (Z)	
SOT-223 (S)	

SOT-143 (M4)	327
SOT-23 (M3)	327
SOT-23-5 (M5)	328
MSOP-8 [MM8 <sup>TM</sup> ] (MM)	328
3-Lead TO-220 (T)	329
5-Lead TO-220 (T)	
5-Lead TO-220 Vertical Lead Bend Option (-LB03)	
5-Lead TO-220 Horizontal Lead Bend Option (-LB02)	
3-Lead TO-263 (U)	
5-Lead TO-263 (U)	
Typical 3-Lead TO-263 PCB Layout	
Typical 5-Lead TO-263 PCB Layout	
3-Lead TO-247 (WT)	
5-Lead TO-247 (WT)	
Section 7. Appendices	335
Appendix A. Table of Standard 1% Resistor Values	336
Appendix A. Table of Standard 1% Resistor Values Appendix B. Table of Standard $\pm 5\%$ and $\pm 10\%$ Resistor Values	
Appendix B. Table of Standard $\pm 5\%$ and $\pm 10\%$ Resistor Values	337
Appendix B. Table of Standard $\pm 5\%$ and $\pm 10\%$ Resistor Values Appendix C. LDO SINK for the HP 48 Calculator	337 338
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary	337 338 341
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References	337 338 341 343
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References Section 10. Index	337 338 341 343
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References	337 338 341 343
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References Section 10. Index	337 338 341 343 344
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References Section 10. Index Section 11. Worldwide	337 338 341 343 344 344
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References Section 10. Index Section 10. Index Section 11. Worldwide Representatives and Distributors Micrel Sales Offices	337 338 341 343 344 347
Appendix B. Table of Standard ±5% and ±10% Resistor Values Appendix C. LDO SINK for the HP 48 Calculator Section 8. Low-Dropout Voltage Regulator Glossary Section 9. References Section 10. Index Section 11. Worldwide Representatives and Distributors	

### **Contributors:**

Jerry Kmetz

Mike Mottola

Jim Cecil

Brian Huffman

Marvin Vander Kooi

Claude Smithson

Micrel Semiconductor 1849 Fortune Drive San Jose, CA 95131 Phone: +1 (408) 944-0800 Fax: +1 (408) 944-0970 http://www.micrel.com

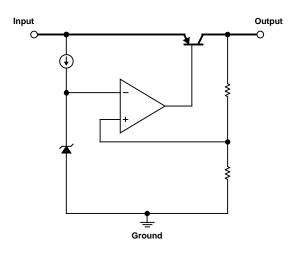
### Section 1. Introduction: Low-Dropout Linear Regulators

### What is a Linear Regulator?

IC linear voltage regulators have been around for decades. These simple-to-use devices appear in nearly every type of electronic equipment, where they produce a clean, accurate output voltage used by sensitive components.

Historically, linear regulators with PNP outputs have been expensive and limited to low current applications. However, Micrel Semiconductor's unique "Super  $\beta$ eta PNP<sup>TM</sup>" line of low dropout regulators provides up to 7.5 amperes of current with dropout voltages less than 0.6V, guaranteed. A lower cost product line outputs the same currents with only 1V of dropout. These low dropout voltages guarantee the microprocessor gets a clean, well regulated supply that quickly reacts to processor-induced load changes as well as input supply variations.

The low dropout linear voltage regulator is a easy-to-use, low cost, yet high performance means of powering your systems.



#### Figure 1-1. A basic linear regulator schematic.

A typical linear regulator diagram is shown in Figure 1-1. A pass transistor is controlled by an operational amplifier which compares the output voltage to a reference. As the output voltage drops, the op-amp increases drive to the pass element, which increases output voltage. Conversely, if the output rises above the desired set point, the op amp reduces drive. These corrections are performed continuously with the reaction time limited only by the speed of the op amp and output transistor loop.

Real linear regulators have a number of other features, including protection from short circuited loads and overtemperature shutdown. Advanced regulators offer extra features such as overvoltage shutdown, reversed-insertion and reversed polarity protection, and digital error indicators that signal when the output is not correct.

### Why Use Regulators?

Their most basic function, voltage regulation, provides clean, constant, accurate voltage to a circuit. Voltage regulators are a fundamental block in the power supplies of most all electronic equipment.

Key regulator benefits and applications include:

- Accurate supply voltage
- Active noise filtering
- Protection from overcurrent faults
- Inter-stage isolation (decoupling)
- Generation of multiple output voltages from a single source
- Useful in constant current sources

Figure 1-2 shows several typical applications for linear voltage regulators. A traditional AC to DC power supply appears in Figure 1-2(A). Here, the linear regulator performs ripple rejection, eliminating AC hum, and output voltage regulation. The power supply output voltage will be clean and constant, independent of AC line voltage variations. Figure 1-2(B) uses a low-dropout linear regulator to provide a constant output voltage from a battery, as the battery discharges. Low dropout regulators are excellent for this application since they allow more usable life from a given battery. Figure 1-2(C) shows a linear regulator configured as a "post regulator" for a switching power

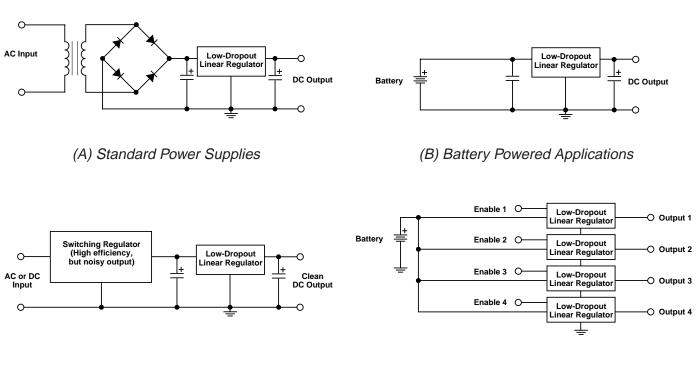
supply. Switching supplies are known for excellent efficiency, but their output is noisy; ripple degrades regulation and performance, especially when powering analog circuits. The linear regulator following the switching regulator provides active filtering and greatly improves the output accuracy of the composite supply. As Figure 1-2(D) demonstrates, some linear regulators serve a double duty as both regulator and power ON/OFF control. In some applications, especially radio systems, different system blocks are often powered from different regulators—even if they use the same supply voltage—because of the isolation (decoupling) the high gain regulator provides.

### **Basic Design Issues**

Let's review the most important parameters of voltage regulators:

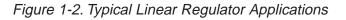
 Output voltage is an important parameter, as this is the reason most designers purchase a regulator. Linear regulators are available in both fixed output voltage and adjustable configurations. Fixed voltage regulators offer enhanced ease-ofuse, with their output voltages accurately trimmed at the factory—but only if your application uses an available voltage. Adjustables allow using a voltage custom-tailored for your circuit.

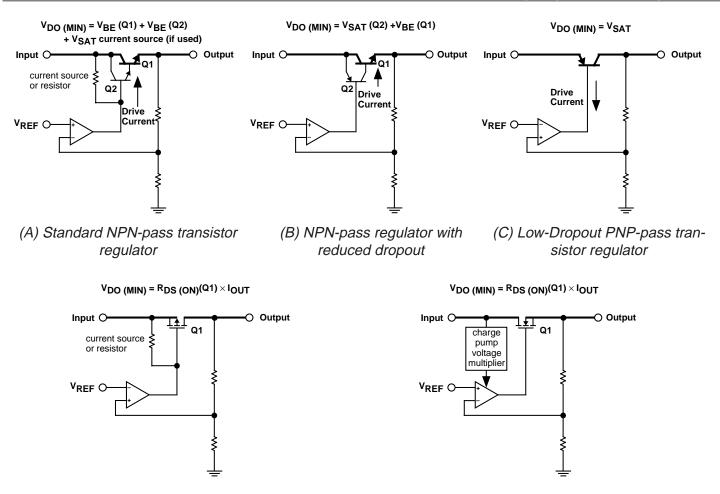
- Maximum output current is the parameter generally used to group regulators. Larger maximum output currents require larger, more expensive regulators.
- Dropout voltage is the next major parameter. This is the minimum additional voltage on the input that still produces a regulated output. For example, a Micrel 5.0V Super βeta PNP regulator will provide regulated output with an input voltage of 5.3V or above. The 300mV term is the dropout voltage. In the linear regulator world, the lower the dropout voltage, the better.
- Ground current is the supply current used by the regulator that does not pass into the load. An ideal regulator will minimize its ground current. This parameter is sometimes called quiescent current, but this usage is incorrect for PNP-pass element regulators.



(C) Post-Regulator for Switching Supplies

(D) "Sleep-mode" and Inter Stage Isolation or Decoupling





(D) P-Channel MOSFET-pass transistor regulator

(E) N-Channel MOSFET-pass transistor regulator

Figure 1-3. The Five Major Types of Linear Regulators

 Efficiency is the amount of usable (output) power achieved from a given input power. With linear regulators, the efficiency is approximately the output voltage divided by the input voltage.

### What is a "Low-Dropout" Linear Regulator?

A low dropout regulator is a class of linear regulator that is designed to minimize the saturation of the output pass transistor and its drive requirements. A low-dropout linear regulator will operate with input voltages only slightly higher than the desired output voltage. For example, "classic" linear regulators, such as the 7805 or LM317 need about 2.5 to 3V higher input voltage for a given output voltage. For a 5V output, these older devices need a 8V input. By comparison, Micrel's Super beta PNP low dropout regulators require only 0.3V of headroom, and would provide regulated output with only 5.3V of input.

Figure 1-3 shows the five major types of linear regulators:

- A. "Classic" NPN-based regulators that require 2.5 to 3V of excess input voltage to function.
- B. "Low Dropout NPN" regulators, with a NPN output but a PNP base drive circuit. These devices reduce the dropout requirement to 1.2 to 1.5V.
- C. True low dropout PNP-based regulators that need 0.3V to 0.6V extra for operation.
- D. P-channel CMOS output regulators. These devices have very low dropout voltages at low currents but require large die area (hence higher costly than bipolar versions) and have high internal drive current requirements when working with noisy inputs or widely varying output currents.

Designing With LDO Regulators

E. Regulator controllers. These are integrated circuits that provide the reference and control functions of a linear regulator, but do not have the pass element on board. They provide the advantage of optimizing die area and cost for higher current applications but suffer the disadvantage of being a multiple package solution.

If we graph the efficiency of the different classes of linear regulators we see very significant differences at low input and output voltages (see Figure 1-4). At higher voltages, however, these differences diminish. A 3.3V high current linear regulator controller such as the Micrel MIC5156 can approach 100% efficiency as the input voltage approaches dropout. But an LM317 set to 3.3V at 1A will have a miserable efficiency of only about 50% at its dropout threshold.

### Linear Regulators vs. Switching Regulators

Linear regulators are less energy efficient than switching regulators. Why do we continue using them? Depending upon the application, linear regulators have several redeeming features:

- lower output noise is important for radios and other communications equipment
- · faster response to input and output transients
- easier to use because they require only filter capacitors for operation
- generally smaller in size (no magnetics required)
- less expensive (simpler internal circuitry and no magnetics required)

Furthermore, in applications using low input-tooutput voltage differentials, the efficiency is not all that bad! For example, in a 5V to 3.3V microprocessor application, linear regulator efficiency approaches 66%. And applications with low current subcircuits may not care that regulator efficiency is less than optimum as the power lost may be negligible overall.

## Who Prefers Linear Low Dropout Regulators?

We see that price sensitive applications prefer linear regulators over their sampled-time counterparts. The design decision is especially clear cut for makers of:

- communications equipment
- small devices
- battery operated systems
- low current devices
- high performance microprocessors with sleep mode (fast transient recovery required)

As you proceed through this book, you will find numerous other applications where the linear regulator is the best power supply solution.

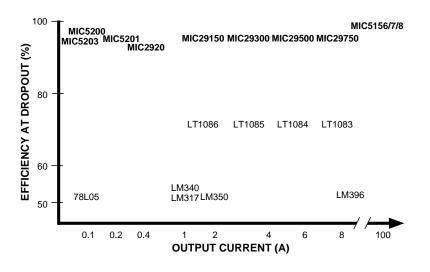


Figure 1-4. Linear Regulator Efficiency at Dropout

### Section 2. Low-Dropout Regulator Design Charts

### **Regulator Selection Charts**

Output Current	Accuracy	Low Noise	Single or Dual	Without Error Flag	With Error Flag
		Yes	Dual	MIC5210         Dual 150mA LDO w/ Noise Bypass           MSOP-8         3.0, 3.3, 3.6, 4.0, 5.0V	
			Single	MIC5205         150mA LDOw/ Noise Bypass           SOT23-5         2.8, 3.0, 3.3, 3.6, 3.8, 4.0, 5.0V, Adj	MIC5206         150mA LDOs w Noise Bypass           SOT23-5, MSOP-8         2.5, 3.0, 3.3, 3.6, 4.0, 5.0V, Adj
	±1.0%		Dual	MIC5202         Dual 100mA LDO           SO-8         3.0, 3.3, 4.5, 4.85, 5.0V	
		No	-	LP2950 100mA LDO Second Source to '2950 TO-92 5.0V	LP2951 100mA LDO Second Source to '2951
			Single	MIC2950         150mA LDO Upgrade to '2950           TO-92         5.0V           MIC5200         100mA LDO	SO-8, PDIP-8         4.85, 5.0V, Adj           MIC2951         150mA LDO Upgrade to '2951           SO-8, PDIP-8, MSOP-8         3.3, 4.85, 5.0V, Adj
0 –180mA–				SO-8, SOT-223, MSOP-8 3.0, 3.3, 4.85, 5.0V	
		Yes		MIC5207         180mA LDO           SOT23-5, TO-92         1.8, 2.5, 3.0, 3.3, 3.6, 3.8, 5.0V, Adj	
	±3.0%		Dual	MIC5211         Dual 50mA μCap LDO           SOT23-6         2.5, 3.0, 3.3, 3.6, 5.0, Mixed 3.3/5.0V           MIC5208         Dual 50mA μCap LDO	
		No	Cinala	MSOP-8 3.0, 3.3, 3.6, 4.0, 5.0V	
			Single	SOT-143, SOT23-5 2.8, 3.0, 3.3, 3.6, 3.8, 4.0, 5.0V	
	Г	Yes	Single	MIC5219         500mA Peak LDO           SOT23-5, MSOP-8         3.0, 3.3, 3.6, 5.0V, Adj           MIC5209         500mA LDO	
	±1.0%			SOT223, SO-8, TO263-5 1.8, 2.5, 3.0, 3.3, 5.0V, Adj	
				MIC201         200000           SOT223, SO-8         3.0, 3.3, 4.85, 5.0V, Adj           MIC2954         250mA LDO	MIC5216         500mA Peak LDO           SOT23-5, MSOP-8         3.0, 3.3, 3.6, 5.0V
200mA – 500mA		No	Single	TO220, SOT223, SO-8, TO92         5.0V, Adj           MIC2920         400mA LDO	MIC29201         400mA LDO           TO220, TO263, SO-8         3.3, 4.85, 5.0V
				TO220, SOT223         3.3, 4.85, 5.0V           MIC29202         400mA LDO           TO220, TO263         Adj	MIC29204 400mA LDO SO-8 Adj
	±3.0%	No	Single	MIC5237         500mA LDO           TO220, TO263         2.5, 3.3, 5.0V	
750mA	±1.0%	No	Single	MIC2937A         750mA LDO           TO220, TO263         3.3, 5.0, 12.0V	MIC29371 750mA LDO
				MIC29372         750mA LDO           TO220, TO263         Adj	TO220, TO263 3.3, 5.0V

#### Figure 2-1a. 0 to 750mA LDO Regulator Selection Guide

Shaded boxes denote automotive load dump protected devices

Output Current	Accuracy	Error Flag	Low-	Dropout Devices	Ultra-Low-Dro	opout Devices
		Yes	MIC29151	1.5A LDO	MIC39151	1.5A LDO
			TO220, TO263	3.3, 5.0, 12V	TO263	1.8, 2.5V
1A –	±1.0%		MIC2940A TO220, TO263	1.25A LDO 3.3, 5.0, 12V		
1.5A			MIC2941A	1.25A LDO	MIC39100	1.0A LDO
		No	TO220, TO263	Adj	SOT223	1.8, 2.5, 3.3V
			MIC29150 TO220, TO263	1.5A LDO 3.3, 5.0, 12.0V	MIC39150 TO220, TO263	1.5A LDO 1.8, 2.5V
			MIC29152	1.5A LDO		
			TO220, TO263	Adj		
		Vee	MIC29301 TO220, TO263	3.0A LDO 3.3, 5.0, 12V	MIC39301	2.04.1.DO
		Yes	MIC29303	3.0A LDO	TO263, TO220	3.0A LDO 1.8, 2.5V
			TO220, TO263	Adj		
3.0A	±1.0%		MIC29300	3.0A LDO		
			TO220, TO263	3.3, 5.0, 12.0V 3.0A LDO		
		No	TO220, TO263	3.0A LDO Adj	MIC39300	3.0A LDO
		<u></u>	MIC29310	3.0A Low Cost LDO	TO220, TO263	1.8, 2.5V
			TO220, TO263	3.3, 5.0V		
			MIC29312 TO220, TO263	3.0A Low Cost LDO Adj		
			MIC29501	5.0A LDO		
			TO220, TO263	3.3, 5.0V		
		Yes	MIC29503 TO220, TO263	5.0A LDO Adj		
			MIC29751	7.5A LDO		
			TO247	3.3, 5.0V		
5.0A	±1.0%		MIC29500 TO220, TO263	5.0A LDO 3.3, 5.0V		
7.5A			MIC29502	5.0A LDO		
			TO220, TO263	Adj		
		No	MIC29510 TO220	5.0A Low Cost LDO 3.3, 5.0V		
			MIC29512	5.0A Low Cost LDO		
			TO220 MIC29750	Adj 7.5A LDO		
			TO247	3.3, 5.0V		
			MIC29752 TO247	7.5A Low Cost LDO Adj		
			MIC29710	7.5A LDO		
			TO220	3.3, 5.0V		
			MIC29712 TO220	7.5A Low Cost LDO Adj		
			MIC5156 SO-8, PDIP-8	LDO Controller 3.3, 5.0V, Adj		
>7.5A	±1.0%	Yes	MIC5157	LDO Controller (w/Charge Pump)		
			SO-14, PDIP-14 MIC5158	3.3, 5.0, 12V LDO Controller (w/Charge Pump)		
			SO-14, PDIP-14	5.0V, Adj		

#### Figure 2-1b. 1A to >7.5A LDO Regulator Selection Guide

Shaded boxes denote automotive load dump protected devices

ts



### **Regulator Selection Table**

(Sorted by Output Current Rating)

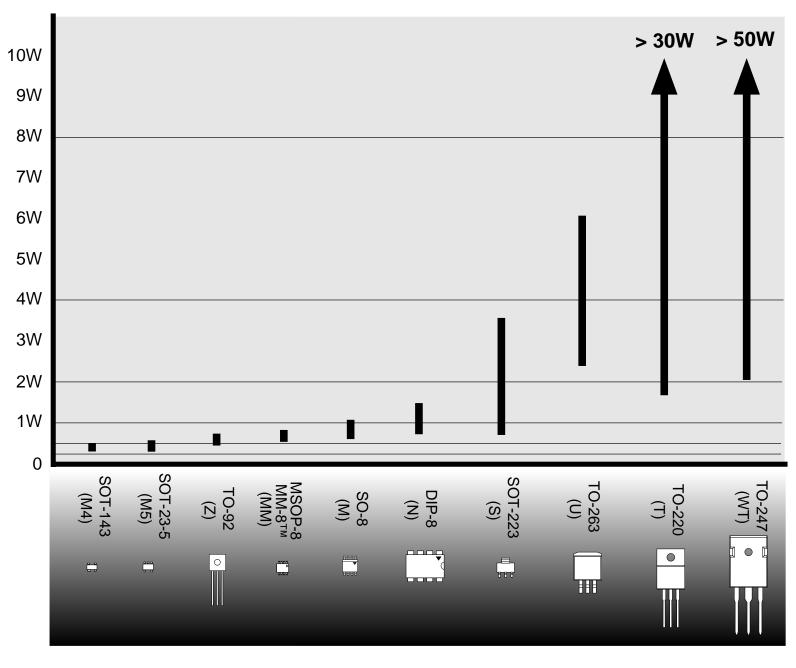
Micrel Semicond

S

O Regulators		Output										age			Adj.		Dropout	Current	Error	Enable/	Thermal	Rev. Input		Packages
eg	Device	Current	1.	8 2.5	2.8	3.0	3.3	3.6	3.8	4.0	4.75	4.85	5.0	12	(max.)	Accuracy	/ (I <sub>MAX</sub> , 25°C)	Limit	Flag	Shutdown	Shutdown	Protection	Dump	Packages S
ulat	MIC5208	$50mA \times 2$				•	•	•		•			٠			3%	250mV	•		•	•	•		MSOP-8
tors	MIC5211	$50mA \times 2$		•		•	•	•					•			3%	250mV	•		•	•	•		SOT-23-6
•	MIC5203	80mA			•	٠	•	•	٠	•	•		•			3%	300mV	•		•	•	•		SOT-143, SOT-23-5
	MIC5200	100mA				٠	•					•	٠			1%	230mV	•		•	•	•		SOP-8, SOT-223, MSOP-8
	MIC5202	$100mA \times 2$				٠	•					•	٠			1%	225mV	•		•	•	•		SOP-8
	LP2950	100mA											٠			<sup>1</sup> ⁄2%,1%	6 380mV	•			•			TO-92
	LP2951	100mA										•	٠		29V	1⁄2%,1%	6 380mV	•	•	•	•			DIP-8, SOP-8
	MIC2950	150mA											٠			<sup>1</sup> ⁄2%,1%	6 300mV	٠			•	•	٠	TO-92
	MIC2951	150mA					•					•	٠		29V	<sup>1</sup> ⁄2%,1%	6 300mV	٠	٠	•	•	•	٠	DIP-8, SOP-8, MSOP-8
15	MIC5205	150mA			•	٠	•	•	٠	•			٠		16V	1%	165mV	٠		•	•	•		SOT-23-5
	MIC5206	150mA				٠	•	•	٠	•			٠		16V	1%	165mV	٠	٠	•	•	•		SOT-23-5, MSOP-8
	MIC5210	$150mA \times 2$				٠	•	•		•			٠			1%	165mV	٠		•	•	•		MSOP-8
	MIC5207	180mV	•	•		٠	•	•	٠	•			٠		16V	3%	165mA	٠		•	•	•		SOT-23-5, TO-92 <sup>SP</sup>
	MIC5201	200mA				٠	•						٠		16V	1%	270mV	٠		•	•	•		SOP-8, SOT-223
	MIC2954	250mA											•		29V	1/2%	375mV	•	٠	•	•	•	٠	TO-92, TO-220, SOT-223
	MIC2920A	400mA					•					•	٠	•		1%	450mV	٠			•	•	٠	TO-220, SOT-223
	MIC29201	400mA					•					•	٠	SP		1%	450mV	٠	٠	•	•	•	٠	TO-220-5, TO-263-5
	MIC29202	400mA													26V	1%	450mV	٠		•	•	•	٠	TO-220-5, TO-263-5 SOP-8, DIP-8 SOT-23-5, MSOP-8
	MIC29204	400mA											٠		26V	1%	450mV	٠	٠	•	•	•	٠	SOP-8, DIP-8
Se	MIC5216	500mA <sup>(1)</sup>				٠	•	•					٠		12V	1%	300mV	٠	٠	•	•	•		SOT-23-5, MSOP-8
ection	MIC5219	500mA <sup>(1)</sup>				٠	•	•					٠		12V	1%	300mV	٠		•	•	•		SOT-23-5, MSOP-8
n	MIC5209	500mA	•	•		٠	•	•					•		16V	1%	300mV	•		•	•	•		SOP-8, SOT-223, TO-263-5
2: D	MIC5237	500mA		٠			•						٠		16V	3%	300mV	٠			•	•		TO-220, TO-263
)esign	MIC2937A	750mA					•						•	•		1%	370mV	٠			•	•	٠	TO-220, TO-263
ign	MIC29371	750mA					•						٠	SP		1%	370mV	٠	٠	•	•	•	٠	TO-220-5, TO-263-5 TO-220-5, TO-263-5
Chart	MIC29372	750mA													26V	1%	370mV	٠		•	•	•	•	TO-220-5, TO-263-5
art																								

MIC2940A	1.25A			•				•	•		1%	400mV	•			•	Protection	•	TO-220, TO-263
MIC2941A	1.25A									26V	1%	400mV	•		•	•	•	•	TO-220-5, TO-263-5
MIC29150	1.5A			•				•	•		1%	350mV	•			•	•	•	TO-220, TO-263
MIC29151	1.5A			•				•	•		1%	350mV	•	•	•	•	•	•	TO-220-5, TO-263-5
MIC29152	1.5A									26V	1%	350mV	•		•	•	•	•	TO-220-5, TO-263-5
MIC29153	1.5A									26V <sup>SP</sup>	1%	350mV	•	•		•	•	•	TO-220-5, TO-263-5
MIC39150	1.5A	•									1%	350mV	•			•	•		TO-220, TO-263
MIC39151	1.5A	•									1%	350mV	٠	٠	•	٠	•		TO-220-5, TO-263-5
MIC29300	ЗA			•				•	•		1%	370mV	٠			٠	•	•	TO-220, TO-263
MIC29301	ЗA			•				•	•		1%	370mV	٠	٠	•	٠	•	•	TO-220-5, TO-263-5
/IC29302	ЗA									26V	1%	370mV	٠		•	•	•	•	TO-220-5, TO-263-5
MIC29303	ЗA									26V	1%	370mV	٠	٠		•	•	•	TO-220-5, TO-263-5
MIC29310	ЗA			•				٠			2%	600mV	•			•			TO-220, TO-263
/IIC29312	ЗA									16V	2%	600mV	•		•	•			TO-220-5, TO-263-5
/IC39300	ЗA	•									1%	400mV	•			•	•		TO-220, TO-263
/IC39301	ЗA	•									1%	400mV	٠	٠	•	٠	•		TO-220-5, TO-263-5
MIC29500	5A			•				•			1%	370mV	٠			٠	•	٠	TO-220
MIC29501	5A			•				•			1%	370mV	٠	٠	•	٠	•	٠	TO-220-5, TO-263-5
MIC29502	5A									26V	1%	370mV	٠		•	٠	•	٠	TO-220-5, TO-263-5
MIC29503	5A									26V	1%	370mV	٠	٠		٠	•	٠	TO-220-5, TO-263-5
MIC29510	5A			•				•			2%	700mV	٠			٠			TO-220, TO-263
MIC29512	5A									16V	2%	700mV	٠		•	٠			TO-220-5
MIC29710	7.5A			•				٠			2%	700mV	•			٠			TO-220
MIC29712	7.5A									16V	2%	700mV	٠		•	٠			TO-220-5
MIC29750	7.5A			•				٠			1%	425mV	•			٠	•	•	TO-247
MIC29751	7.5A			•				٠			1%	425mV	٠	٠	•	٠	•	•	TO-247-5
MIC29752	7.5A									26V	1%	425mV	٠		•	٠	•	٠	TO-247-5
MIC5156	(2)			•				٠		36V	1%	(2)	٠	٠	•	٠			SOP-8, DIP-8
MIC5157	(2)			(3)					(3)		1%	(2)	•	٠	•				SOP-14, DIP-14
MIC5158	(2)							(4)		(4)	1%	(2)	٠	٠	•				SOP-14, DIP-14
<sup>2</sup> Special orde Output curren Maximum out	t limited by p	ackage an	•	re de	termined b	y the	e choice of	exter	nal N	IOSFE	T.								

and over 30W with a good sink. The chart is approximate, and assumes an ambient temperature of 25°C heat sink. For example, through-hole TO-220 packages can dissipate a bit less than 2W without a heat sink, case" mounting techniques. The maximum point shows power capability with a very good (not infinite, though) Packages are not shown in their approximate relative size The minimum point on each line of Figure 2-3 shows package power dissipation capability using "worst



*Figure 2-3* Maximum Power Dissipation by Package Type

**Designing With LDO Regulators** 

1

### Table 2-2. Typical Thermal Characteristics

Device	$\theta^{C}$	$\theta_{cs}$	"Typical" heat	Equivalent Thermal
201100	JC	CS	$\sin k \theta_{JA}$	Graph (Figures 2-6, 2-7)
MIC5203BM4			250	A
MIC5200BM			160	B
MIC5200BS	15		50	E
MIC5202BM			160	 B
LP2950BZ	_		160 - 180	B
LP2951BM	—	—	160	В
MIC2950BZ	—	_	160 – 180	D
MIC2951BM	—	—	160	D
MIC2951BN	—	—	105	
MIC5205BM5	—		220	С
MIC5206BM5	—	—	220	С
MIC5206BMM MIC5207BM5	—		200 220	C C
MIC5207BM5 MIC5201BM	_	<u> </u>	160	D
MIC5201BS	15		50	E
MIC2954BM			160	L L
MIC2954BS	15		50	
MIC2954BT	3	1	15 - 30	
MIC2954BZ			160 - 180	1
MIC2920ABS	15		50	
MIC2920ABT	3	1	15 - 30	F
MIC29202BU	3	—	30 – 50	F
MIC29203BU	3	_	30 – 50	F
MIC29204BM	_		160	
MIC2937ABT	3	1	15 – 30	G
MIC2937ABU	3	—	30 – 50	G
MIC29371BT	3	1	15 – 30	G
MIC29371BU	3	—	30 – 50	G
MIC29372BT	3	1	15 – 30	G
MIC29372BU	3	—	30 - 50	G
MIC29373BT	3	1	15 – 30	G
MIC29373BU	3		30 - 50	G
MIC2940ABT MIC2940ABU	3	1	15 – 30 30 – 50	Н
MIC2940ABO MIC2941BT	3	1	15 - 30	н
MIC2941BU	2		30 - 50	11
MIC294100 MIC29150BT	2	1	10 - 30	Н
MIC29150BU	2		30 - 40	
MIC29151BT	2	1	10 - 30	Н
MIC29151BU	2		30 - 40	
MIC29152BT	2	1	10 - 30	Н
MIC29152BU	2		30 – 40	
MIC29153BT	2	1	10 – 30	Н
MIC29153BU	2		30 - 40	
MIC29300BT	2	1	10 – 30	
MIC29300BU	2	—	30 – 40	
MIC29301BT	2	1	10 - 30	
MIC29301BU	2		30 - 40	
MIC29302BT	2	1	10 - 30	
MIC29302BU	2		30 - 40	1
MIC29303BT MIC29303BU	2	1	10 – 30 30 – 40	1
MIC29303BU MIC29310BT	2 2	1	<u> </u>	1
MIC29310BT MIC29312BT	2	1	10 - 30	
MIC29512B1 MIC29500BT	2	1	5 – 15	J
MIC29500BU	2		20 - 30	
MIC29501BT	2	1	5 - 15	J
MIC29501BU	2		20 - 30	, · · ·
MIC29502BT	2	1	5 – 15	J
MIC29502BU	2		20 - 30	-
MIC29503BT	2	1	5 – 15	J
MIC29503BU	2	_	20 - 30	
MIC29510BT	2	1	5 – 15	J
MIC29512BT	2	1	5 – 15	J
MIC29710BT	2	1	5 – 15	К
MIC29712BT	2	1	5 – 15	К
MIC29750BWT	1.5	0.5	3 – 9	L
MIC29751BWT	1.5	0.5	3 – 9	
MIC29752BWT	1.5	0.5	3 – 9	L

### Output Current vs. Junction Temperature and Voltage Differential

#### (Figure 2-6)

These graphs show the junction temperature with a given output current and input-output voltage differential. Ambient temperature is 25°C. The thermal resistance used for the calculations is shown under each graph. This resistance assumes that a heat sink of suitable size for the particular regulator is employed; higher current regulator circuits generally require larger heat sinks. Refer to *Thermal Management*, in **Section 3**, for definitions and details.

For example, a MIC5203-3.3BM4, supplying 50mA and with 6.3V on its input ( $V_{IN} - V_{OUT} = 3V$ ), will have a junction temperature of approximately 63° (Figure 2-6 (A)).

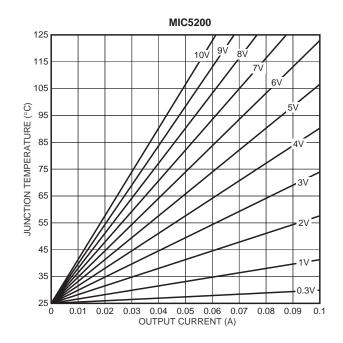


Figure 2-6 (B). SO-8 with  $\theta_{JA} = 160^{\circ}C/W$ 

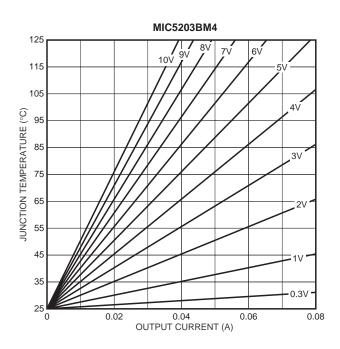


Figure 2-6 (A). SOT-143 with  $\theta_{,JA} = 250^{\circ}C/W$ 

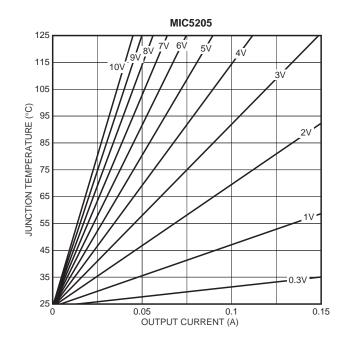


Figure 2-6 (C). SOT-23-5 with  $\theta_{JA} = 220^{\circ}C/W$ 

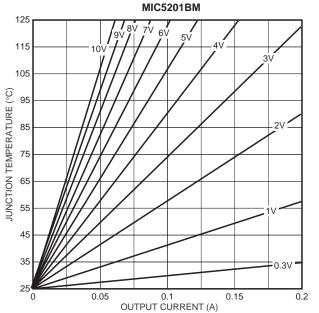


Figure 2-6 (D). High Current SO-8 with  $\theta_{JA} = 160^{\circ}C/W$ 

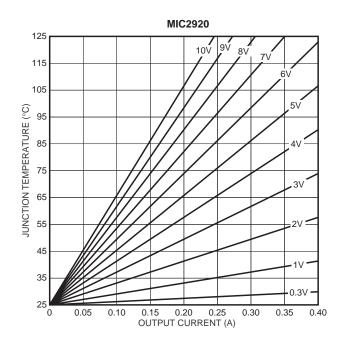


Figure 2-6 (F). TO-263 with  $\theta_{_{JA}} = 40^{\circ}C/W$ 

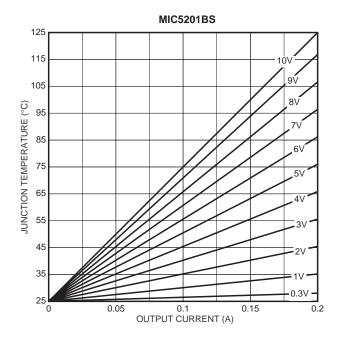


Figure 2-6 (E). SOT-223 with  $\theta_{\rm JA}$  = 50°C/W

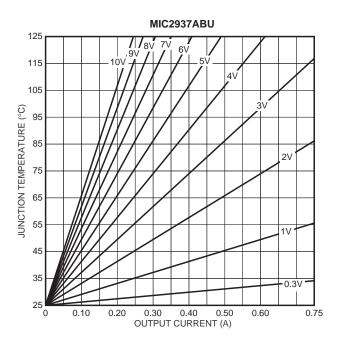


Figure 2-6 (G). TO-263 with  $\theta_{JA} = 40^{\circ}C/W$ 

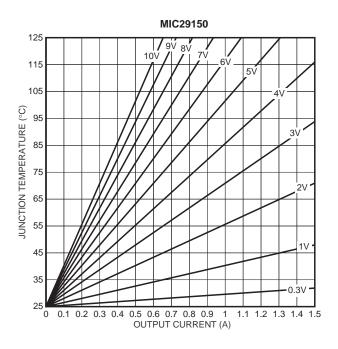


Figure 2-6 (H). TO-220 with  $\theta_{JA} = 15^{\circ}C/W$ 

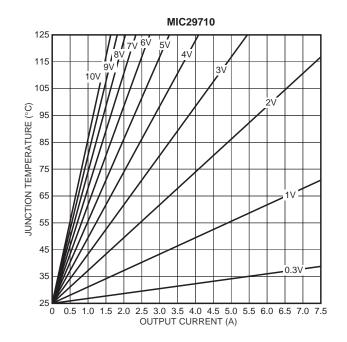


Figure 2-6 (K). TO-220 with 
$$\theta_{JA} = 6^{\circ}C/W$$

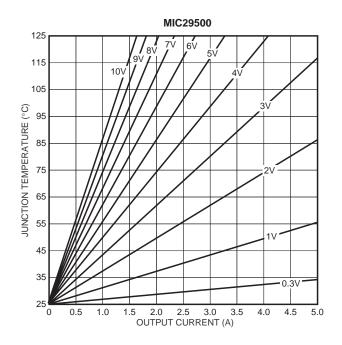


Figure 2-6 (J). TO-220 with  $\theta_{_{J\!A}} = 6^\circ C/W$ 

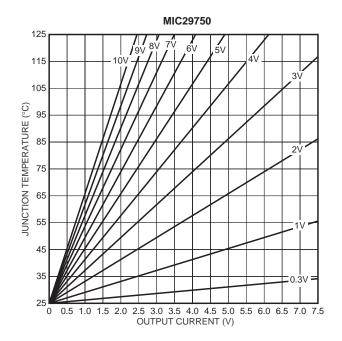


Figure 2-6 (L). TO-247 with  $\theta_{_{JA}} = 4^{\circ}C/W$ 

### Junction Temperature Rise vs. Available Output Current and Differential Voltage

#### (*Figure 2-7*)

These graphs show the available thermally-limited steady-state output current with a given thermal resistance and input—output voltage differential. The assumed  $\theta_{JA}$  (thermal resistance from junction to ambient) is shown below each graph. Refer to *Thermal Management* in **Section 3** for definitions and details.

For example, Figure 2-7 (C) shows that the MIC5205BM5, with 3V across it ( $V_{IN} = V_{OUT} + 3V$ ) and supplying 120mA, will have a temperature rise of 80°C (when mounted normally).

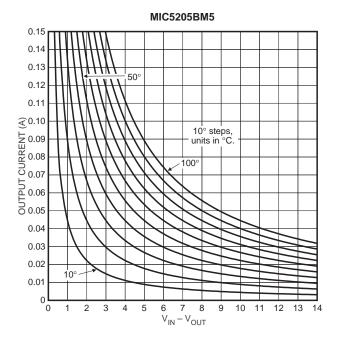


Figure 2-7 (C). SOT-23-5 with  $\theta_{JA} = 220^{\circ}C/W$ 

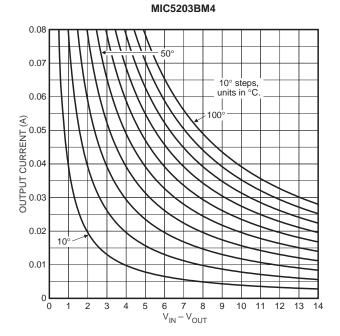


Figure 2-7 (A). SOT-143 with  $\theta_{,JA} = 250^{\circ}C/W$ 

0.20 0.18 0.16 0.14 E 50 10° steps, units in °C 00 0.06 0.04 0.02 10 0 L 2 4 6 8 10 12 14 16 18 20 22 24 V<sub>IN</sub> - V<sub>OUT</sub>

MIC5201BM

Figure 2-7 (D). SO-8 with  $\theta_{JA} = 140^{\circ}C/W$ 



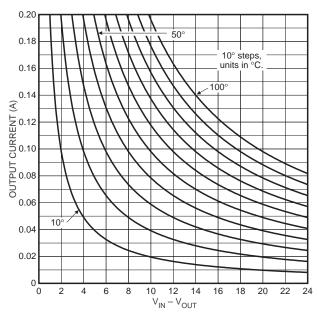


Figure 2-7 (E). SOT-223 with  $\theta_{JA} = 50^{\circ}C/W$ 

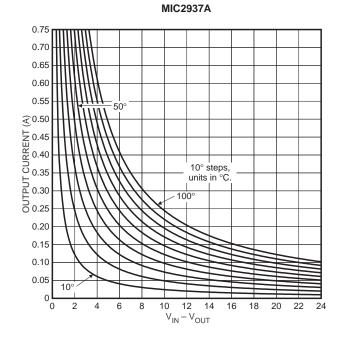


Figure 2-7 (G). TO-263 with  $\theta_{JA} = 40^{\circ}C/W$ 

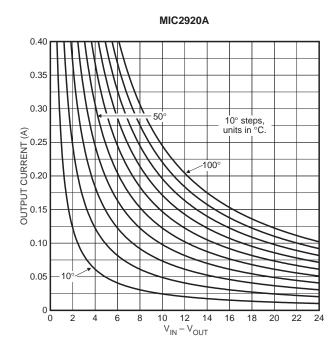


Figure 2-7 (F). TO-263 with  $\theta_{JA} = 40^{\circ}C/W$ 

1.5 1.4 1.3 1.2 1.1 50 €1.0 10° steps, units in °C. 100<sup>°</sup> 0.4 0.3 0.2 10°. 0.1 0 L 2 4 6 8 10 12 14 16 18 20 22 24 V<sub>IN</sub> - V<sub>OUT</sub>

Figure 2-7 (H). TO-220 with  $\theta_{JA} = 15^{\circ}C/W$ 

MIC29150



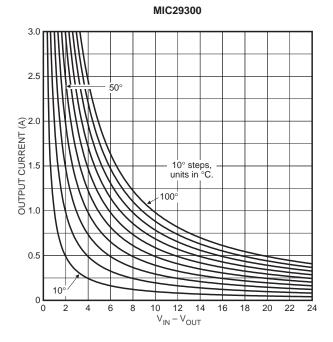


Figure 2-7 (I). TO-220 with  $\theta_{JA} = 10^{\circ}C/W$ 

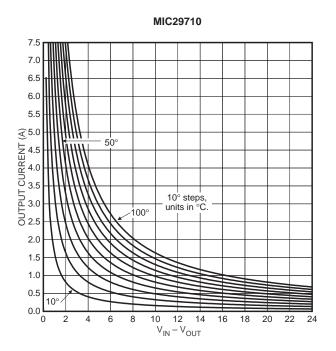


Figure 2-7 (K). TO-220 with 
$$\theta_{JA} = 6^{\circ}C/W$$

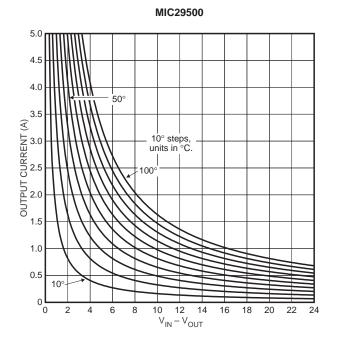


Figure 2-7 (J). TO-220 with  $\theta_{JA} = 6^{\circ}C/W$ 

7.5 7.0 6.5 6.0 5.5 50° €5.0 4.5 4.0 3.5 3.0 2.5 10° steps, units in °C ·100° 2.0 1.5 1.0 10° 0.5 0.0 L 2 4 6 8 10 12 14 16 18 20 22 24 V<sub>IN</sub> - V<sub>OUT</sub>

Figure 2-7 (L). TO-247 with  $\theta_{JA} = 4^{\circ}C/W$ 

MIC29750

### Section 3. Using LDO Linear Regulators

### General Layout and Construction Considerations

#### Layout

Although often considered "just a D.C. Circuit", low-dropout linear regulators are actually built with moderately high frequency transistors because rapid response to input voltage or output current changes demand excellent high frequency performance. These characteristics place some requirements on bypass capacitors and board layout.

#### **Bypass Capacitors**

Low-dropout linear regulators need capacitors on both their input and output. The input capacitor provides bypassing of the internal op amp used in the voltage regulation loop. The output capacitor improves regulator response to sudden load changes, and in the case of the Super  $\beta$ eta PNP<sup>TM</sup> devices, provides loop compensation that allows stable operation.

The input capacitor for monolithic regulators should feature low inductance and generally good high frequency performance. Capacitance is not too critical except for systems where excessive input ripple voltage is present. The capacitor must, as a minimum, maintain the input voltage minimum value above the dropout point. Otherwise, the regulator ceases regulation and becomes merely a saturated switch. In an AC-line powered system, where the regulator is mounted within a few centimeters from the main filter capacitor, additional capacitors are often unnecessary. A  $0.1\mu$ F ceramic directly adjacent to the regulator is farther away from the filter capacitor, local bypassing is mandatory.

With the high current MIC5157 and MIC5158 Super LDO<sup>TM</sup> regulator controllers, the input capacitor should be a medium sized ( $10\mu$ F or larger) low ESR (effective series resistance) type.

#### **Output Capacitor**

The Super βeta PNP regulators require a certain minimum value of output capacitance for operation—below this minimum value, the output may exhibit oscillation. The output capacitor is inside the voltage control loop and is necessary for loop stabilization. Minimum recommended values are listed on each device data sheet. There is *no* maximum value the output capacitor may be increased without limit.<sup>1</sup>

Excellent response to high frequency load changes (load current transient recovery) demands low inductance, low ESR, high frequency filter capacitors. Stringent requirements are solved by paralleling multiple medium sized capacitors. Capacitors should be chosen by comparing their lead inductance, ESR, and dissipation factor. Multiple small or medium sized capacitors provide better high frequency characteristics than a single capacitor of the same total capacity since the lead inductance and ESR of the multiple capacitors is reduced by paralleling.

Although the capacitance value of the filter may be increased without limit, if the ESR of the paralleled capacitors drops below a certain (device family dependent) threshold, a zero in the transfer plot appears, lowering phase margin and decreasing stability. With some devices, especially the MIC5157 and MIC5158 Super LDO, this problem is solved by using a low ESR input decoupling capacitor. Worst-case situations may require changes to higher ESR output capacitors—perhaps increasing both the ESR and the capacitance by using a different chemistry—or, as a last resort, by adding a small series resistance ( < 1 $\Omega$ ) between the regulator and the capacitor(s).

NOTE 1: Truly huge output capacitors will extend the start-up time, since the regulator must charge them. This time is determined by capacitor value and the current limit value of the regulator.

#### **Circuit Board Layout**

Stray capacitance and inductance may upset loop compensation and promote instability. Excessive input lead resistance increases the dropout voltage, and excessive output lead resistance reduces output load regulation. Ground loops also cause both problems. Careful layout is the solution.

Reduce stray capacitance and inductance by placing bypass and filter capacitors close to the regulator. Swamp parasitic reactances by using a  $0.1\mu$ F ceramic capacitor (or equivalent) in parallel with the regulator input filter capacitor. Designers of battery-powered circuits often overlook the finite high-frequency impedance of their cells. The ceramic capacitor solves many unexpected problems.

Excessive lead resistance, causing unwanted voltage drops and ruining load regulation, is solved by merely increasing conductor size. Regulators with remote sensing capability—like all Micrel adjustables—may utilize a Kelvin-sense connection directly to the load. As Figure 3-1 shows, an additional pair of wires feeds back the load voltage to the regulator sense input.<sup>2</sup> This lets the regulator compensate for line drop. As the Kelvin sense leads carry only the small voltage-programming resistor current, they may be very narrow traces or small diameter wire. A judicious layout is especially important in remote-sensed designs, since these long, high impedance leads are susceptible to noise pickup.

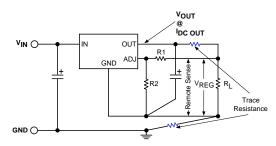


Figure 3-1. Remote Voltage Sense (Kelvin) Connections

A common ground loop problem occurs when rectifier ripple current flows through the regulator's

ground lead on its way to the filter capacitor (see Figure 3-2). The ripple current, which is several times larger than the average DC current, may create a voltage drop in the ground line, raising its voltage relative to the load. As the regulator attempts to compensate, load regulation suffers. Solve the problem by ensuring rectifier current flows directly into the filter capacitor.

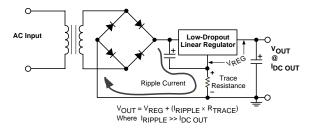


Figure 3-2. Ground Loop and Ripple Currents Degrade Output Accuracy

Figure 3-3 shows an ideal layout for remotesensed loads. If a single point ground is not practical, load regulation is improved by employing a large ground plane.

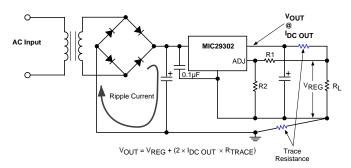


Figure 3-3. Regulator Layout With Remote Voltage Sensing

#### Assembly

Low power regulator circuits are built like any other analog system. Surface mounted systems are assembled using normal reflow (or similar), techniques. Larger leaded packages may require special lead bending before installation; specific lead bend options are available from Micrel, or the assembler may bend them. When power demands force the use of a heat sink, extra care must be applied during assembly and soldering. Our assembly discussion will focus on the popular TO-220 package but it is generally applicable to other package types.

NOTE 2: The internal reference in most Micrel regulators is positioned between the adjust pin and ground, unlike the older "classic" NPN regulator designs. This technique, while providing excellent performance with Micrel regulators, does not work with the older voltage regulators; in fact, it reduces their output voltage accuracy.

#### Lead Bending

If lead bending is necessary, use the standard bend options offered by Micrel whenever possible. These bending operations are performed on tooling developed specifically for this purpose and with the safety of the package, die, and internal wire bonds in mind. Custom lead bending is also available for a nominal charge.

For prototyping or other low quantity custom lead bending requirements, clamp the leads at the junction of the case with long nosed pliers. Using your fingers or another pair of pliers, bend the outer lead as desired. Please observe the following cautions:

- Do not spread or compress the leads
- Do not bend or twist the leads at the body junction: start the bend at least 3mm from the body
- Maintain a lead bend radius of approximately 1mm
- Do not re-bend leads multiple times

Micrel TO-220 packages are made from nickelplated or tinned copper for best electrical and thermal performance. While rugged electrically, they are susceptible to mechanical stress and fatigue. Please handle them with care!

#### **Heat Sink Attachment**

TO-220 package applications at moderate (room) temperatures may not require heat sinking if the power dissipation is less than 2 watts. Otherwise, heat sinks are necessary. Use the minimum practical lead length so heat may travel more directly to the board, and use the board itself as a heat sink.

Attachment techniques vary depending upon the heat sink type, which in turn depends upon the power dissipated. The first consideration is whether or not electrical isolation is required. Micrel's Super ßeta PNP regulators all have a grounded tab, which usually means no insulation is necessary. This helps by reducing or eliminating one of the thermal resistances. Next, we determine heat sink size. See the *Thermal Management* chapter for details. If a standard commercial heat sink is chosen, we may generally assume minimal surface roughness or burrs.

Otherwise, machining the mounting pad may be necessary to achieve a flatness (peak-to-valley) of 4

mils per inch with a surface finish of  $\pm$  1.5µm or better for minimum thermal resistance.

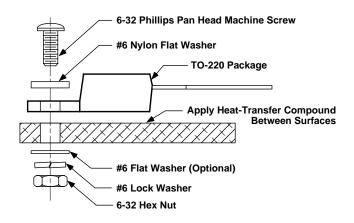
Holes for the mounting screw should be drilled and deburred. Slightly oversized holes allow for slippage during temperature cycling and is generally recommended.

Heat sinks of bare aluminum or copper are not optimum heat radiators. Anodizing or painting improves heat radiation capability. For more details on heat sinks, see the *References*.

Thermal grease, thermal pads, or other thermally conductive interface between the package and the heat sink compensates for surface flatness errors, mounting torque reduction over time, air gaps, and other sins, and is recommended. Heat sink manufacturers offer a variety of solutions with widely varying prices, installation ease, and effectiveness.

Many heat sinks are available with mounting clips. These allow fast assembly and, when the clip also presses against the plastic body instead of only the metal tab, provide excellent heat contact area and low thermal resistance.

Machine screws are often used for heat sink attachment (see Figure 3-4). Proper torque is imperative; too loose and the thermal interface resistance is excessive; too tight and the semiconductor die will crack. The 0.68N-m specification applies to clean threads; ensure that the thermal grease does not interfere with the threads.



Maximum Torque: 0.68 N-m (6 in-lbs) (Caution: Excessive torque may crack semiconductor)



### Output Voltage Accuracy

#### Adjustable Regulator Accuracy Analysis

Micrel LDO Regulators are high accuracy devices with output voltages factory-trimmed to much better than 1% accuracy. Across the operating temperature, input voltage, and load current ranges, their worst-case accuracies are still better than  $\pm 2\%$ . For adjustable regulators, the output also depends upon the accuracy of two programming resistors. Some systems require supply voltage accuracies better than  $\pm 2.5\%$ —including noise and transients. While noise is generally not a major contributor to output inaccuracy, load transients caused by rapidly varying loads (such as high-speed microprocessors), are significant, even when using fast transient-response LDO regulators and high-quality filter capacitors.

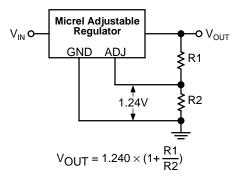


Figure 3-5. An adjustable linear regulator uses the ratio of two resistors to determine its output voltage.

Adjustable regulators use the ratio of two resistors to multiply the reference voltage to produce the desired output voltage (see Figure 3-5). The formula for output voltage from two resistors is presented as Equation 3-1.

$$(3-1) \quad V_{OUT} = V_{REF} \left( 1 + \frac{R1}{R2} \right)$$

The basic MIC29512 has a production-trimmed reference (V<sub>REF</sub>) with better than ±1% accuracy at a fixed temperature of 25°C. It is guaranteed better than ±2% over the full operating temperature range, input voltage variations, and load current changes. Since practical circuits experience large temperature swings we should use the ±2% specification as our theoretical worst-case. This value assumes no error contribution from the programming resistors.

Referring to Figure 3-5 and Equation 3-1, we see that resistor tolerance (tol) must be added to the

reference tolerance to determine the total regulator inaccuracy. A sensitivity analysis of this equation shows that the error contribution of the adjust resistors is:

(3-2) 
$$\underset{\text{Contribution}}{\text{Error}} \% = \left(\frac{2 \times \text{tol}\%}{1 - \left(\frac{\text{tol}\%}{100}\right)}\right) \times \left(1 - \frac{\text{V}_{\text{REF}}}{\text{V}_{\text{OUT}}}\right)$$

Since the output voltage is proportional to the product of the reference voltage and the ratio of the programming resistors, at high output voltage, the error contribution of the programming resistors is the sum of each resistor's tolerance. Two standard ±1% resistors contribute as much as 2% to output voltage error. At lower voltages, the error is less significant. Figure 3-6 shows the effects of resistor tolerance on regulator accuracy from the minimum output voltage (V<sub>RFF</sub>) to 12V. At the minimum V<sub>OUT</sub>, theoretical resistor tolerance has no effect on output accuracy. Resistor error increases proportionally with output voltage: at an output of 2.5V, the sensitivity factor is 0.5; at 5V it is about 0.75; and at 12V it is over 0.9. This means that with 5V of output, the error contribution of 1% resistors is 0.75 times the sum of the tolerances, or  $0.75 \times 2\% = 1.5\%$ . As expected, more precise resistors offer more accurate performance.

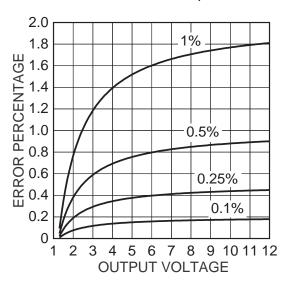


Figure 3-6. Resistor Tolerance Effects on Adjustable Regulator Accuracy

The output voltage error of the entire regulator system is the sum of reference tolerance and the resistor error contribution. Figure 3-7 shows this worstcase tolerance for the MIC29512 as the output volt-

age varies from minimum to 12V using  $\pm 1\%$ ,  $\pm 0.5\%$ ,  $\pm 0.25\%$ , and  $\pm 0.1\%$  resistors. The more expensive, tighter accuracy resistors provide improved tolerance, but it is still limited by the adjustable regulator's  $\pm 2\%$  internal reference.

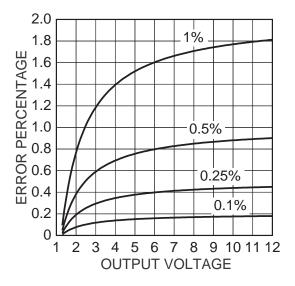


Figure 3-7. Worst-Case Output Tolerance

A better method is possible: increase the overall accuracy of the regulator by employing a precision reference in the feedback loop.

#### Improving Regulator Accuracy

Achieving a worst-case error of ±2.5%, including all D/C and A/C error terms, is possible by increasing the basic accuracy of the regulator itself, but this is expensive since high current regulators have significant self-heating. Its internal reference must maintain accuracy across a wide temperature range. Testing for this level of performance is time consuming and raises the cost of the regulator, which is unacceptable for extremely price-sensitive marketplaces. Some systems require better than ±2% accuracy. This high degree of accuracy is possible using Micrel's LM4041 voltage reference instead of one of the programming resistors (refer to Figure 3-8). The regulator output voltage is the sum of the internal reference and the LM4041's programmed voltage (Equation 3-3).

(3-3) 
$$V_{OUT} = V_{REF} \text{ Regulator} + V_{LM4041}$$
  
= 1.240 +  $V_{LM4041}$ 

The benefit of this circuit is the increased accuracy possible by eliminating the multiplicative effect

#### Designing With LDO Regulators

of the regulator's internal reference. In normal configurations, the reference error is multiplied up by the resistor ratio, keeping the error percentage constant. With this circuit, the error voltage is within 25mV, absolute. Another benefit of this arrangement is that the LM4041 is not a dissipative device: there is only a small internal temperature rise to degrade accuracy. Additionally, both references are operating in their lowsensitivity range so we get less error contribution from the resistors. A drawback of this configuration is that the minimum output voltage is now the sum of both references, or about 2.5V. The adjustable LM4041 is available in accuracies of  $\pm 0.5\%$  and  $\pm 1\%$ , which allows better overall system output voltage accuracy.

Equation 3-4 presents the formula for the LM4041-ADJ output voltage. Note the output voltage has a slight effect on the reference. Refer to the LM4040 data sheet for full details regarding this second-order coefficient.

(3-4) 
$$V_{LM4041} = \left[V_{OUT} \times \frac{\Delta V_{REF}}{\Delta V_{OUT}} + 1.233\right] \times \left[\frac{R1b}{R1a} + 1\right]$$

Actually, the voltage drop across R1b is slightly higher than that calculated from Equation 3-4. Approximately 60nA of current flows out of the LM4041 FB terminal. With large values of R1b, this current creates millivolts of higher output voltage; for best accuracy, compensate R1b by reducing its size accordingly. This error is +1mV with R1b =  $16.5k\Omega$ .

Equation 3-5 shows the nominal output voltage for the composite regulator of Figure 4.

(3-5)

(

$$V_{OUT} = \frac{1.233 \left(\frac{R1b}{R1a} + 1\right)}{1.0013 \left(\frac{0.0013R1b}{R1a}\right)} + (60nA \times R1b) + 1.240$$

Note that the tolerance of R2 has no effect on output voltage accuracy. It sets the diode reverse (operating) current and also allows the divider current from R1a and R1b to pass. With R2 =  $1.2k\Omega$ , 1mA of bias flows. If R2 is too small (less than about  $105\Omega$ , the maximum reverse current of the LM4041-ADJ is exceeded. If it is too large with respect to R1a and R1b then the circuit will not regulate. The recommended range for R2 is from  $121\Omega$  to R1a/10.

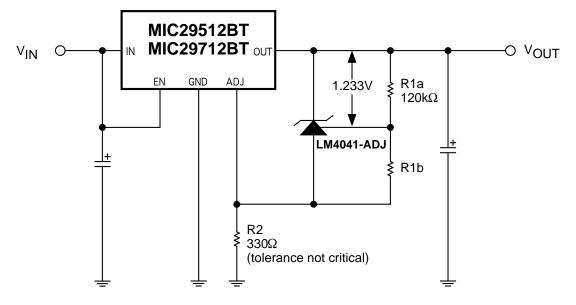
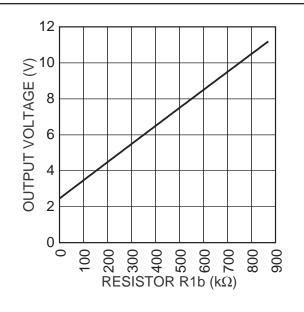


Figure 3-8. Improved Accuracy Composite Regulator Circuit





#### Regulator & Reference Circuit Performance

With this circuit we achieve much improved accuracies. Our error terms are:

25mV	(constant) from the MIC29512
0.5%	from the LM4041C
+ 0 to 2%	from R1a and R1b
0.5% + 25mV to 2.5% + 25mV	Total Error Budget

Figure 3-10 shows the resistor error contribution to the LM4041C reference output voltage tolerance. Figure 3-11 shows the worst-case output voltage error of the composite regulator circuit using various resistor tolerances, when a 0.5% LM4041C reference is employed. The top four traces reflect use of 1%, 0.5%, 0.25%, and 0.1% resistors. Table 3-1 lists the production accuracy obtained with the lowcost LM4041C and standard 1% resistors as well as the improvement possible with 0.1% resistors.

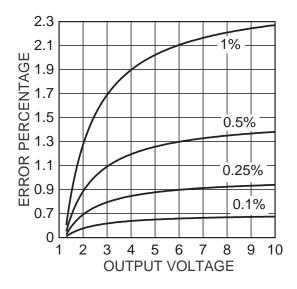


Figure 3-10. Resistor Tolerance Effects on LM4041 Voltage Reference Accuracy

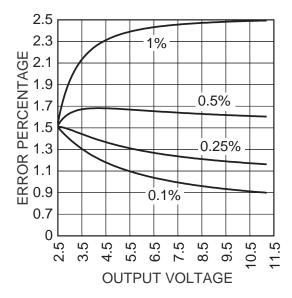


Figure 3-11. Composite Regulator Accuracy

What does the extra complexity of the composite regulator circuit of Figure 3-8 buy us in terms of extra accuracy? With precision components, we may achieve tolerances better than  $\pm 1\%$  with the composite regulator, as compared to a theoretical best case of somewhat worse than 2% with the standard regulator and resistor configuration. Figure 3-12 and Table

V <sub>OUT</sub>	1% Resistors	0.1% Resistors
2.50V	±1.54%	±1.50%
2.90V	±1.88%	±1.41%
3.00V	±1.94%	±1.39%
3.30V	±2.07%	±1.34%
3.45V	±2.12%	±1.31%
3.525V	±2.14%	±1.30%
3.60V	±2.16%	±1.29%
5.00V	±2.36%	±1.13%
6.00V	±2.41%	±1.07%
8.00V	±2.46%	±0.98%
10.00V	±2.49%	±0.92%
11.00V	±2.49%	±0.90%

Table 3-1. Worst-Case Output Voltage Error forTypical Operating Voltages Using the LM4040C(±0.5% Accuracy Version)

#### Designing With LDO Regulators

3-2 show the accuracy difference between the circuits as the output voltage changes. The accuracy difference is the tolerance of the two-resistor circuit minus the tolerance of the composite circuit. Both tolerances are the calculated worst-case value, using 1% resistors. This figure shows the composite circuit is always at least 1% better than the standard configuration. Both the figure and the table assume standard ±1% resistors and the LM4041C-ADJ (0.5%) reference.

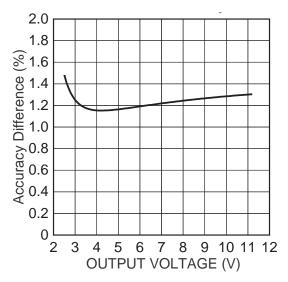


Figure 3-12. Accuracy difference between the Standard Two-Resistor Circuit and the Composite Circuit of Figure 3-8

V <sub>OUT</sub>	Composite Circuit	Standard Circuit
2.50V	±1.6%	±3.0%
3.00V	±1.9%	±3.2%
3.30V	±2.1%	±3.3%
3.50V	±2.1%	±3.2%
5.00V	±2.4%	±3.5%
6.00V	±2.4%	±3.6%
8.00V	±2.5%	±3.7%
10.00V	±2.5%	±3.8%
11.00V	±2.5%	±3.8%

Table 3-2. Comparing the Worst-Case Output Voltage Error for the Two Topologies With Typical Output Voltages

### Design Issues and General Applications

#### Noise and Noise Reduction

Most of the output noise caused by a LDO regulator emanates from the voltage reference. While some of this noise may be shunted to ground by the output filter capacitor, bypassing the reference at a high impedance node provides more attenuation for a given capacitor value. The MIC5205 and MIC5206 use a lower noise bandgap reference and also provide external access to this reference. A small value (470pF or so) external capacitor attenuates output noise by about 10dB for a 5 volt output.

All of Micrel's adjustable regulators allow a similar technique. By shunting one of the voltage programming resistors with a small-value capacitor, the high frequency gain of the regulator is reduced which serves to reduce high frequency noise. The capacitor should be placed across the resistor connecting between the feedback pin and the output (R1 on data sheet schematics).

#### Stability

Low dropout linear regulators with a PNP output require an output capacitor for stable operation. See *Stability Issues* in **Section 4, Linear Regulator Solutions** for a discussion on stability with Super  $\beta$ eta PNP regulators.

The Super LDO is more stable than the monolithic devices and rarely needs much attention to guarantee stability. *Micrel's Unique "Super LDO"*, also in Section 4, discusses the few parameters requiring vigilance.

#### LDO Efficiency

The electrical efficiency of all electronic devices is defined as  $\mathsf{P}_{OUT} \div \mathsf{P}_{IN}.$  A close efficiency approximation for linear regulators is

$$Eff = \frac{V_{OUT}}{V_{IN}}$$

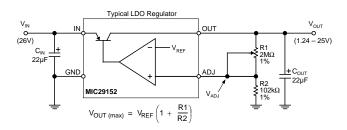
This approximation neglects regulator operating current, but is very accurate (usually within 1%) for Super  $\beta$ eta PNP and Super LDO regulators with their

very low housekeeping power draw. The full formula is:

$$\mathsf{Eff} = \frac{\mathsf{V}_{\mathsf{IN}} \times (\mathsf{I}_{\mathsf{GND}}) + (\mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}}) \times \mathsf{I}_{\mathsf{OUT}}}{\mathsf{V}_{\mathsf{OUT}} \times \mathsf{I}_{\mathsf{OUT}}}$$

### Building an Adjustable Regulator Allowing 0V Output

Some power supplies, especially laboratory power supplies and power systems demanding wellcontrolled surge-free start-up characteristics, require a zero-volt output capability. In other words, an adjustable laboratory power supply should provide a range than includes 0V. However, as shown in Figure 3-13, a typical adjustable regulator does not facilitate adjustment to voltages lower than VRFF (the internal bandgap voltage). Adjustable regulator ICs are designed for output voltages ranging from their reference voltage to their maximum input voltage (minus dropout); the reference voltage is generally about 1.2V. The lowest output voltage available from this circuit is provided when  $R1 = 0\Omega$ . For the MIC29152 LDO regulator,  $V_{REF} = 1.240V$ , so  $V_{OUT}(min) = V_{REF}(1+R1/R2), \text{ or } 1.240V.$ 



#### Figure 3-13. Typical Adjustable Regulator

Two designs work around the minimum output voltage limitation. The first uses a low-cost reference diode to create a "virtual"  $V_{OUT}$  that cancels the reference. The second uses op-amps to convince the regulator adjust pin that zero volts is a proper output level. In both cases, the feedback-loop summing junction must be biased at  $V_{REF}$  to provide linear operation.

#### Reference Generates a "Virtual V<sub>OUT</sub>"

Figure 3-14 shows a simple method of achieving a variable output laboratory supply or a less-than-1.2V fixed-output supply. The circuit uses a second bandgap reference to translate the regulator's output up to a "virtual  $V_{OUT}$ " and then uses that virtual  $V_{OUT}$  as the top of a feedback divider. The output voltage adjusts from 0V to about 20V.

When R1 goes to  $0\Omega$ , the output is about 0V, the virtual V<sub>OUT</sub> is one bandgap voltage above ground, and the adjust input is also one bandgap voltage above ground. The regulator's error amplifier loop is satisfied that both of its inputs are at one bandgap voltage and it keeps the output voltage constant at 0V. The virtual V<sub>OUT</sub> tracks any increases in R1, remaining one bandgap voltage above the actual V<sub>OUT</sub>, as the output rises from ground. The maximum possible V<sub>OUT</sub> equals the regulator's maximum input voltage minus the approximately 2V housekeeping voltage required by the current-source FET and the external bandgap reference.

The current source, composed of a 2N3687 JFET and R3, is designed for about  $77\mu$ A. Seven microamperes for the resistor string (about 100 times the nominal 60nA input current of the regulator's adjust input) and  $70\mu$ A for the bandgap. R2 is optional, and is needed only if no load is present. It bleeds off the  $70\mu$ A of reference current and satisfies the minimum load current requirement of the regulator.

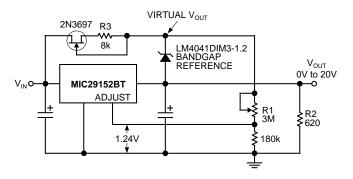


Figure 3-14. Adjust to Zero Volt Circuit Using a Reference Diode

A drawback of this simple design is that the voltage of the internal reference in the regulator must match the external (LM4041) voltage for the output to actually reach zero volts. In practice, the minimum output voltage from this simple circuit is a few millivolts.

#### **Op-Amp Drives Ground Reference**

The circuit of Figure 3-15 provides adjustability down to 0V by controlling the ground reference of the feedback divider. It uses the regulator's internal bandgap reference to provide both accuracy and economy. Non-inverting amplifier A2 senses  $V_{REF}$ (via  $V_{ADJ}$ ) and provides a gain of just slightly more than unity. When R5 is adjusted to supply ground to voltage follower A1 then ground is also applied to the

#### Designing With LDO Regulators

bottom of feedback voltage divider R1 and R2, and operation is identical to the standard adjustable regulator configuration, shown in Figure 3-13 (when adjusted to provide maximum output voltage). Conversely, when R5 is adjusted so the input to voltage follower A1 is taken directly from the output of amplifier A2 the bottom of voltage divider R1 and R2 is biased such that  $V_{ADJ}$  will equal  $V_{REF}$  when  $V_{OUT}$  is 0V. Rotation of R5 results in a smooth variation of output voltage from 0V to the upper design value, which is determined by R1 and R2.

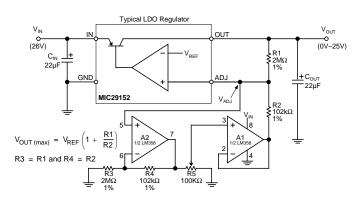


Figure 3-15. 0V-to-25V Adjustable Regulator

The gain of amplifier A2 is 1 + R4 / R3 = 1.05, in this example. Note that the portion of gain above unity is the reciprocal of the attenuation ratio afforded by feedback divider R1 and R2; i.e., R4 / R3 = 1 / (R1 / R2) To provide optimal ratio matching, resistors R3 and R4 have been chosen to be the same values and types as their counterparts R1 and R2, respectively.

#### Systems With Negative Supplies

A common start-up difficulty occurs if a regulator output is pulled below ground. This is possible in systems with negative power supplies. An easy fix is shown in Figure 3-16: adding a power diode, such as a 1N4001, from the regulator output to ground (with its anode to ground). This clamps the worst-case regulator output pin voltage to 0.6V or 0.7V and prevents start-up problems.

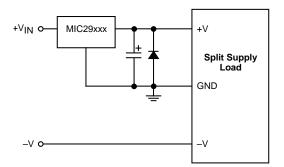


Figure 3-16. Diode Clamp Allows Start-Up in Split-Supply System

#### High Input Voltages

If the input voltage ranges above the maximum allowed by the regulator, a simple preregulator circuit may be employed, as shown in Figure 3-17. A preregulator is a crude regulator which drops extra voltage from the source to a value somewhat lower than the maximum input allowed by the regulator. It also helps thermal design by distributing the power dissipation between elements. The preregulator need not have good accuracy or transient response, since these parameters will be "cleaned up" by the final regulator.

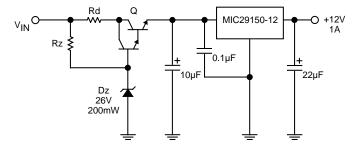


Figure 3-17. Preregulator Allows High Input Supply

Figure 3-17 shows the generic circuit. Table 3-3 provides component values for a typical application: +12V output at 1A. With up to 40V of input, no Rd is required. Above 40V, heat sinking is eased by power sharing with Rd. Note that a minimum input voltage is also listed; the composite regulator enters dropout below this minimum value. Assumptions made include a Q1 beta of 1000 and zener diode dissipation of 200mW. The MIC29150 dissipates a maximum of 13W; Q1 generates less than 15W of heat.

V <sub>MAX</sub>	V <sub>MIN</sub>	Rz	Rd
30V	15V	1.1kΩ	0
40V	17.5V	3.6kΩ	0
50V	23V	6.2kΩ	10Ω
60V	34V	8.87kΩ	20Ω

Table 3-3. Component Values for Figure 3-17

#### Controlling Voltage Regulator Turn-On Surges

When a power supply is initially activated, inrush current flows into the filter capacitors. The size of this inrush surge is dependent upon the size of the capacitors and the slew rate of the initial power-on ramp. Since this ramp plays havoc with the upstream power source, it should be minimized. Employing the minimum amount of capacitance is one method, but this technique does not solve the general problem. Slew rate limiting the power supply is a good solution to the general problem.

The turn-on time interval of a voltage regulator is essentially determined by the bandwidth of the regulator, its maximum output current (in current limit), and the load capacitance. To some extent, the rise time of the applied input voltage (which is normally quite short, tens of milliseconds, or less) also affects the turn-on time. However, the regulator output voltage typically steps abruptly at turn-on. Increasing the turn-on interval via some form of slew-limiting decreases the surge current seen by both the regulator and the system. These applications describe circuitry that changes the step-function to a smoother RC charge waveform.

Various performance differences exist between the three circuits that are presented. These are:

- (1) whether stability is impacted
- (2) whether start-up output voltage is 0V
- (3) whether the circuit quickly recovers from a momentarily interrupted input voltage or a shorted output.

Table 3-4 summarizes each circuit's features.

Circuit Figure	Stability Impacted?	Start-Up Pedestal?	V <sub>IN</sub> Interrupt Recovery?	V <sub>OUT</sub> Short Recovery?
3-18	yes	1.2V	no	no
3-20	no	1.8V	no	yes
3-22	no	0V	yes	no

Table 3-4. Slow Turn-On Circuit Performance Features

#### The Simplest Approach

Figure 3-18 illustrates a typical LDO voltage regulator, the MIC29152, with an additional capacitor ( $C_T$ ) in parallel with the series leg (R1) of the feedback voltage divider. Since the voltage ( $V_{ADJ}$ ) will be maintained at  $V_{REF}$  by the regulator loop, the output of this circuit will still rapidly step to  $V_{REF}$  (and then rise slowly). Since  $V_{REF}$  is usually only about 1.2V, this eliminates a large part of the surge current.

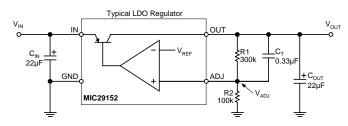


Figure 3-18. Simplest Slow Turn-On Circuit

As C<sub>T</sub> charges, the regulator output (V<sub>OUT</sub>) asymptotically approaches the desired value. If a turnon time of 300 milliseconds is desired then about three time constants should be allowed for charge time: 3t = 0.3s, or t = 0.1s = R1 × C<sub>T</sub> =  $300k\Omega \times 0.33\mu$ F.

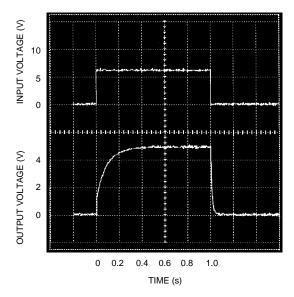


Figure 3-19. Turn-On Behavior for Circuit of Figure 3-18

Figure 3-19 shows the waveforms of the circuit of Figure 3-18. This circuit has three shortcomings: (1) the approximately 1.2V step at turn-on, (2) the addition of capacitor  $C_T$  places a zero in the closed-loop transfer function (which affects frequency and transient responses and can potentially cause stability problems) and (3) the recovery time associated with a momentarily short-circuited output may be unacceptably long<sup>3</sup>.

#### Improving the Simple Approach

Figure 3-20 addresses the problems of potential instability and recovery time. Diode D1 is added to the circuit to decouple the (charged) capacitor from the feedback network, thereby eliminating the effect of  $C_T$  on the closed-loop transfer function. Because of the non-linear effect of D1 being in series with  $C_T$ , there is a slightly longer "tail" associated with approaching the final output voltage at turn-on. In the event of a momentarily shorted output, diode D2 provides a low-impedance discharge path for  $C_T$  and thus assures the desired turn-on behavior.

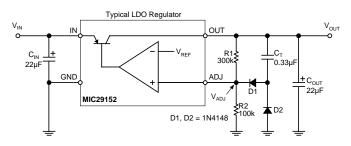


Figure 3-20. Improved Slow Turn-On Circuit

Figure 3-21 shows the waveforms of the circuit of Figure 3-20. Note that the initial step-function output is now 0.6V higher than with the circuit of Figure 3-18. This (approximately) 1.8V turn-on pedestal may

NOTE 3: This is because when the output is shorted,  $C_T$  is discharged only by R2; if the short is removed before  $C_T$  is fully discharged the regulator output will not exhibit the desired turn-on behavior.

be objectionable, especially in applications where the desired final output voltage is relatively low.

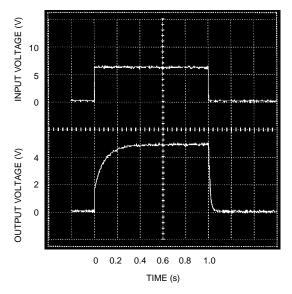


Figure 3-21. Turn-On Behavior of Figure 3-20

#### **Eliminating Initial Start-Up Pedestal**

The circuits of Figures 3-18 and 3-19 depend upon the existence of an output voltage (to create V<sub>AD.I</sub>) and, therefore, produce the initial step-function voltage pedestals of about 1.2V and 1.8V, as can be seen in Figures 3-19 and 3-21, respectively. The approach of Figure 3-22 facilitates placing the output voltage origin at zero volts because V<sub>CONTROL</sub> is derived from the input voltage. No reactive component is added to the feedback circuit. The value of R<sub>T</sub> should be considerably smaller than R3 to assure that the junction of  $R_T$  and  $C_T$  acts like a voltage source driving R3 and so  $R_{T}$  is the primary timing control. If sufficient current is introduced into the loop summing junction (via R3) to generate  $V_{AD,I} \ge$ V<sub>REF</sub>, then V<sub>OUT</sub> will be zero volts. As R<sub>T</sub> charges CT, VCONTROL decays, which would eventually result in  $V_{ADJ} < V_{REF}$ . In normal operation,  $V_{ADJ} =$ V<sub>RFF</sub>, so V<sub>OUT</sub> becomes greater than zero volts. The process continues until V<sub>CONTROL</sub> decays to V<sub>REF</sub> + 0.6V and V<sub>OUT</sub> reaches the desired value. This circuit requires a regulator with an enable function, (such as the MIC29152) because a small (< 2V) spike is generated coincident with application of a step-function input voltage. Capacitor C1 and resistor R4 provide a short hold-off timing function that eliminates this spike.

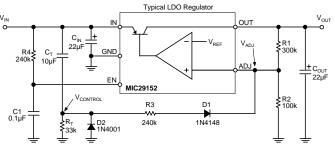


Figure 3-22. Slow Turn-On Without Pedestal Voltage

Figure 3-23 illustrates the timing of this operation. The small initial delay (about 40 milliseconds) is the time interval during which V<sub>ADJ</sub> > V<sub>REF</sub>. Since VIN is usually fairly consistent in value R3 may be chosen to minimize this delay. Note that if R3 is calculated based on the minimum foreseen  $V_{IN}$  (as described below), then higher values of VIN will produce additional delay before the turn-on ramp begins. Conversely, if VIN(max) is used for the calculation of R3, then lower values of V<sub>IN</sub> will not produce the desired turn-on characteristic; instead, there will be a small initial step-function prior to the desired turn-on ramp. Recovery from a momentarily shorted output is not addressed by this circuit, but interrupted input voltage is handled properly. Notice that the buildup of regulator output voltage differs from the waveforms of Figures 3-19 and 3-21 in that it is more ramp-like (less logarithmic). This is because only an initial portion of the RC charge waveform is used; i.e., while  $V_{CONTROL} > V_{REF} + 0.6V$ . The actual time constant used for Figure 3-22 is 0.33 second, so 3t is one second. As shown by Figure 3-23, this provides about 600 milliseconds of ramp time, which corresponds to the first 60% of the capacitor RC charge curve. R3 is calculated as follows:

at turn-on time force  $V_{ADJ} = 1.5V$ 

(just slightly higher than V<sub>REF</sub>)

th

 $_{\text{TROL}} = \frac{1.5\text{V}}{\left(\frac{\text{R1} \times \text{R2}}{\text{R1} + \text{R2}}\right)}$ 

and R3 = 
$$\frac{V_{IN min} - 0.6V}{I_{CONTROL}}$$

Since the MIC29152 is a low-dropout regulator, 6V was chosen for  $V_{IN}(min)$ . This corresponds to the small (approximately 40msec) delay before the out-

put begins to rise. With 7V input the initial delay is considerably more noticeable.

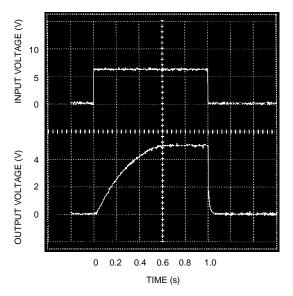


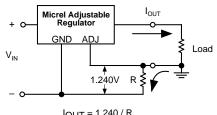
Figure 3-23. Turn-On Behavior of Figure 3-22

## **Current Sources**

Another major application for voltage regulators is current sources. Among other uses, most rechargeable batteries need some type of constant current chargers.

#### Simple Current Source

Several techniques for generating accurate output currents exist. The simplest uses a single resistor in the ground return lead (Figure 3-24). This technique works with all Micrel adjustable regulators except for the MIC5205 or the MIC5206. The output current is  $V_{RFF} \div R$ . A drawback of this simple circuit is that power supply ground and load ground are not common. Also, compliance ranges from 0V to only  $V_{OUT} - (V_{DO} + V_{REF}).$ 



I<sub>OUT</sub> = 1.240 / R

Figure 3-24. Simple Current Source Uses Reference Resistor in –V Return

#### The Super LDO Current Source

The adjustable Super LDOs, MIC5156 and MIC5158, feature linear current limiting. This is referenced to an internal 35mV source. A simple, high efficiency, high output current source may be built (Figure 3-25). Current source compliance is excellent, ranging from zero volts to  $V_{IN}$  – dropout, which is only IOUT × RDS (ON) + 35mV (generally only a few hundred millivolts even at 10A). Output current is

 $I_{OUT} = 35 \text{mV} \div \text{Rs}$ 

This circuit suffers from relatively poor accuracy, however, since the 35mV threshold is not production trimmed. R1 and R2 allow clamping the output voltage to a maximum value, if desired.

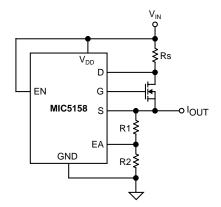


Figure 3-25. Simple Current Source Using the Super LDO

#### Accurate Current Source Using Op Amps

High accuracy and maintaining a common ground are both possible with an alternative circuit using two op amps and a low current MOSFET (Figure 3-26). This technique works with all Micrel adjustable regulators except for the MIC52xx series. Compliance is from 0V to  $V_{IN} - V_{DO}$ .

## A Low-Cost 12V & 5V Power Supply

Taking advantage of the low-dropout voltage capability of Micrel's regulators, we may build a dual output 12V & 5V linear power supply with excellent efficiency using a low cost 12.6V center-tapped "filament" transformer.

Figure 3-27 shows the schematic for the simple power supply. Using a single center-tapped transformer and one bridge rectifier, both 12V and 5V outputs are available. Efficiency is high because the transformer's RMS output voltage is only slightly above our desired outputs. The 12.6V center tapped

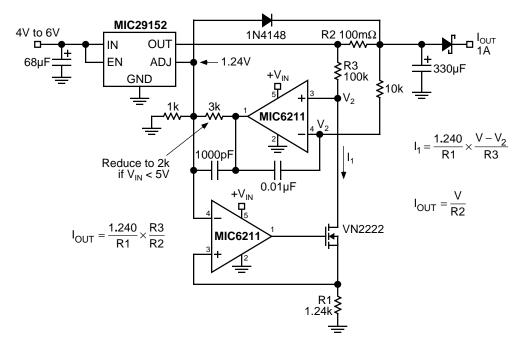


Figure 3-26. Current Source Using a Pair of Op-Amps

filament transformer is a decades-old design originally used for powering vacuum tube heaters. It is perhaps the most common transformer made. The outside windings feed the bridge rectifier and filter capacitor for the 12V output. A MIC29150-12 produces the regulated 12V output. The transformer center tap feeds the 5V filter capacitor and the MIC29150-5.0 directly—*no rectifier diode is needed*. This circuit may be scaled to other output currents as desired. Overall efficiency is extremely high due to the low input voltage, so heat sinking requirements are minimal. A final benefit: since the power tabs of the TO-220 packages are at ground potential, a single non-isolated, non-insulated heat sink may be used for both regulators.

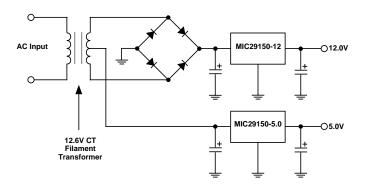


Figure 3-27. A Dual-Output Power Supply From a Single Transformer and Bridge Rectifier

# **Computer Power Supplies**

The decreasing silicon geometries of microprocessors and memory have forced a reduction in operating voltage from the longtime standard of 5V. This rise of sub-5V microprocessors, logic, and memory components in personal computer systems created demand for lower voltage power supplies. Several options exist for the desktop computer system designer. One of these options is to provide both 3.3V and 5.0V from the main system power supply. Another is to use the existing high current 5V supply and employ a low dropout (LDO) linear regulator to provide 3.3V.

The low-cost, production proven desktop computer power supplies output ±5V and ±12V-but not 3V. Redesigning the system power supply would increase cost and break the long standing power supply to motherboard connector standard which has no provision for 3V. Further complicating matters is that "3V" is not really defined. Microprocessor manufacturers produce devices requiring 2.9V, 3.3V, 3.38V, 3.45V, 3.525V, 3.6V, and several other similar voltages. No single standard has been adopted. Designing and stocking dedicated power supplies for all of these different voltages would be extremely difficult and expensive. Also, motherboard makers want to maximize their available market by allowing as many different microprocessors as possible on each board; this means they must design an on-board supply that produces all of the most popular voltages to remain competitive. This is even more important for the motherboard vendors who sell boards sans-microprocessor. They must not only provide the expected voltages, they must simplify the selection process so that all system integrators-and even some end usersmay configure the voltage properly. With too low an operating voltage, the microprocessor will generate errors; too high a voltage is fatal.

Instead, system integrators use motherboards with an on-board power supply, which converts the readily available +5V source into the required low voltage output. The simplest, lowest cost solution for this problem is the modern, very low dropout version of the venerable linear regulator. This is a low cost option, requiring only quick design work and little motherboard space. Linear regulators provide clean, accurate output and do not radiate RFI, so government certification is not jeopardized. Adjustable linear regulators allow voltage selection by means of jumper-selected resistors. They are fast starting, and may optionally provide ON/OFF control and an error flag that indicates power system trouble.

## **Dropout Requirements**

While linear regulators are extremely easy to use, one design factor must be considered: dropout voltage. For example, a regulator with 2 volts of dropout producing a 3.3V output requires over 5.3 volts on its input. Furthermore, reliable circuit operation requires operating a linear regulator above its dropout region—in other words, with a higher than minimum input voltage. In dropout, the regulator is not regulating and it responds sluggishly to load changes.

What is the required dropout voltage performance? Let's assume we have a 5V supply and need to provide 3.525V to our microprocessor. The worst case occurs when the input voltage from the 5V supply is at its minimum and the output is at its maximum. An example will illustrate.

V <sub>IN</sub> =	5V – 5% =	4.75V
V <sub>OUT</sub> =	3.525V + 2% =	<u>3.60V</u>
Maximur	n Allowable	
Dropout	Voltage:	1.15V

This simplified example does not include the effects of power supply connector, microprocessor socket, or PC board trace resistances, which would further subtract from the required dropout voltage. Fast response to load current changes (from a processor recovering from "sleep" mode, for example) occurs only when the regulator is away from its dropout point. In real systems, a maximum dropout voltage between 0.6V to 1V is ideal. Achieving this performance means the output device must be either a PNP bipolar transistor or a MOSFET.

Historically, linear regulators with PNP outputs have been expensive and limited to low current applications. However, Super ßeta PNP low dropout regulators provide up to 7.5 amperes of current with dropout voltages less than 0.6V, guaranteed. A lower cost product line outputs the same currents with only 1V of dropout. These low dropout voltages guarantee the microprocessor gets a clean, well regulated supply that quickly reacts to processor-induced load changes as well as input supply variations.

The low dropout linear voltage regulator is an easy-to-use, low cost, yet high performance means

of powering high performance low voltage microprocessors. By selecting a modern low dropout regulator, you assure reliable operation under all working conditions.

## 5V to 3.xV Conversion Circuits

Recommended circuits for on-board desktop computer power supplies follow. Due to the high speed load changes common to microprocessors, fast load transient response is crucial. This means circuit layout and bypass and filter capacitor selection is also critical. At low current levels, thermal considerations are not difficult; however, at currents of above 3 amperes, the resulting heat may be troublesome.

#### Method 1: Use a Monolithic LDO

The simplest method of providing a second V<sub>CC</sub> on a computer motherboard is by using a monolithic regulator. If the required voltage is a standard value, a fixed-voltage regulator is available. In this ideal situation, your electrical design consists of merely specifying a suitable output filter capacitor. If the output voltage is not available from a fixed regulator, adjustables are used. They use two resistors to program the output voltage but are otherwise similar to the fixed versions. Figure 3-28 and 3-29 show fixed and adjustable regulator applications.

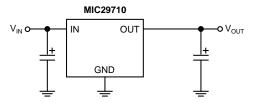
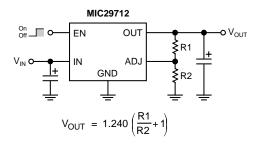


Figure 3-28. Fixed Regulator Circuit Suitable for Computer Power Supply Applications





#### Method 2: The MIC5156 "Super LDO"

The Micrel MIC5156 is a linear regulator controller that works with a low cost N-Channel power MOSFET to produce a very low dropout regulator system. The MIC5156 is available in a small 8-pin SOIC or in a standard 8-pin DIP, and offers fixed 3.3V, 5.0V, or user selectable (adjustable) voltage outputs. Figure 2 shows the entire schematic-two filter capacitors, a MOSFET, and a printed circuit board trace about a centimeter long (used as a current sense resistor) is all you need for the fixed voltage version. For the adjustable part, add two resistors. The MIC5156 requires an additional power supply to provide gate drive for the MOSFET: use your PC's 12V supply-the current drawn from the 12V supply is very small; approximately one milliampere. If a 12V supply is not available, the MIC5158 generates its own bias and does not need an additional supply.

Figure 3-30 shows a typical 3.3V and 5V computer power supply application. The MIC5156 provides regulated 3.3V using Q1 as the pass element and also controls a MOSFET switch for the 5V supply.

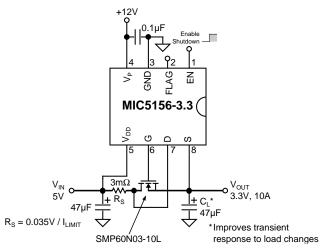


Figure 3-30. MIC5156 5V-to-3.3V Converter

When the 3.3V output has reached regulation, the FLAG output goes high, enhancing Q2, which switches 5V to Load 2. This circuit complies with the requirements of some dual-voltage microprocessors that require the 5V supply input to remain below 3.0V until the 3.3V supply input is greater than 3.0V.

An optional current limiting sense resistor (R<sub>S</sub>) limits the load current to 12A maximum. For less costly designs, the sense resistor's value and function can be duplicated using one of two techniques: A solid piece of copper wire with appropriate length and di-

#### Micrel Semiconductor

ameter (gauge) makes a reasonably accurate lowvalue resistor. Another method uses a printed circuit trace to create the sense resistor. The resistance value is a function of the trace thickness, width, and length. See *Alternative Resistors*, in **Section 4**, for current sense resistor details.

NOTE: the tab of the power MOSFET is connected to +5V. Use an insulator between the MOS-FET and the heat sink, if necessary.

#### Method 3: The MIC5158 "Super LDO"

Like the MIC5156, the MIC5158 is a linear regulator controller that works with a low cost N-Channel power MOSFET to produce a very low dropout regulator system. The MIC5158, however, generates the bias voltage required to drive the N-channel MOS-FET and does not require a 12V supply. Its on-board charge pump uses three capacitors and takes care of the level shifting. Figure 3-31 shows the MIC5158 circuit.

An idea for the motherboard manufacturer: build the MIC5158 circuit on a plug-in daughterboard with three or five pins that allow it to mount on the system board like a monolithic regulator.

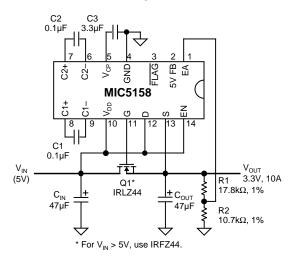


Figure 3-31. MIC5158 5V-to-3.3V Converter

#### Method 4: Current Boost a MIC2951

The 150mA MIC2951 gets a capacity boost to several amperes by using an external PNP transistor. Figure 3-32 shows the MIC2951 driving a DH45H8 or equivalent PNP transistor to achieve a 3A output. This circuit has a number of problems, including poor stability (a large output capacitor is required to squelch oscillations), poor current limiting characteristics, poor load transient response, no overtemperature shutdown protection, and requires numerous external components. It is not recommended.

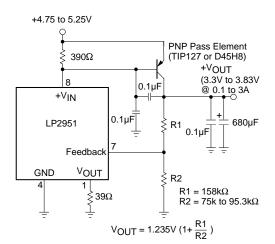


Figure 3-32. PNP Transistor Boosts Current Output From MIC2951 Regulator

#### Adjust Resistor Values

Table 3-5 shows recommended resistor values for various voltages. The values shown represent the calculated closest-match for the desired voltage using standard 1% tolerance resistors. Since Micrel's adjustable regulators use a high impedance feedback stage, large value adjust resistors are generally recommended. Valid resistor values range from a few ohms to about  $500k\Omega$ .

While the MIC29152/29302/29502 have a 1.240V reference, the Super LDO and current boosted MIC2951 circuits use a 1.235V reference.

		28 & 29	Figs. 3-30, 31, & 32
Voltage		1.240V) <b>R2</b>	(V <sub>REF</sub> = 1.235V) <b>R1 R2</b>
1.5	80.6k	16.9k	53.6k 11.5k
1.8	237k	107k	301k 137k
2.85	287k	221k	187k 143k
2.9	162k	121k	137k 102k
3.0	102k	71.5k	150k 105k
3.1	158k	105k	154k 102k
3.15	191k	124k	158k 102k
3.3	196k	-	178k 107k
3.45	221k	124k	191k 107k
3.6	102k	53.6k	383k 200k
3.8	221k	107k	221k 107k
4.0	255k	115k	115k 51.1k
4.1	316k		232k 100k
4.5	137k	52.3k	107k 40.2k

## 3.3V to 2.xV Conversion

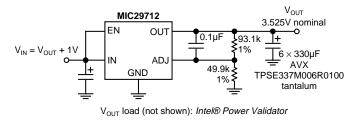
Like the 5V to 3.3V conversion discussed above, dropping to voltages below 3.3V from a 3.3V rail is a useful application for LDO regulators. Here, the regulator dropout voltage is much more critical. Applications using 2.9V only have 400mV of headroom when powered from a perfect 3.3V supply. For the standard 3.3V supply tolerance of  $\pm$ 300mV, the headroom drops to only 100mV. For this situation, the most reasonable solution is one of the Super LDO circuits shown in Figures 3-30 and 3-31. These circuits feature excellent efficiency—approximately 88%. Monolithic LDO solutions powered from a standard 3.3V  $\pm$  300mV supply become tenable with output voltages of 2.5V or below.

## Improving Transient Response

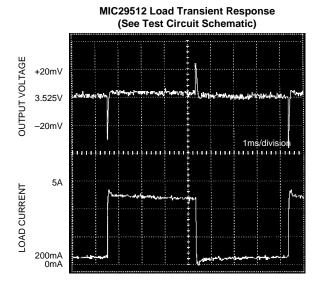
Modern low-voltage microprocessors have multiple operating modes to maximize both performance and minimize power consumption. They switch between these modes quickly, however, which places a strain on their power supply. Supply current variations of several orders of magnitude in tens of nanoseconds are standard for some processors—and they still require that their supply voltage remain within specification throughout these transitions.

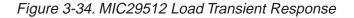
Micrel low-dropout regulators have excellent response to variations in input voltage and load current. By virtue of their low dropout voltage, these devices do not saturate into dropout as readily as similar NPN-based designs. A 3.3V output Super  $\beta$ eta PNP LDO will maintain full speed and performance with an input supply as low as 4.2V, and will still provide some regulation with supplies down to 3.8V, unlike NPN devices that require 5.1V or more for good performance and become nothing more than a resistor under 4.6V of input. Micrel's PNP regulators provide superior performance in "5V to 3.3V" conversion applications, especially when all tolerances are considered.

Figure 3-33 is a test schematic using the Intel<sup>®</sup> Pentium<sup>™</sup> Validator. The Validator is a dynamic load which simulates a Pentium processor changing states at high speed. Using Figure 3-33, the MIC29512 (Figure 3-34) was tested with fast 200mA to 5A load transitions. The MIC29712 was tested with fast transitions between 200mA and 7.5A (Figure 3-35).



#### Figure 3-33. Load Transient Response Test Circuit. Super LDO System Driving an Intel Pentium "Validator" Test System





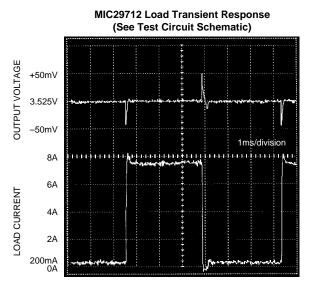


Figure 3-35. MIC29712 Load Transient Response. Load Varies from 200mA to 7.5A

The following photographs show the transient response of the MIC5156 Super LDO with an IRL3103 power MOSFET (R<sub>DS (ON)</sub>  $\leq$  14m $\Omega$ , Ciss = 1600pF) driving the Intel Pentium<sup>™</sup> Validator. Figure 3-36 shows the performance with four (4) 330µF AVX surface mount capacitors. The peak transient response voltage is -55mV on attack and +60mV on turn-off. Figure 3-37 shows the tremendous improvement another four  $330\mu$ F capacitors make: with eight (8) 330µF AVX capacitors, the transient peaks drop to only approximately ±25mV. These measurements are made with  $V_{DD}$  = 5.0V,  $V_{P}$  = 12.0V, and a single  $330\mu F$  bypass capacitor on the V<sub>DD</sub> input to the MIC5156. As both the 5156 and the MIC5158 use the same error amplifier circuit, their transient response should be similar. Furthermore, the transient response of the MIC5156 does not change as the input voltage  $(V_{\Box \Box})$  decreases from 5.0V down to nearly dropout levels (a bit less than 3.6V input with the 3.525V output).

#### Accuracy Requirements

Microprocessors have various voltage tolerance requirements. Some are happy with supplies that swing a full ±10%, while others need better than ±2.5% accuracy for proper operation. Fixed 3.3V devices operate well with any of these microprocessors, since Micrel guarantees better than  $\pm 2\%$  across the operating load current and temperature ranges. Locating the regulator close to the processor to minimize lead resistance and inductance is the only design consideration that is necessary. Microprocessors that use nonstandard or varying voltages have a problem: while the basic adjustable regulator offers  $\pm 1\%$ accuracy and ±2% worst case over temperature extremes, any error in the external programming resistors (either in tolerance or compromise in resistance ratio that is unavoidable when using standardized resistor values) directly appears as output voltage error. The error budget quickly disappears. See Adjustable Regulator Accuracy Analysis, in this section, for a discussion of voltage tolerance and sensitivity.

When any trace resistance effects are considered, it is painfully apparent that this solution will not provide the needed  $\pm 2.5\%$  accuracy. Resistors of 0.1% tolerance are one step. Other ideas are presented in *Improving Regulator Accuracy*, also in this section.

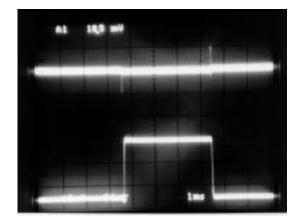


Figure 3-36. Transient response of the MIC5156 Super LDO driving an Intel Pentium "Validator" microprocessor simulator. Output capacitance is  $4 \times 330 \mu F$ .

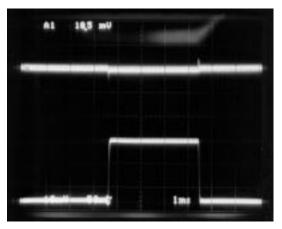
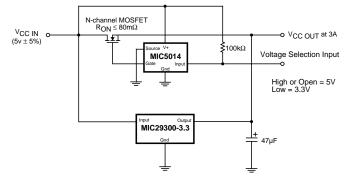


Figure 3-37. Transient response of the MIC5156 Super LDO driving an Intel Pentium "Validator" microprocessor simulator. Output capacitance is  $8 \times$ 330µF.

## Multiple Output Voltages

Another design parameter computer motherboard designers cope with is the need to support different types of microprocessors with one layout. Since processors in a single family may require different voltages, it is no surprise that different processor types also may need various supply voltages. Since it is expensive to provide multiple variable outputs from the system power supply, the economical solution to this problem is to generate or switch between supplies directly on the motherboard.

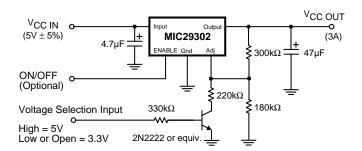
Occasionally, a designer will get lucky and some motherboard options can use a standard voltage from the power supply. In this case, we may switch the higher voltage around the LDO generating the lower voltage, as shown in Figure 3-38. This circuit was designed to allow Intel DX4Processors<sup>™</sup>, running on 3.3V, to operate in the same socket as a standard 5V 486. A pin on the DX4Processor is hard wired to ground, which provides the switching needed for automatically selecting the supply voltage. Standard 486 processors have no connection to this pin.



#### Figure 3-38. Switching 5V or 3.3V to a Microprocessor

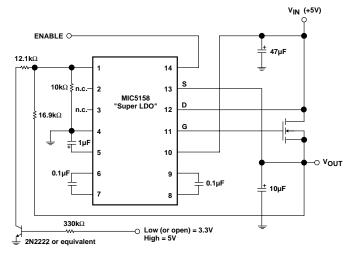
This circuit capitalizes on the reversed-battery protection feature built into Micrel's Super  $\beta$ eta PNP regulators. The regulators survive a voltage forced on their output that is higher than their programmed output. In this situation, the regulator places its pass transistor in a high impedance state. Only a few microamperes of current leaks back into the regulator under these conditions, which should be negligible. Note that an adjustable regulator could be used in place of the fixed voltage version shown.

An adjustable regulator and an analog switch will perform this task, as shown in Figure 3-39. Only one supply (of the maximum desired output voltage, or higher) is necessary.



#### Figure 3-39. Adjustable LDO and analog switch provides selectable output voltages

Another method of providing two or more output voltages to a socket with the higher of the two provided is by using the Super LDO. Program the adjustable MIC5156 or MIC5158 as shown in Figure 3-40. When the higher of the two voltages is chosen, the regulator simply acts as a low-loss switch. Use a transistor switch to select the lower voltage. This technique may be expanded to any number of discrete voltages, if desired. The MIC5158 will operate from a single input supply of 3.0V or greater. The MIC5156 needs a low current 12V supply to provide gate bias for the pass MOSFET, but if this is available, it is smaller than the MIC5158 and requires no charge pump capacitors.



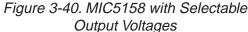


Figure 3-41 is a switched voltage PNP regulator that relies on jumpers for output voltage programming. While perhaps not as "elegant" as the previous techniques, it provides full functionality and flexibility. This circuit was designed so if all jumpers are accidentally removed, the output voltage drops to its lowest value. By configuring the jumpers as shown, the system is relatively safe—if someone inadvertently removes all

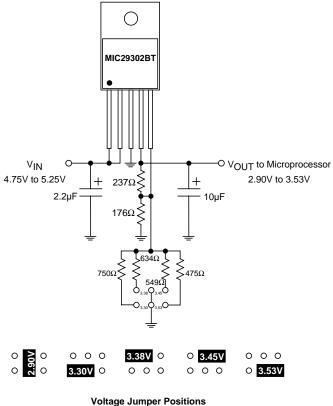


Figure 3-41. Jumper Selectable Output Voltages

the jumpers, the output voltage drops to a low value. While the system may be error-prone or nonfunctional with this low voltage, at least the microprocessor will survive.

## Multiple Supply Sequencing

Some microprocessors use multiple supply voltages; a voltage for the core, another for the cache memory, and a different one for I/O, for example. Sequencing these supplies may be critical to prevent latch-up. Figure 3-42 shows an easy way of guaranteeing this sequencing using Micrel's regulators with an enable control. As the output voltage of Supply 1 rises above 2V, the regulator for Supply 2 starts up. Supply 2 will never be high until Supply 1 is active. Supply 1 need not be the higher output voltage; it must only be 2.4V or above (necessary to assure the second regulator is fully enabled). Note that Supply 1 may not need an enable pin.

This technique works with the MIC29151 through MIC29752 monolithic regulators as well as with the Super LDO (MIC5156/57/58). It also is applicable for systems requiring any number of sequenced supplies, although for simplicity we only show two supplies here.

## Thermal Design

Once the electrical design of your power system is complete, we must deal with thermal issues. While they are not terribly difficult, thermal design is lightly covered in most electrical engineering curriculum. Properly addressing thermal issues is imperative to LDO system reliability, and is covered in detail in *Thermal Management*, later in this section.

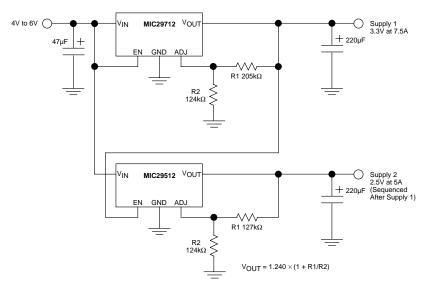


Figure 3-42. Multiple Supply Sequencing

# **Portable Devices**

Voltage regulators are necessary in almost all electronic equipment, and portable devices are no exception. Portable equipment includes cellular and "wireless" telephones, radio receivers and handheld transceivers, calculators, pagers, notebook computers, test equipment, medical appliances and most other battery operated gear.

## **Design Considerations**

Portable electronics are characterized by two major distinguishing features:

- Small size
- Self-contained power source (batteries)

Beyond these similarities, portable equipment power requirements vary as much as their intended application.

#### **Small Package Needed**

Portable devices are, by definition, relatively small and lightweight. Most circuitry is surface mounted and power dissipation is normally minimized.

#### Self Contained Power

Most portable equipment is battery powered. Batteries are often the largest and heaviest component in the system, and may account for 80% or more of the total volume and mass of the portable device. Power conservation is an important design consideration. Low power components are used and power management techniques, such as "sleep mode", help maximize battery life. Just as one is never too rich, one's batteries never last long enough!

Yet another battery-imposed limitation is that batteries are available in discrete voltages, determined by their chemical composition. Converting these voltages into a constant supply suitable for electronics is the regulator's most important task.

## Low Current (And Low Voltage)

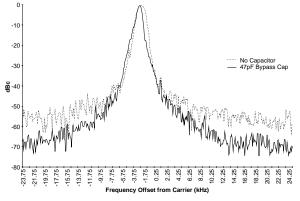
The regulators used in portable equipment are usually low output current devices, generally under 250mA, since their loads are also (usually) low current. Few portable devices have high voltage loads<sup>4</sup> and those that do need little current.

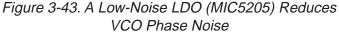
#### Low Output Noise Requirement

Cellular telephones, pagers, and other radios have frequency synthesizers, preamplifiers, and mixers that are susceptible to power supply noise. The frequency synthesizer voltage controlled oscillator (VCO), the block that determines operating frequency, may produce a noisy sine wave output (a wider bandwidth signal) if noise is present on V<sub>CC</sub>. Making matters worse for portable equipment designers, lower powered/lower cost VCOs are generally more susceptible to V<sub>CC</sub> noise.

Ideal VCOs produce a single spectral line at the operating frequency. Real oscillators have sideband skirts; poor devices have broad skirts. Figure 3-43 shows the measured phase noise from a free running Murata MQE001-953 VCO powered by a MIC5205 low-noise regulator. Note the significant improvement when using the noise bypass capacitor. Regulators not optimized for noise performance produce skirts similar to or worse than the MIC5205 without bypass capacitors.

Broad oscillator skirts decrease the noise figure and the strong signal rejection capability of receivers (reducing performance) and broaden the transmitted signal in transmitters (possibly in violation of spectral purity regulations).





Although not as susceptible to noise as VCOs, preamplifiers and mixers operating from noisy supplies also reduce receiver and transmitter performance in similar ways.

NOTE 4: The notable exceptions to this statement are the fluorescent backlights in notebook computers and the electroluminescent lamps in telephones, watches, etc. These lamps must be driven with a switching regulator that boosts the battery voltage—something a linear regulator cannot do.

#### **Dropout and Battery Life**

Low dropout regulators allow more operating lifetime from batteries by generating usable output to the load well after standard regulators would be saturated. This allows discharging batteries to lower levels or—in many cases—eliminating a cell or two from a series string. Compared to older style regulators with 2 to 3V of dropout, Micrel's 0.3V to 0.6V LDOs allow eliminating one to two alkaline, NiCd, or NiMH cells.

#### **Ground Current and Battery Life**

The quiescent, or ground, current of regulators employed inside portable equipment is also important. This current is yet another load for the battery, and should be minimized.

#### **Battery Stretching Techniques**

#### Sleep Mode Switching

Sleep mode switching is an important technique for battery powered devices. Basically, sleep mode switching powers down system blocks not immediately required. For example, while a cellular phone must monitor for an incoming call, its transmitter is not needed and should draw no power; it can be shut off. Likewise, audio circuits may be powered down. Portable computers use sleep mode switching by spinning down the hard disk drive and powering down the video display backlight, for example. Simpler devices like calculators automatically turn off after a certain period of inactivity.

Micrel's LDO regulators make sleep mode implementation easy because each family has a version with logic-compatible shutdown control. Many families feature "zero power" shutdown—when disabled, the regulator fully powers down and draws virtually zero current.<sup>5</sup> Designers updating older systems that used MOSFETs for switching power to regulators may now eliminate the MOSFET. The regulator serves as switch, voltage regulator, current limiter, and overtemperature protector. All are important features in any type of portable equipment.

#### **Power Sequencing**

A technique related to Sleep Mode Switching is Power Sequencing. This is a power control technique that enables power blocks for a short while and then disables them. For example, in a cellular telephone awaiting a call, the receiver power may be pulsed on and off at a low-to-medium duty cycle. It listens for a few milliseconds each few hundred milliseconds.

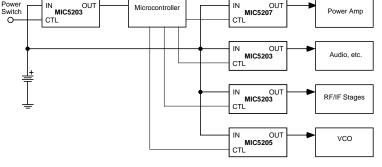
## Multiple Regulators Provide Isolation

The close proximity between different circuit blocks naturally required by portable equipment increases the possibility of interstage coupling and interference. Digital noise from the microprocessor may interfere with a sensitive VCO or a receiver preamplifier, for example. A common path for this noise is the common supply bus. Linear regulators help this situation by providing active isolation between load and input supply. Noise from a load that appears on the regulator's output is greatly attenuated on the regulator's input.

Figure 3-44 shows a simplified block diagram of a cellular telephone power distribution system. Between five and seven regulators are used in a typical telephone, providing regulation, ON/OFF (sleep mode) switching, and active isolation between stages.

NOTE 5: In the real world, there is no such thing as zero, but Micrel's regulators pass only nanoamperes of device leakage current when disabled—"virtually zero" current.

Figure 3-44. Cellular Telephone Block Diagram



# **Thermal Management**

## A Thermal Primer

Micrel low dropout (LDO) regulators are very easy to use. Only one external filter capacitor is necessary for operation, so the electrical design effort is minimal. In many cases, thermal design is also quite simple, aided by the low dropout characteristic of Micrel's LDOs. Unlike other linear regulators, Micrel's LDOs operate with dropout voltages of 300mV-often less. The resulting Voltage  $\times$  Current power loss can be quite small even with moderate output current. At higher currents and/or higher input-to-output voltage differentials, however, selecting the correct heat sink is an essential "chore".

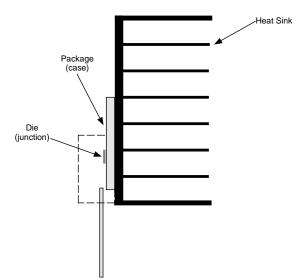


Figure 3-45. Regulator Mounted to a Heat Sink

## **Thermal Parameters**

Before working with thermal parameters, we will define the applicable symbols and terms.

$\Delta T$	Temperature difference, °C)	rise	(temperature
q	Heat flow (Watts)		
θ	Thermal resistance	ce (°C/W	)
PD	Power Dissipation	n (Watts)	
$\theta_{JA}$	Thermal resistand to ambient (free a		on (die)
θJC	Thermal resistand package (case)	ce, juncti	on (die) to the
θCS	Thermal resistand the heat sink	ce, case	(package) to

<sup>θ</sup> SA	Thermal resistance, heat sink to ambient
0/1	(free air)

T<sub>A</sub> Ambient temperature

T<sub>.1</sub> Junction (die) temperature

 $T_{J(MAX)}$  Maximum allowable junction temperature

Figure 3-46 shows the thermal terms as they apply to linear regulators. The "junction" or "die" is the active semiconductor regulator; this is the heat source. The package shown is the standard TO-220; the "case" is the metal tab forming the back of the package which acts as a heat spreader. The heat sink is the interface between the package and the ambient environment. Between each element-junction, package, heat sink, and ambient-there exists interface thermal resistance. Between the die and the package is the junction to case thermal resistance,  $\theta_{JC}$ . Between the package and the heat sink is the case-to-sink thermal resistance,  $\theta_{CS}$ . And between the heat sink and the external surroundings is the heat sink to ambient thermal resistance,  $\theta_{SA}$ . The total path from the die to ambient is  $\theta_{JA}$ .

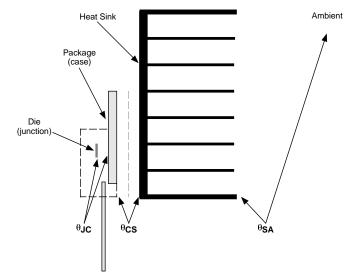


Figure 3-46. Thermal Parameters

#### **Thermal/Electrical Analogy**

For those of us more comfortable with the laws of Kirchhoff and Ohm than those of Boyle or Celsius, an electrical metaphor simplifies thermal analysis. Heat flow and current flow have similar characteristics. Table 3-6 shows the general analogy.

Thermal Parameter	Electrical Parameter
Power (q)	Current (I)
Thermal Resistance (θ)	Resistance (R)
Temperature Difference (∆T)	Voltage (V)

Table 3-6. Thermal/Electrical Analogy

The formula for constant heat flow is:

 $\theta = \Delta T / q$ 

The equivalent electrical (Ohm's Law) form is:

 $I = \Delta V / R$ 

Electrically, a voltage difference across a resistor produces current flow. Thermally, a temperature gradient across a thermal resistance creates heat flow. From this, we deduce that if we dissipate power as heat and need to minimize temperature rise, we must minimize the thermal resistance. Taken another way, if we have a given thermal resistance, dissipating more power will increase the temperature rise.

Thermal resistances act like electrical resistances: in series, they add; in parallel, their reciprocals add and the resulting sum is inverted. The general problem of heat sinking power semiconductors may be simplified to the following electrical schematic (Figure 3-47).

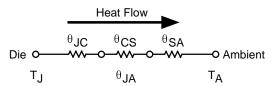


Figure 3-47. Heat flow through the interface resistances.

Summing these resistances, the total thermal path for heat generated by the regulator die is:

 $\theta_{JA} = \theta_{JC} + \theta_{CS} + \theta_{SA}$ 

## **Calculating Thermal Parameters**

Two types of thermal parameters exist; those we may control and those fixed by the application (or physics). The application itself determines which category the parameters fit—some systems have a specific form factor dictated by other factors, for example. This serves to limit the maximum heat sink size possible.

Parameter	Extenuating Circumstances
<sup>θ</sup> SA	Set by heat sink size, design and air flow
$\theta$ JC	Set by regulator die size and package type
θCS	Set by mounting technique and package type
<sup>T</sup> J(MAX)	Set by regulator manufac- turer and lifetime consider- ations
Power dissipation	Set by V <sub>IN</sub> , V <sub>OUT</sub> , and I <sub>OUT</sub>

Each regulator data sheet specifies the junction to case thermal resistance,  $\theta_{JC}$ . Heat sink manufacturers specify  $\theta_{SA}$ , (often graphically) for each product. And  $\theta_{CS}$  is generally small compared to  $\theta_{JC}$ . The maximum die temperature for Micrel regulators is generally 125°C, unless specified otherwise on the data sheet. The last remaining variable is the regulator power dissipation.

Power dissipation in a linear regulator is:

$$\mathsf{P}_\mathsf{D} = [(\mathsf{V}_\mathsf{IN} - \mathsf{V}_\mathsf{OUT}) \ \mathsf{I}_\mathsf{OUT}] + (\mathsf{V}_\mathsf{IN} \times \mathsf{I}_\mathsf{GND})$$

Where:

 $P_D$  = Power dissipation

V<sub>IN</sub> = Input voltage applied to the regulator

V<sub>OUT</sub> = Regulator output voltage

I<sub>OUT</sub> = Regulator output current

IGND = Regulator biasing currents

Proper design dictates use of worst case values for all parameters. Worst case  $V_{IN}$  is high supply. Worst case  $V_{OUT}$  for thermal considerations is the lowest possible output voltage, subtracting all tolerances from the nominal output. I<sub>OUT</sub> is taken at its highest steady-state value. The ground current value comes from the device's data sheet, from the graph of I<sub>GND</sub> vs. I<sub>OUT</sub>.

#### Calculating Maximum Allowable Thermal Resistance

Given the power dissipation, ambient operating temperature, and the maximum junction temperature of a regulator, the maximum allowable thermal resistance is readily calculated.

 $\theta_{JA} \leq (T_{J(MAX)} - T_A) / P_D$ 

Maximum heat sink thermal resistance is

 $\theta_{SA} \le \theta_{JA} - (\theta_{JC} + \theta_{CS})$ 

We calculate the thermal resistance ( $\theta_{SA}$ ) required of the heat sink using the following formula:

$$\theta_{SA} = \frac{T_J - T_A}{P_D} - (\theta_{JC} + \theta_{CS})$$

## Why A Maximum Junction Temperature?

Why do semiconductors, including LDO regulators, have a maximum junction temperature  $(T_{I})$ ? Heat is a natural enemy of most electronic components, and regulators are no exception. Semiconductor lifetimes, statistically specified as mean time to failure (MTTF) are reduced significantly when they are operated at high temperatures. The junction temperature, the temperature of the silicon die itself, is the most important temperature in this calculation. Device manufacturers have this lifetime-versus-operating temperature trade-off in mind when rating their devices. Power semiconductor manufacturers must also deal with the inevitable temperature variations across the die surface, which are more extreme for wider temperature-range devices. Also, the mechanical stress induced on the semiconductor, its package, and its bond wires is increased by temperature cycling, such as that caused by turning equipment on and off. A regulator running at a lower maximum junction temperature has a smaller temperature change, which creates less mechanical stress.

The expected failure rate under operating conditions is very small, and expressed in FITs (failures in time), which is defined as failures per one billion device hours. Deriving the failure rate from the operating life test temperature to the actual operating temperature is performed using the Arrhenius equation:

$$\frac{100}{FR2} = \frac{MTTF2}{MTTF1} = e^{\left(\frac{Ea}{k}\right)\left(\frac{1}{T2} - \frac{1}{T1}\right)}$$

Designing With LDO Regulators

Where:

FR1 is the failure rate at temperature T1 (Kelvin) FR2 is the failure rate at temperature T2 MTTF1 is the mean time to failure at T1 MTTF2 is the mean time to failure at T2 Ea is the activation energy in electron volts (eV) k is Boltzmann's constant (8.617386 x  $10^{-5}$  eV/K)

The activation energy is determined by long-term burn-in testing. An average value of 0.62eV is determined, after considering all temperature-related failure mechanisms, including silicon-related failure modes and packaging issues, such as the die attach, lead bonding, and package material composition. Using a reference temperature of 125°C (498K) and normalizing to 100 FITs, the formula becomes:

$$\frac{100}{\mathsf{FR2}} = e^{\left(\frac{0.62}{\mathsf{k}}\right)\left(\frac{1}{\mathsf{T2}} - \frac{1}{498}\right)}$$

The standard semiconductor reliability versus junction temperature characteristic is shown in Figure 3-48. We see that a device operating at 125°C has a relative lifetime of 100. For each 15°C rise in junction temperature, the MTTF halves. At 150°C, it drops to about 34. On the other hand, at 100°C, its life is more than tripled, and at 70°C, it is 1800.

As a designer of equipment using LDOs, the most important rule to remember is "cold is cool; hot is not". Minimizing regulator temperatures will maximize your product's reliability.

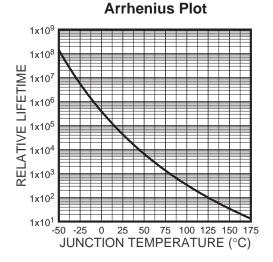


Figure 3-48. Typical MTTF vs. Temperature Curve

## Heat Sink Charts for High Current Regulators

The heat sink plays an important role in high current regulator systems, as it directly affects the safe operating area (SOA) of the semiconductor. The following graphs, Figure 3-49 through 3-53, show the maximum output current allowable with a given heat

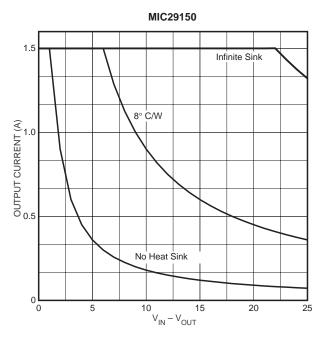


Figure 3-49. Maximum Output Current With Different Heat Sinks, MIC29150 Series

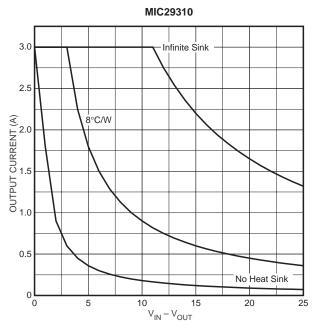


Figure 3-50. Maximum Output Current With Different Heat Sinks, MIC29300 Series

sink for different input-output voltages at an ambient temperature of 25°C. Three curves are shown: no heat sink, nominal heat sink, and infinite heat sink ( $\theta_{SA} = 0$ ). Additional thermal design graphs appear in **Section 2**.

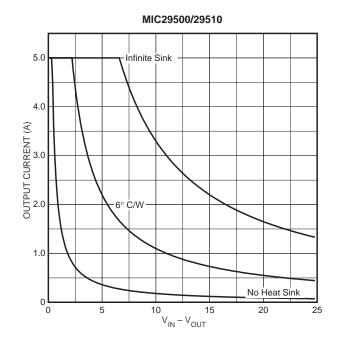


Figure 3-51. Maximum Output Current With Different Heat Sinks, MIC29500 Series

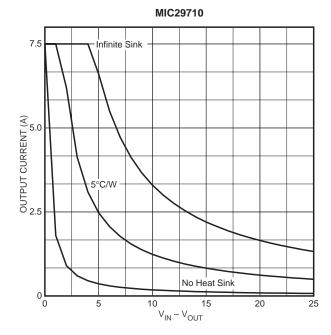


Figure 3-52. Maximum Output Current With Different Heat Sinks, MIC29710/MIC29712

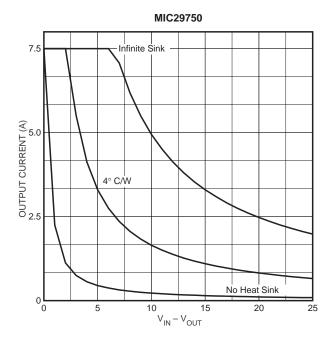


Figure 3-53. Maximum Output Current With Different Heat Sinks, MIC29750/MIC29752

## Thermal Examples

Let's do an example. We need to design a power supply for a low voltage microprocessor which requires 3.3V at up to 3A. It will get its input from a 5V ±5% supply. We choose a MIC29300-3.3BT for our regulator. The worst case V<sub>IN</sub> is high supply; in this case, 5V + 5%, or 5.25V. The LDO has a maximum die temperature of 125°C in its TO-220 package with a  $\theta_{JC}$  of 2°C/W and a mounting resistance ( $\theta_{CS}$ ) of 1°C/W<sup>2</sup>, and will operate at an ambient temperature of 50°C. Worst case V<sub>OUT</sub> for thermal considerations is minimum, or 3.3V – 2% = 3.234V.<sup>5</sup> I<sub>OUT</sub> is taken at its highest steady-state value. The ground current value comes from the device's data sheet, from the graph of I<sub>GND</sub> vs. I<sub>OUT</sub>.

Armed with this information, we calculate the thermal resistance ( $\theta_{SA}$ ) required of the heat sink using the previous formula:

$$\theta_{SA} = \frac{125 - 50^{\circ}C}{10.5W} - (2 + 1^{\circ}C/W) = 4.1^{\circ}C/W$$

Performing similar calculations for 1.25A, 1.5A, 2.0A, 2.5A, 3.0A, 4.0A, and 5.0A gives the results shown in Table 3-7. We choose the smallest regulator for the required current level to minimize cost.

Regulator	I <sub>OUT</sub>	P <sub>D</sub> (W)	θ <sub>SA</sub> (°C/W)
MIC29150	1.25A	2.6	25
MIC29150	1.5A	3.2	21
MIC29300	2.0A	4.2	15
MIC29300	2.5A	5.2	11
MIC29300	3.0A	6.3	8.8
MIC29500	4.0A	8.4	5.9
MIC29500	5.0A	10.5	4.1

Table 3-7. Micrel LDO power dissipation and heat sink requirements for various 3.3V current levels.

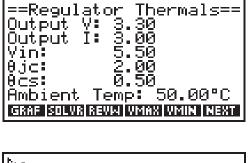
Table 3-8 shows the effect maximum ambient temperature has on heat sink thermal properties. Lower thermal resistances require physically larger heat sinks. The table clearly shows cooler running systems need smaller heat sinks, as common sense suggests.

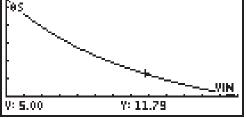
Output	Ambient Temperature		
	40°C	50°C	60°C
1.5A	24°C/W	21°C/W	17°C/W
5A	5.1°C/W	4.1°C/W	3.2°C/W

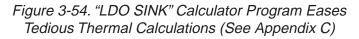
Table 3-8. Ambient Temperature Affects Heat Sink Requirements

Although routine, these calculations become tedious. A program written for the HP 48 calculator is available from Micrel that will calculate any of the above parameters and ease your design optimization process. It will also graph the resulting heat sink characteristics versus input voltage. See Appendix C for the program listing or send e-mail to Micrel at apps@micrel.com and request program "LDO SINK for the HP48".

NOTE 5: Most Micrel regulators are production trimmed to better than  $\pm 1\%$  accuracy under standard conditions. Across the full temperature range, with load current and input voltage variations, the device output voltage varies less than  $\pm 2\%$ .







## Heat Sink Selection

With this information we may specify a heat sink. The worst case is still air (natural convection). The heat sink should be mounted so that at least 0.25 inches (about 6mm) of separation exists between the sides and top of the sink and other components or the system case. Thermal properties are maximized when the heat sink is mounted so that natural vertical motion of warm air is directed along the long axis of the sink fins.

If we are fortunate enough to have some forced airflow, reductions in heat sink cost and space are possible by characterizing air speed—even a slow air stream significantly assists cooling. As with natural convection, a small gap allowing the air stream to pass is necessary. Fins should be located to maximize airflow along them. Orientation with respect to vertical is not very important, as airflow cooling dominates the natural convection.

As an example, we will select heat sinks for 1.5A and 5A outputs. We consider four airflow cases: natural convection, 200 feet/minute (1m/sec), 300 feet/ minute (1.5m/sec), and 400 feet/minute (2m/sec). Table 3 shows heat sinks for these air velocities; note the rapid reduction in size and weight (fin thickness) when forced air is available. Consulting manufacturer's charts, we see a variety of sinks are made that are suitable for our application. At 5A (10.5W worst case package dissipation) and natural convection, sinks are sizable, but at 1.5A (3.2W worst case package dissipation) and 400 feet/minute air-flow, modest heat sinks are adequate.

Output Current				
Airflow	1.5A	5A		
400 ft./min. (2m/sec)	Thermalloy 6049PB	Thermalloy 6232 Thermalloy 6034 Thermalloy 6391B		
300 ft./min. (1.5m/sec)		AAVID 504222B AAVID 563202B AAVID 593202B AAVID 534302B Thermalloy 7021B Thermalloy 6032 Thermalloy 6234B		
200 ft./min. (1m/sec)	AAVID 577002 Thermalloy 6043PB Thermalloy 6045B	AAVID 508122 AAVID 552022 AAVID 533302 Thermalloy 7025B Thermalloy 7024B Thermalloy 7022B Thermalloy 6101B		
Natural Convection (no forced airflow)	AAVID 576000 AAVID 574802 592502 579302 Thermalloy 6238B Thermalloy 6038 Thermalloy 7038	AAVID 533602B (v) AAVID 519922B (h) AAVID 532802B (v) Thermalloy 6299B (v) Thermalloy 7023 (h)		

Table 3-9. Commercial Heat Sinks for 1.5A and 5.0A Applications [Vertical Mounting Denoted by (V); (H) Means Horizontal Mounting]

## **Reading Heat Sink Graphs**

Major heat sink manufacturers provide graphs showing their heat sink characteristics. The standard graph (Figure 3-55) depicts two different data: one curve is the heat sink thermal performance in still air (natural convection); the other shows the performance possible with forced cooling. The two graphs should be considered separately since they do not share common axes. Both are measured using a single device as a heat source: if multiple regulators are attached, thermal performance improves by as much as one-third (see *Multiple Packages on One Heat Sink*, below).

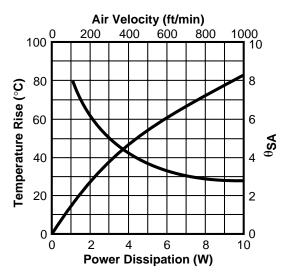


Figure 3-55. Typical Heat Sink Performance Graph

Figure 3-56 shows the natural convection portion of the curve. The x-axis shows power dissipation and the y-axis represents temperature rise over ambient. While this curve is nearly linear, it does exhibit some droop at larger temperature rises, representing increased thermodynamic efficiency with larger  $\Delta T$ . At any point on the curve, the  $\theta_{SA}$  is determined by dividing the temperature rise by the power dissipation.

Figure 3-57 shows the thermal resistance of the heat sink under forced convection. The x-axis (on top, by convention) is air velocity in lineal units per minute. The y-axis (on the right side) is  $\theta_{SA}$ .

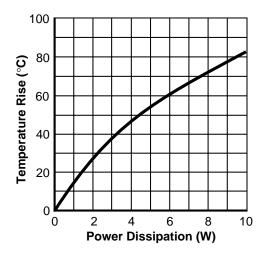


Figure 3-56. Natural Convection Performance

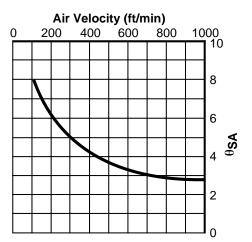


Figure 3-57. Forced Convection Performance

## Power Sharing Resistor

The heat sink required for 5A applications in still air is massive and expensive. There is a better way to manage heat problems: we take advantage of the very low dropout voltage characteristic of Micrel's Super ßeta PNP<sup>™</sup> regulators and dissipate some power externally in a series resistance. By distributing the voltage drop between this low cost resistor and the regulator, we distribute the heating and reduce the size of the regulator heat sink. Knowing the worst case voltages in the system and the peak current requirements, we select a resistor that drops a portion of the excess voltage without sacrificing performance. The maximum value of the resistor is calculated from:

$$\mathsf{R}_{\mathsf{MAX}} = \frac{\mathsf{V}_{\mathsf{IN}\;(\mathsf{MIN})} - (\mathsf{V}_{\mathsf{OUT}\;(\mathsf{MAX})} + \mathsf{V}_{\mathsf{DO}})}{\mathsf{I}_{\mathsf{OUT}\;(\mathsf{PEAK})} + \mathsf{I}_{\mathsf{GND}}}$$

Where:  $V_{IN (MIN)}$  is low supply (5V - 5% = 4.75V)

 $V_{OUT (MAX)}$  is the maximum output voltage across the full temperature range (3.3V + 2% = 3.366V)

 $V_{\text{DO}}$  is the worst case dropout voltage across the full temperature range (600mV)

 $I_{OUT (PEAK)}$  is the maximum 3.3V load current

 $I_{GND}$  is the regulator ground current.

For our 5A output example:

$$\mathsf{R}_{\mathsf{MAX}} = \frac{4.75 - (3.366 + 0.6) \text{ V}}{5 + 0.08 \text{ A}} = \frac{0.784 \text{ V}}{5.08 \text{ A}} = 0.154 \Omega$$

The power drop across this resistor is:

$$P_{D (RES)} = (I_{OUT (PEAK)} + I_{GND})^2 \times R$$

or 4.0W. This subtracts directly from the 10.5W of regulator power dissipation that occurs without the resistor, reducing regulator heat generation to 6.5W.

 $P_{D(Regulator)} = P_{D(R = 0\Omega)} - P_{D(RES)}$ 

Considering 5% resistor tolerances and standard values leads us to a  $0.15\Omega \pm 5\%$  resistor. This produces a nominal power savings of 3.9W. With worst-case tolerances, the regulator power dissipation drops to 6.8W maximum. This heat drop reduces our heat sinking requirements for the MIC29500 significantly. We can use a smaller heat sink with a larger thermal resistance. Now, a heat sink with 8.3°C/W thermal characteristics is suitable—nearly a factor of 2 better than without the resistor. Table 3-10 lists representative heat sinks meeting these conditions.

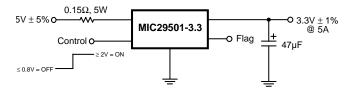


Figure 3-58. Resistor Power Sharing Reduces Heat Sink Requirement

For the 1.5A output application using the MIC29150, we calculate a maximum R of  $0.512\Omega$ . Using R =  $0.51\Omega$ , at least 1.1W is saved, dropping power dissipation to only 2.0W—a heat sink is probably not required. This circuit is shown in Figure 3-59.

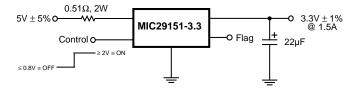


Figure 3-59. Power Sharing Resistor Eliminates Need for Separate Heat Sink

Another option exists for designers of lower current systems. The MIC29150 and MIC29300 regulators are available in the surface mount derivative of the TO-220 package, the TO-263, which is soldered directly to the PC board. No separate heat sink is necessary, as copper area on the board acts as the heat exchanger. For further information, refer to *Heat Sinking Surface Mount Packages*, which follows.

Airflow	Heat Sink Model
400 ft./min. (2m/sec)	AAVID 530700 AAVID 574802 Thermalloy 6110 Thermalloy 7137, 7140 Thermalloy 7128
300 ft./min. (1.5m/sec)	AAVID 57302 AAVID 530600 AAVID 577202 AAVID 576802 Thermalloy 6025 Thermalloy 6109 Thermalloy 6022
200 ft./min. (1m/sec)	AAVID 575102 AAVID 574902 AAVID 523002 AAVID 504102 Thermalloy 6225 Thermalloy 6070 Thermalloy 6030 Thermalloy 6230 Thermalloy 6021, 6221 Thermalloy 7136, 7138
Natural Convection (no forced airflow)	AAVID 563202 AAVID 593202 AAVID 534302 Thermalloy 6232 Thermalloy 6032 Thermalloy 6034 Thermalloy 6234

Table 3-10. Representative Commercial Heat Sinks<br/>for the 5.0A Output Example Using a SeriesDropping Resistor (Assumptions:  $T_A = 50^{\circ}C$ , R = $0.15\Omega \pm 5\%$ ,  $I_{OUT MAX} = 5.0A$ ,  $\theta_{JC} = 2^{\circ}C/W$ ,  $\theta_{CS}$ <br/> $= 1^{\circ}C/W$ , resulting in a required  $\theta_{SA} = 8.0^{\circ}C/W$ )

## Multiple Packages on One Heat Sink

The previous calculations assume the power dissipation transferred to the heat sink emanates from a single point source. When multiple heat sources are applied, heat sink thermal performance ( $\theta_{SA}$ ) improves. Two mechanisms decrease the total effective thermal resistance:

- 1. Paralleling multiple devices reduces the effective  $\theta_{JS}$ .
- 2. Heat sink efficiency is increased due to improved heat distribution

Paralleled  $\theta_{JC}$  and  $\theta_{CS}$  terms lead to a reduction in case temperature of each regulator, since the power dissipation of each semiconductor is reduced proportionally. Distributing the heat sources, instead of a single-point source, minimizes temperature gra-

dients across the heat sink, resulting in lower conduction loss. As much as a 33% reduction in  $\theta_{SA}$  is possible with distributed heat sources.

Micrel's Super Beta PNP regulators are a natural for multiple package mounting on a single heat sink because their mounting tabs are all at ground potential. Thus, no insulator is needed between the package and the heat sink, allowing the best possible  $\theta_{CS}$ .

#### Paralleled Devices on a Heat Sink Example

An example will clarify this concept. Given a regulator that must dissipate 30W of heat, operating at an ambient temperature of 25°C, what heat sink  $\theta_{SA}$  is needed? Given the following parameters:

$$T_{J(MAX)} = 125^{\circ}C$$
  
 $\theta_{JC} = 2^{\circ}C/W$   
 $\theta_{CS} = 1^{\circ}CW$ 

#### Case 1: Single Regulator

This configuration is shown graphically in Figure 3-60.

$$\begin{split} \theta_{\text{SA}} &= \Delta T/W - (\theta_{\text{JC}} + \theta_{\text{CS}}) \\ &= (125^\circ - 25^\circ) / 30W - (2+1) \,^\circ\text{C/W} \\ \theta_{\text{SA}} &= 0.33^\circ\text{C/W} \end{split}$$

This is a very large heat sink.

Figure 3-60. Single Heat Source Thermal "Circuit"

#### Case 2: Two Paralleled Regulators

This configuration is shown graphically in Figure 3-61. The effective  $\theta_{JS}$  is reduced because the thermal resistances are connected in parallel.

$\theta_{JC'} = 1/((1/\theta_J)^2)$	C1) + (1/θ	JC2 <sup>))</sup>	
Assuming $\theta_{JC}$	$1 = \theta_{JC2}, \dagger$	then	
$\theta_{JC'} = \theta_{JC1} \div$	2 =	= 1°C/W	
$\theta_{CS'} = 1/((1/\theta_{CS'}))$	CS1 + (1/0	CS2))	
Assuming $\theta_{CS1} = \theta_{CS2}$ , then			
	0		

$$\theta_{CS}' = \theta_{CS1} \div 2 = 0.5^{\circ}C/W$$

now

$$\theta_{SA} = \Delta T/W - (\theta_{JC}' + \theta_{CS}') = 1.83^{\circ}C/W$$

With the 33% efficiency gain, we could use a heat sink with a  $\theta_{SA}$  rating as high as 2.4°C/W. This represents a tremendous reduction in heat sink size.

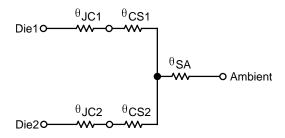


Figure 3-61. Dual Heat Source Thermal "Circuit"

#### Case 3: Multiple Paralleled Regulators

This configuration is shown graphically in Figure 3-62. For the condition of "n" paralleled heat sources, the  $\theta_{JC}$  and  $\theta_{CS}$  are reduced to 1/n their per-unit value. The heat sink needs the following rating:

$$\theta_{\mathsf{SA}} = \Delta \mathsf{T}/\mathsf{W} - ((\theta_{\mathsf{JC1}}/\mathsf{n}) + (\theta_{\mathsf{CS1}}/\mathsf{n}))$$

$$\begin{array}{c} \theta JC1 & \theta CS1 \\ \hline Die 10 & & \\ \theta JC2 & \theta CS2 \\ \hline Die 20 & & \\ \theta JC n & \theta CS n \\ \hline \end{array}$$
 Ambient

Figure 3-62. "n" Heat Source Thermal Circuit

Table 3-11 shows the reduction in heat sink performance allowed by paralleled regulators.

n	θ <sub>SA</sub>
1	0.33
2	1.83
3	2.33
4	2.58
5	2.73
6	2.83

Table 3-11. Paralleled Regulators Allow Smaller(Physical Size) Heat Sinks.  $T_A = 25^{\circ}C$ 

\_\_\_\_

Another way of looking at this situation is to ask what is the increase in maximum ambient temperature paralleled regulators allow?

$$T_{A} = T_{J(MAX)} - W \times [\theta_{SA} + (\theta_{JC}/n) + (\theta_{CS}/n)]$$

Table 3-12 shows the highest allowable  $T_A$  using the 0.33°C/W heat sink of Case 1.

n	т <sub>А</sub> (°С)	
1	25	
2	70	
3	85	
4	92	
5	97	
6	100	

Table 3-12. Highest Allowable Ambient Temperature With a 0.33°C/W Heat Sink

## Heat Sinking Surface Mount Packages

System designers increasingly face the restriction of using all surface-mounted components in their new designs—even including the power components. Through-hole components can dissipate excess heat with clip-on or bolt-on heat sinks keeping things cool. Surface mounted components do not have this flexibility and rely on the conductive traces or pads on the printed circuit board for heat transfer. We will address the question "How much PC board pad area does my design require?"

#### Example 1: TO-263 Package

We will determine if a Micrel surface mount low dropout linear regulator may operate using only a PC board pad as its heat sink. We start with the circuit requirements.

#### System Requirements:

$$V_{OUT} = 5.0V$$
  
 $V_{IN (MAX)} = 9.0V$   
 $V_{IN (MIN)} = 5.6V$   
 $I_{OUT} = 700mA$   
Duty cycle = 100%  
 $T_{A} = 50^{\circ}C$ 

This leads us to choose the 750mA MIC2937A-5.0BU voltage regulator, which has these characteristics:

 $T_{JMAX} = 125^{\circ}C$ 

 $\theta_{JC}$  of the TO-263 = 3°C/W

 $\theta_{CS}$  + 0°C/W (soldered directly to board)

#### **Preliminary Calculations**

 $V_{OUT (MIN)} = 5V - 2\% = 4.9V$   $P_{D} = (V_{IN} (MAX) - V_{OUT} (MIN))$   $\times I_{OUT} + (V_{IN} (MAX) \times I_{GND})$  $= [9V - 4.9V] \times 700mA + (9V \times 15mA) = 3W$ 

Maximum temperature rise,  $\Delta T = T_{J(MAX)} - T_A$ 

 $= 125^{\circ}C - 50^{\circ}C = 75^{\circ}C$ 

Thermal resistance requirement,  $\theta_{JA}$  (worst case):

$$\frac{\Delta T}{P_{D}} = \frac{75^{\circ}C}{3.0W} = 25^{\circ}C/W$$

Heat sink thermal resistance

$$\begin{split} \theta_{\text{SA}} &= \theta_{\text{JA}} - (\theta_{\text{JC}} + \theta_{\text{CS}}) \\ \theta_{\text{SA}} &= 25 - (3 + 0) = \textbf{22}^{\circ}\textbf{C/W} \text{ (max)} \end{split}$$

#### **Determining Heat Sink Dimensions**

Figure 3-63 shows the total area of a round or square pad, centered on the device. The solid trace represents the area of a square, single sided, horizontal, solder masked, copper PC board trace heat sink, measured in square millimeters. No airflow is assumed. The dashed line shows a heat sink covered in black oil-based paint and with 1.3m/sec (250 feet per minute) airflow. This approaches a "best case" pad heat sink.

Conservative design dictates using the solid trace data, which indicates a pad size of 5000 mm<sup>2</sup> is needed. This is a pad 71mm by 71mm (2.8 inches per side).

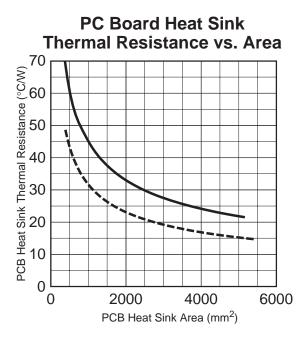


Figure 3-63. Graph to Determine PC Board Area for a Given Thermal Resistance (See text for Discussion of the Two Curves)

#### Example 2: SO-8 and SOT-223 Package

Given the following requirements, determine the safe heat sink pad area.

$$V_{OUT} = 5.0V$$
$$V_{IN (MAX)} = 14V$$
$$V_{IN (MIN)} = 5.6V$$
$$I_{OUT} = 150mA$$
Duty cycle = 100%

Your board production facility prefers handling the dual-in-line SO-8 packages whenever possible. Is the SO-8 up to this task? Choosing the MIC2951-03BM, we get these characteristics:

$$T_{J (MAX)} = 125^{\circ}C$$
  
 $\theta_{JC}$  of the SO-8 = 100°C/W

#### **SO-8 Calculations:**

 $P_D = [14V - 5V] \times 150mA + (14V \times 8mA) = 1.46W$ Temperature rise =  $125^{\circ}C - 50^{\circ}C = 75^{\circ}C$  Thermal resistance requirement,  $\theta_{JA}$  (worst case):

$$\frac{\Delta T}{P_{D}} = \frac{75^{\circ}C}{1.46W} = 51.3^{\circ}C/W$$

Heat sink  $\theta_{SA} = 51 - 100 = -49^{\circ}C/W$  (max)

The negative sign flags the problem: without refrigeration, the SO-8 is not suitable for this application. Consider the MIC5201-5.0BS in a SOT-223 package. This package is smaller than the SO-8, but its three terminals are designed for much better thermal flow. Choosing the MIC5201-3.3BS, we get these characteristics:

$$T_{J (MAX)} = 125^{\circ}C$$
  
 $\theta_{JC}$  of the SOT-223 = 15°C/W

 $\theta_{CS} = 0^{\circ}C/W$  (soldered directly to board)

#### SOT-223 Calculations:

 $P_D = [14V - 4.9V] \times 150mA + (14V \times 1.5mA)$ = **1.4W** 

Temperature rise =  $125^{\circ}C - 50^{\circ}C = 75^{\circ}C$ 

Thermal resistance requirement,  $\theta_{JA}$  (worst case):

$$\frac{\Delta T}{P_D} = \frac{75^{\circ}C}{1.4W} = 54^{\circ}C/W$$

Heat sink  $\theta_{SA} = 54 - 15 = 39^{\circ}$ C/W (max)

#### **Board Area**

Referring to Figure 3-63, a pad of 1400mm<sup>2</sup> (a square pad 1.5 inches per side) provides the required thermal characteristics.

#### Example 3: SOT-23-5 Package

A regulator for a cellular telephone must provide 3.6V at 50mA from a battery that could be as high as 6.25V. The maximum ambient temperature is 70°C and the maximum desired junction temperature is 100°C. The minimum-geometry thermal capability of the MIC5205 in the SOT-23-5 is 220°C/W; must we provide additional area for cooling?

 $P_{D}$ = [6.25 - 3.56V] × 50mA + (6.25V × 0.35mA) = 137mW

 $\frac{\Delta T}{P_D} = \frac{30^{\circ}C}{0.137W} = 219^{\circ}C/W$ 

Which is close enough to 220°C/W  $\theta_{JA}$  for our purposes. We can use the minimum-geometry layout.

If our electrical or thermal parameters worsened, we could refer to Figure 3-63 and determine the additional copper area needed for heat sinking. Use a value of  $130^{\circ}$ C/W  $\theta_{\rm LC}$  for the MIC5205-xxBM5.

## Example 4, Measurement of $\theta_{\ensuremath{\mathsf{JA}}}$ with a MSOP-8

An MIC5206-3.6BMM (in the 8-pin MSOP package) was soldered to 1oz. double-sided copper PC board material. The board, measuring 4.6 square inches, had its top layer sliced into four quadrants, corresponding to input, output, ground, and enable (see Figure 3-64), and a temperature probe was soldered close to the regulator. The device thermal shutdown temperature was measured at zero power dissipation to give an easy-to-detect temperature reference point. The device was cooled, then the load was increased until the device reached thermal shutdown. By combining  $T_A$ ,  $T_J$  (SHUTDOWN), and  $P_D$ , we may accurately determine  $\theta_{JA}$  as:

 $\theta_{JA} = (T_J (SHUTDOWN) - T_A) \div P_D$ 

For a given board size. Next, the board was trimmed to about 2 square inches and retested. Measurements were also taken at 1 and 0.5 square inches. The results are shown in Figure 3-65.

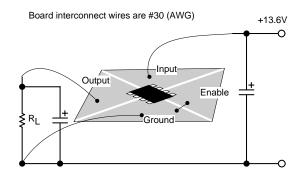


Figure 3-64. MSOP-8 Thermal Resistance Test Jig

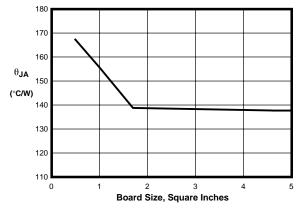


Figure 3-65. Junction to Ambient Thermal Resistance for the MSOP-8 Package

#### Comments

These formulas are provided as a general guide to thermal characteristics for surface mounted power components. Many estimations and generalizations were made; your system will vary. Please use this information as a rough approximation of board area required and fully evaluate the thermal properties of each board you design to confirm the validity of the assumptions.

# Linear Regulator Troubleshooting Guide

Problem	Possible Cause
Output Voltage Low at Heavy Load	Regulator in dropout Excessive lead resistance between regulator and load Regulator in current limit Regulator in thermal shutdown
Output Voltage Bad at Light Load	Regulator in Dropout Minimum output load current not satisfied Input voltage too high (overvoltage shutdown) Layout problem
Regulator Oscillates	Output capacitor too small (Super βeta PNP) Output capacitor ESR too small Input capacitor bad or missing Layout problems
Regulator Does Not Start	Output polarity reversed Input voltage too high (overvoltage shutdown) Load is shorted or latched up
AC Ripple on Output	Ground loop with input filter capacitor

Solutions to each of these possible causes are presented earlier in this section. If problems persist, please contact Micrel Applications Engineering for assistance.

# **Section 4. Linear Regulator Solutions**

# Super βeta PNP<sup>TM</sup> Regulators

Micrel's easy to use Super ßeta PNP<sup>™</sup> LDO monolithic regulators deliver highly accurate output voltages and are fully protected from fault conditions. Their maximum output currents range from 80mA to 7.5A. They are available in numerous fixed voltages, and most families offer adjustable versions.

Micrel's monolithic linear regulator family appears below, listed by increasing output current capability.

•

- MIC5203 80mA regulator in the tiny SOT-143 package. Fixed output voltages of 2.85, 3.0, 3.3, 3.6, 3.8, 4.0, 4.75, and 5.0V are available.
- LP2950 100mA fixed 3.3, 4.85, and 5.0V regulator available in the TO-92 package.
- LP2951 100mA fixed 5.0V and adjustable regulator available in the SO-8 package.
- MIC5200 100mA regulator available in SO-8 and SOT-223 packages. Fixed output voltages of 3.0, 3.3, 4.85, and 5.0V are available.
- MIC5202 dual 100mA version of the '5200, available in the SO-8 package.
- MIC5205 150mA low-noise fixed and adjustable regulator supplied in the small SOT-23-5 package.
- MIC5206 150mA low-noise regulator supplied in the small SOT-23-5 or MSOP-8 packages.
- MIC5207 180mA low-noise regulator supplied in the small SOT-23-5 or TO-92 packages.
- MIC2950 150mA fixed 3.3, 4.85, and 5.0V regulator available in the TO-92 package.
- MIC2951 150mA fixed 5.0V and adjustable regulator available in the SO-8 package.
- MIC5201 200mA regulator available in SO-8 and SOT-223 packages. Fixed output voltages of 3.0, 3.3, 4.85, and 5V, plus an adjustable version are available.

- MIC2920A family of 400mA regulators in TO-220, TO-263-3, SOT-223, and SO-8 packages.
   Fixed output voltages of 3.3V, 4.85V, 5V, and 12V plus three adjustable versions are available.
- MIC2937A family of 750mA regulators in TO-220 and TO-263 packages. Fixed output voltages of 3.3V, 5V, and 12V, plus two adjustable versions are available.
- MIC2940A 1250mA regulators in TO-220 and TO-263 packages with fixed output voltages of 3.3V, 5V, and 12V. The MIC2941A is an adjustable version.
- MIC29150 family of 1.5A regulators in TO-220 and TO-263 packages. Fixed output voltages of 3.3V, 5V, and 12V, plus two adjustable versions are available.
- MIC29300 family of 3A regulators in TO-220 and TO-263 packages. Fixed output voltages of 3.3V, 5V, and 12V, plus two adjustable versions are available.
- MIC29310 low-cost 3A regulator with 3.3 and 5V fixed outputs in a TO-220 package. The MIC29312 is an adjustable version.
- MIC29500 family of 5A regulators in TO-220, and TO-263 packages. Fixed output voltages of 3.3V and 5V, plus two adjustable versions are available.
- MIC29510 low-cost 5A regulator with 3.3 and 5V fixed outputs in a TO-220 package. The MIC29512 is an adjustable version.
- MIC29710 low-cost 7.5A regulator with 3.3 and 5V fixed outputs in a TO-220 package. The MIC29712 is an adjustable version.
- MIC29750 7.5A regulator in a TO-247 power package with 3.3 and 5V fixed outputs. The MIC29752 is an adjustable version.

Micrel's medium and high-current regulators (400mA and higher output current capability) have a part numbering code that denotes the additional features offered. The basic family number, ending in "A" or "0" denotes the easy-to-use three-pin fixed voltage regulator.

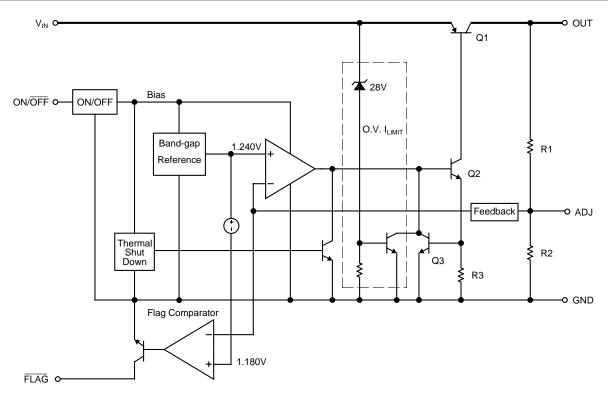


Figure 4-1. Super ßeta PNP™ Regulator Simplified Schematic Diagram

- Part numbers ending in "1" are five-pin fixed devices with a digital control pin for turning the regulator ON or OFF and an Error Flag output that signals when the output is not in regulation.
- Part numbers ending in "2" are adjustable parts with ON/OFF control.
- Devices ending with "3" are adjustables with an Error Flag.

## Super *βeta* PNP Circuitry

The simplified schematic diagram of Micrel's medium and high current monolithic LDOs appears as Figure 4-1. The high current path from input to output through the pass transistor is in bold. The bandgap reference and all other circuitry is powered via the Enable Circuit, which allows for "zero" current draw when disabled. The reference voltage is compared to the sampled output voltage fed back by R1 and R2. If this voltage is less than the bandgap reference, the op amp output increases. This increases the current through driver transistor Q2, which pulls down on the base of Q1, turning it on harder. If Q1's base current rises excessively, the voltage drop across R3 enables Q3, which in turn limits the current through Q2. Die temperature is monitored, and if it becomes excessive, the thermal shutdown circuit activates, clamping the base of Q2 and shutting down Q1. The flag circuit looks at the output voltage sample and compares it to a reference set 5% lower. If the sample is even lower, the flag comparator saturates the open collector flag transistor, signaling the fault condition.

## Dropout Voltage

The Super βeta PNP family of low-dropout regulators offers typical dropout voltages of only 300mV across the output current range. This low dropout is achieved by using large and efficient multicelled PNP output transistors, and operating them in their highbeta range well below their capacity. Dropout voltage in the Super  $\beta$  eta PNP regulators is determined by the saturation voltage of the PNP pass element. As in all bipolar transistors, the saturation voltage is proportional to the current through the transistor. At light loads, the dropout voltage is only a few tens of millivolts. At moderate output currents, the dropout rises to 200 to 300mV. At the full rated output, the typical dropout voltage is approximately 300mV for most of the families. Lower cost versions have somewhat higher dropout at full load, generally in the 400 to

500mV range. The data sheet for each device graphs typical dropout voltage versus output current.

## Ground Current

Micrel's Super  $\beta$ eta PNP process allows these high current devices to maintain very high transistor beta—on the order of 100 at their full rated current. This contrasts with competitive PNP devices that suffer with betas in the 10 to 30 range. This impacts regulator designs by reducing wasteful ground current. Micrel's beta of 100 translates into typical full load ground currents of only 1% of your output. The data sheet for each device graphs typical ground current versus output current.

When linear regulators approach dropout, generally due to insufficient input voltage, base drive to the pass transistor increases to fully saturate the transistor. With some older PNP regulators, the ground current would skyrocket as dropout approached. Micrel's Super  $\beta$ eta PNP regulators employ saturation detection circuitry which limits base drive when dropout-induced saturation occurs, limiting ground current.

## **Fully Protected**

Micrel regulators are survivors. Built-in protection features like current limiting, overtemperature shutdown, and reversed-input polarity protection allow LDO survival under otherwise catastrophic situations. Other protection features are optionally available, such as overvoltage shutdown and a digital error flag.

#### **Current Limiting**

Current limiting is the first line of defense for a regulator. It operates nearly instantaneously in the event of a fault, and keeps the internal transistor, its wire bonds, and external circuit board traces from fusing in the event of a short circuit or extremely heavy output load. The current limit operates by linearly clamping the output current in case of a fault. For example, if a MIC29150 with a 2A current limit encounters a shorted load, it will pass up to 2A of current into that load. The resulting high power dissipation (2A multiplied by the entire input voltage) causes the regulator's die temperature to rise, triggering the second line of defense, overtemperature shutdown.

#### **Overtemperature Shutdown**

As the output fault causes internal dissipation and die temperature rise, the regulator approaches its operating limits. At a predetermined high temperature, the regulator shuts off its pass element, bringing output current and power dissipation to zero. The hot die begins cooling. When its temperature drops below an acceptable temperature threshold, it automatically re-enables itself. If the load problem has been addressed, normal operation resumes. If the short persists, the LDO will begin sourcing current, will heat up, and eventually will turn off again. This sequence will repeat until the load is corrected or input power is removed. Although operation at the verge of thermal shutdown is not recommended. Micrel has tested LDOs for several million ON/OFF thermal cycles without undue die stress. In fact, during reliability testing, regulators are burned-in at the thermal shutdown-cycle limit.

#### **Reversed Input Polarity**

Protection from reversed input polarity is important for a number of reasons. Consumer products using LDOs with this feature survive batteries inserted improperly or the use of the wrong AC adapter. Automotive electronics must survive improper jump starting. All types of systems should last through initial production testing with an incorrectly inserted (backward) regulator. By using reversed input protected regulators, both the regulator and its load are protected against reverse polarity, which limits reverse current flow.

This feature may be simulated as an ideal diode, with zero forward voltage drop, in series with the output. Actually, a small current flows from the input pin to ground through the voltage divider network, but this may generally be neglected. Measured data from Super ßeta PNP regulators with a  $100\Omega$ resistor from output to ground follows:

Input Voltage (V)	Load Current (mA)
0	0
-5	0
-10	0
-15	-2.0
-20	-6.9
-25	-7.8
-30	-14

Although the devices were tested to -30V for this table without any failure, the reverse-polarity specification ranges only to -20V.

**Micrel Semiconductor** 

**Overvoltage Shutdown** 

If the input voltage rises above a certain predetermined level, generally between 35V and 40V, the control circuitry disables the output pass transistor. This feature allows the regulator to reliably survive high voltage (60V or so-see the device data sheet for the exact limit) spikes on the input regardless of output load conditions. The automotive industry calls this feature "Load-Dump Protection"<sup>1</sup> and it is crucial to reliability in automotive electronics.

Most Micrel LDOs feature overvoltage shutdown.

Many of Micrel's regulator families offer a version with a digital error flag output. The error flag monitors the output voltage and pulls its open collector (or drain) output low if the voltage is too low. The definition of "too low" ranges from about -5% to -8% below nominal output, depending upon the device type. The flag comparator is unaffected by low input voltage or a too-light or too-heavy load (although a too-heavy load generally will cause the output voltage to drop, triggering the flag).

## Variety of Packages

From the tiny SOT-143 to the large TO-247 (also known as the TO-3P), Micrel Super ßeta PNP regulators span orders of magnitude in both size and output current.

## Why Choose Five Terminal Regulators?

What do the extra pins of the five pin linear regulators provide? After all, three terminal regulators give Input, Output, and Ground; what else is necessary? Five terminal devices allow the system designer to monitor power quality to the load and digitally switch the supply ON and OFF. Power quality is indicated by a flag output. When the output voltage is within a few percent of its desired value, the flag is high, indicating the output is good. If the output drops, because of either low input voltage to the regulator or an overcurrent condition, the flag drops to signal a fault condition. A controller can monitor this output and make decisions regarding the system's readiness. For example, at initial power-up, the flag will instantaneously read high (if pulled up to an external supply), but as soon as the input supply to the regulator reaches about 2V, the flag pulls low. It stays low until the regulator output nears its desired value. With the MIC29150 family of low-dropout linear regulators, the flag rises when the output voltage reaches about 97% of the desired value. In a 3.3V system, the flag indicates "output good" with  $V_{OUT} = 3.2V$ .

Logic-compatible power control allows "sleep" mode operation and results in better energy efficiency. The ENABLE input of the MIC29150 family is TTL and 5V or 3.3V CMOS compatible. When this input is pulled above approximately 1.4V, the regulator is activated. A special feature of this regulator family is zero power consumption when inactive. Whenever the logic control input is low, all internal circuitry is biased OFF. (A tiny leakage current, measured in nanoamperes, may flow).

Three terminal regulators are used whenever ON/OFF control is not necessary and no processing power is available to respond to the flag output information. Three terminal regulators need only a single output filter capacitor minimizing design effort. Micrel three-terminal regulators all are fixed-output voltage devices with the same pin configuration: input, ground, output.

Five terminal regulators provide all the functionality of three pin devices PLUS allow power supply quality monitoring and ON/OFF switching for "sleep" mode applications.

## *Compatible Pinouts*

Micrel's MIC29150/29300/29500 and MIC29310/ 29510/29710 families of low-dropout regulators have identical pinouts throughout the line. A single board layout accommodates from 1.5A through 7.5A of maximum current, simply by replacing one LDO with another of different rating. Additionally, the three pin and five pin versions of these two families have a similarity that allows a three pin regulator to function in a socket designed for a five pin version.

Three Pin Regulator	Five Pin Regulator
_	Enable or Flag
Input	Input
Ground	Ground
Output	Output
_	Adjust or Flag

Many applications do not require the ENABLE or FLAG functions. In these cases, if a fixed voltage is suitable, a three pin LDO may be substituted in the

NOTE 1: A "load dump" fault occurs in an automobile when the battery cable breaks loose and the unfiltered alternator output powers the vehicle.

five pin socket by simply leaving the outer holes open. Use care when forming the leads; gently bend them 90° before compressing them. The plastic may crack if the leads are forced excessively.

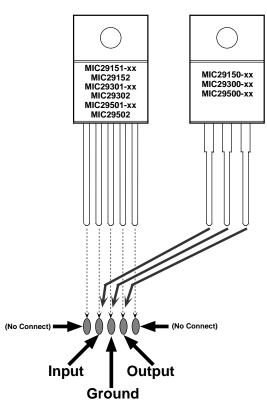


Figure 4-2. PC Board Layout for 5-Pin and 3-Pin Regulators

## Stability Issues

PNP output regulators require a minimum value of output filter capacitance for stability. The data sheet for each device specifies the minimum value of output capacitor necessary.

A stability analysis of the PNP regulators shows there are two main poles, one low internal pole at about 10Hz, and an external pole provided by the output filter capacitor. An internal zero of approximately 1.5kHz cancels the internal pole, leaving the output capacitor to provide the dominant pole for stability. Gain/phase characteristics are affected by several parameters:

- Internal design (compensation and configuration)
- Load capacitor value
- Load capacitor ESR
- Load current
- Output transistor beta
- Driver stage transconductance

Stray capacitance on the feedback pins of adjustable regulators serves to decrease the phase margin. Circuits designed for minimum output noise often intentionally add capacitance across a feedback resistor, which couples back to the feedback pin. Increasing the size of the output filter capacitor in this situation recovers the phase margin required for stability.

## Paralleling Bipolar Regulators

The most difficult aspect of using linear regulators is heat sinking. As output current and/or input-tooutput voltage differential increases, the heat sink size rapidly increases. One method of mitigating this is to split the heat into more than one point source. In **Section 3**, *Thermal Management*, using a resistor to dissipate excess power when the input voltage is much higher than the desired output was discussed, but this technique is unusable when we need low system dropout. Another method of power sharing is to parallel the regulators. This preserves their low dropout characteristics and also allows scaling to higher output currents. As also shown in *Thermal Management*, heat sinking two devices is up to 33% more efficient than sinking one at the same overall power level.

Bipolar transistors have a negative temperature coefficient of resistance; as they get hotter, they pass more current for a given voltage. This characteristic makes paralleling bipolar transistors difficult—if the transistors are not precisely matched and at identical temperatures, one will draw more current than the others. This transistor will thereby get hotter and draw even more current. This condition, known as thermal runaway, prevents equal current sharing between devices and often results in the destruction of the hottest device.

We may parallel bipolar transistors if we monitor the current through each of the devices and somehow force them to be equal. An easy and accurate method is by using current sense resistors and op amps. Figure 4-3 shows two 7.5A MIC29712 in parallel to produce a 15A composite output. One regulator is chosen as the master. Its output is adjusted to the desired voltage in the usual manner with two resistors. A small-value sense resistor samples the output for the op amp. The resistor value is chosen to provide an output voltage large enough to swamp the input offset voltage (V<sub>OS</sub>) of the op amp with medium output current. If the resistor is too small, matching will be poor; if it is too large, system dropout voltage

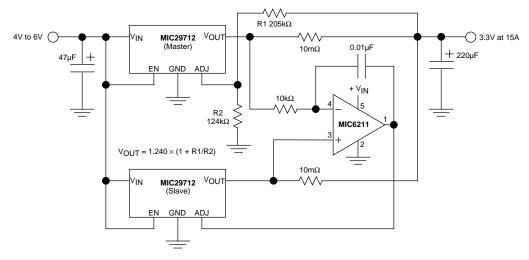


Figure 4-3. Two Super ßeta PNP Regulators in Parallel

will increase. The op amp drives the ADJ input of the slave regulator and matches its output to the master.

This technique is also applicable to three or more paralleled regulators: Figure 4-4 shows three in parallel. This may be extended to any number of devices by merely adding a sense resistor and op amp circuit to each additional slave regulator. Although a fixed regulator can be used as a master, this is not recommended. Load regulation suffers because fixed output regulators (usually) do not have a separate SENSE input to monitor load voltage. As current through the sense resistor increases, the output voltage will drop because voltage sensing occurs on the wrong side of the current sense resistor.

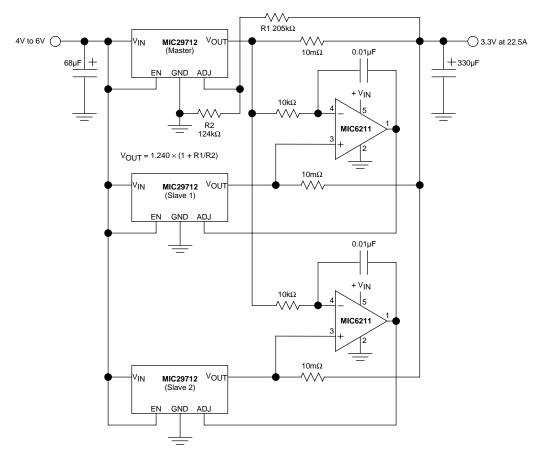
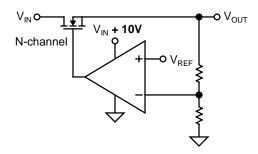


Figure 4-4. Three or More Parallel Super ßeta PNP Regulators

# Micrel's Unique "Super LDO<sup>TM</sup>"

The Super LDO<sup>™</sup> is a dedicated control IC to drive an external N-channel MOSFET pass element. It allows economical management of moderate to high output currents.

The external pass element offers the designer three advantages unattainable with the monolithic approach: First, because the control circuitry is separate, the pass element's die area in a given package can be increased. This results in lower dropout voltages at higher output currents. Second, the junctionto-case thermal resistance is much less allowing higher output currents before a heat sink is required. Third, the semiconductor process for manufacturing MOSFETs is simpler and less costly than the process needed to fabricate accurate voltage references and analog comparators. High current monolithic regulators have most of their die area dedicated to the output device; why build a large, relatively simple device on an expensive process? The Super LDO combines all three advantages to produce a high performance, low cost regulating system.



#### Figure 4-5. N-Channel Regulator

The most attractive device for the external pass element is the N-channel power MOSFET (see Figure 4-5). Discrete N-channel MOSFET prices continue to decrease (due to high volume usage), and the race for lower and lower ON resistance works in your favor. The N-channel MOSFET, like the P-channel MOSFET, reduces ground current. With device ON resistance now below  $10m\Omega$ , dropout voltages below 100mV are possible with output currents in excess of 10A. Even lower dropouts are possible by using two or more pass elements in parallel.

Unfortunately, full gate-to-source enhancement of the N-channel MOSFET requires an additional 10V to 15V above the required output voltage. Controlling the MOSFET's gate using a second higher voltage supply requires additional circuitry and is clumsy at best.

## Micrel's Super LDO Family

Micrel's Super LDO Regulator family consists of three regulators which control an external N-channel MOSFET for low dropout at high current. Two members of the family internally generate the required higher MOSFET enhancement voltage, while the other relies on an existing external supply voltage.

All members of the Super LDO Regulator family have a 35mV current limit threshold,  $\pm 2\%$  nominal output voltage setting, and a 3V to 36V operating voltage range. All family members also include a TTL compatible enable/shutdown input (EN) and an open collector fault output (FLAG). When shutdown (TTL low), the device draws less than 1µA. The FLAG output is low whenever the output voltage is 6% or more below its nominal value.

#### *The MIC5156*

The MIC5156 Super LDO Regulator occupies the least printed circuit board space in applications where a suitable voltage is available for MOSFET gate enhancement. To minimize external parts, the MIC5156 is available in fixed output versions of 3.3V or 5V. An adjustable version is also available which uses two external resistors to set the output voltage from 1.3V to 36V.

## The MIC5157 and MIC5158

For stand-alone applications the MIC5157 and MIC5158 incorporate an internal charge-pump voltage tripler to supply the necessary gate enhancement for an external N-channel MOSFET. Both devices can fully enhance a logic-level N-channel MOSFET from a supply voltage as low as 3.0V. Three inexpensive small value capacitors are required by the charge pump.

The MIC5157 output voltage is externally selected for a fixed output voltage of 3.3V, 5V or 12V.

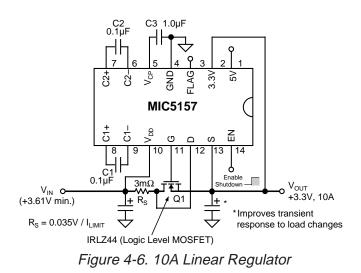
The MIC5158 output voltage is externally selectable for either a fixed 5V output or an adjustable output. Two external resistors are required to set the output voltage for adjustable operation.

## 3.3V, 10A Regulator Application

Figure 4-6 shows the MIC5157's ability to supply the additional MOSFET gate enhancement in a

#### **Micrel Semiconductor**

low dropout 3.3V, 10A supply application. Capacitors C1 and C2 perform the voltage tripling required by the N-channel logic-level MOSFETs. Improved response to load transients is accomplished by using output capacitors with low ESR characteristics. The exact capacitance value required for a given design depends on the maximum output voltage disturbance that can be tolerated during a worse case load change. Adding low-value ( $0.01\mu$ F to  $0.1\mu$ F) film capacitors (such as Wima MKS2 series) near the load will also improve the regulator's transient response.



## **Comparison With Monolithics**

#### **Similarities to Monolithics**

Like Micrel's Super ßeta PNP monolithic regulators, the Super LDO is a linear regulator. It provides a regulated and filtered output voltage from a (at least) slightly higher input source; it does not require inductors; it is available in fixed as well as user-adjustable output voltages; and it protects itself and its load by implementing current limiting. There are significant differences between the Super LDO and monolithic designs, however.

#### **Differences from Monolithics**

The differences between the Super LDO and monolithic designs is depicted in Table 4-1. The external N-channel MOSFET required by the Super LDO gives it great flexibility—by simply selecting the MOSFET, the designer may choose output current capability as well as dropout voltage. You may customize your regulator for your exact needs: the dropout voltage is simply  $V_{DO} = I \times R_{DS ON}$  and the current limit is adjustable by selecting one resistor. Also, by placing the hot pass element away from the sensitive refer-

ence and voltage comparators, better performance over the operating temperature range and much higher output currents are possible.

The Super LDO does not offer thermal shutdown protection and the pass MOSFET's tab is  $V_{OUT}$  instead of ground, unlike the Super  $\beta$ eta PNP versions.

Above approximately 5A, the Super LDO is generally the most economical regulation solution.

Super LDO	Monolithic LDO
"Any" output current	Output current set by die size
Adjustable current limit	Fixed Current limit
User-selectable dropout voltage	Dropout voltage set by die size
Better stability than PNP LDOs	
Reference temperature independent of hot pass element	Reference gets hot
Pass transistor tab is V <sub>OUT</sub>	Tab is grounded
No thermal shutdown	Thermal shutdown
Multiple component solution	Only capacitors needed

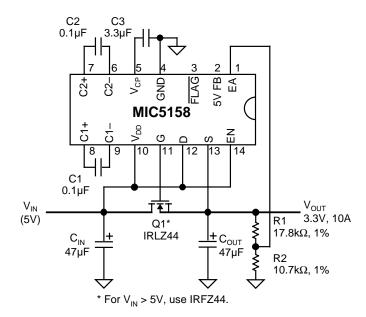
Table 4-1. Super LDO and MonolithicRegulator Comparison

## *Unique Super LDO Applications* Super High-Current Regulator

Figure 4-7 shows a linear regulator offering output current to 30A with a dropout voltage of only 330mV. Current limit is set to 45A. With proper cooling and current-limit resistor changes, this circuit scales to any arbitrary output current: 50A, 100A you name it!

Achieving the heat sinking required for the high current output mentioned above is difficult. As output current and/or input-to-output voltage differentials increase, the heat sink size rapidly increases. One technique to ease the heat sinking problem is to split the heat generators into multiple sources—by using multiple pass MOSFETs in parallel.

#### **Micrel Semiconductor**



#### Figure 4-7. A High Current Regulator Using the MIC5158

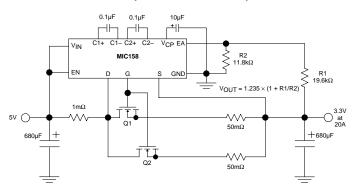
Unlike bipolar transistors, MOSFETs have a negative temperature coefficient of resistance. This makes them easier to parallel than bipolars. The MOSFET carrying more current heats up; the heat increases the channel resistance, reducing the current flow through that FET.

Unfortunately for Super LDO applications, the MOSFET threshold voltage varies from part-to-part and over the operating temperature range. Unlike power switching applications, Super LDO linear regulator operation of the pass MOSFET is in the linear region, which is at or just above the threshold. This means device-to-device threshold voltage variation causes mismatch.

If two MOSFETs are mounted on the same heat sink, it is possible to directly parallel them in less demanding applications where the maximum output current is within the rating of a single device and total power dissipation is close to that possible with a single unit.

A better solution, usable with two or more MOS-FETs in parallel, is to use ballast resistors in series with the source lead (output). Size the ballast resistors to drop a voltage equal to or a bit larger than the worst-case gate-to-source threshold voltage variation. As current flow through one MOSFET and ballast resistor increases, the ballast resistor voltage drop reduces MOSFET V<sub>GS</sub>, increasing its resistance. This Designing With LDO Regulators

reduces current flow through that MOSFET. Figure 4-8 shows an example of this technique.



#### Figure 4-8. Ballast Resistors Promote Current Sharing With Parallel MOSFETs

Lower dropout voltage and even better matching is possible using op amps to force sharing. A low current drain op amp may be powered by the  $V_{CP}$  pin of the MIC5157 or MIC5158, as shown in Figure 4-9.

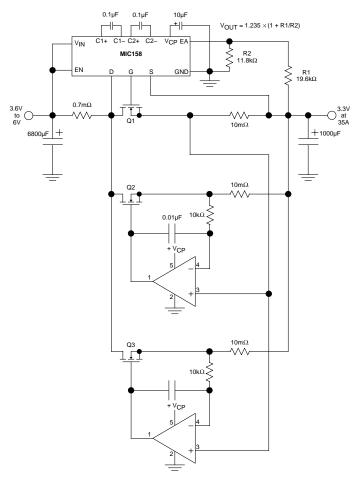


Figure 4-9. Parallel MOSFETs for High Current and/or High Power Dissipation Regulators

#### Selecting the Current Limit Threshold

By choosing one resistor value, the current limit threshold of the Super LDO is set. The resistor is chosen to drop 35mV at the desired output current limit value. While discrete resistors may be used, a more economical solution is often a length of copper wire or PC board trace used as the current sense resistor. The wire diameter or the width of the copper trace must be suitable for the current density flowing through it, and its length must provide the required resistance.

#### **Sense Resistor Power Dissipation**

The power dissipation of sense resistors used in Super LDO regulator circuits is small and generally does not require the power dissipation capability found in most low-value resistors.

#### **Kelvin Sensing**

A Kelvin, or four-lead, connection is a measurement connection that avoids the error caused by voltage drop in the high-current path leads.

Referring to Figure 4-10, sense leads are attached directly across the resistance element—intentionally excluding the power path leads. Because the sense conductors carry negligible current (sense inputs are typically high impedance voltage measurement inputs), there is no voltage drop to skew the  $E = I \times R$  measurement.

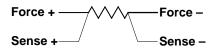


Figure 4-10. A Kelvin-sense Resistor

Manufacturers of Kelvin-sensed resistors are listed in the References section.

## Alternative Current Sense Resistors

A low-value resistor can be made from a length of copper magnet wire or from a printed circuit board trace. Tables 4-2, 4-3, and 4-4 are provided for wire and printed circuit traces.

Copper has a positive temperature coefficient of resistivity of +0.39%/°C. This can be significant when higher-accuracy current limiting is required.

A Kelvin connection between the sense element and the Super LDO Regulator Controller improves the accuracy of the current limit set-point.

Table	4-2.	Copper	Wire	Resistance
-------	------	--------	------	------------

AWG		
Wire	Resistance at 20°C 10 <sup>-6</sup> $\Omega$ / cm 10 <sup>-6</sup> $\Omega$ / in	
Size		
10	32.70	83.06
11	41.37	105.1
12	52.09	132.3
13	65.64	166.7
14	82.80	210.3
15	104.3	264.9
16	131.8	334.8
17	165.8	421.1
18	209.5	532.1
19	263.9	670.3
20	332.3	844.0
21	418.9	1064.0
22	531.4	1349.8
23	666.0	1691.6
24	842.1	2138.9
25	1062.0	2697.5
26	1345.0	3416.3
27	1687.6	4286.5
28	2142.7	5442.5
29	2664.3	6767.3
30	3402.2	8641.6
31	4294.6	10908.3
32	5314.9	13499.8
33	6748.6	17141.4
34	8572.8	21774.9
35	10849	27556.5
36	13608	34564.3
37	16801	42674.5
38	21266	54015.6
39	27775	70548.5
40	35400	89916.0
41	43405	110248.7
42	54429	138249.7
43	70308	178582.3
44	85072	216082.9

## **Overcurrent Sense Resistors from PC Board Traces**

Building the resistor from printed-circuit board (PCB) copper is attractive; arbitrary values can be provided inexpensively. The ever-shrinking world of electronic assemblies requires minimizing the physical size of this resistor which presents a power-dissipation issue. Making the resistor too small could cause excessive heat rise, leading to PCB trace damage or destruction (i.e., a fuse rather than a controlled resistor).

#### **Table 4-3 Printed Circuit Copper Resistance**

Conductor Thickness	Conductor Width (inches)	Resistance m $\Omega$ / in
0.5oz/ft <sup>2</sup>	0.025	39.3
(18µm)	0.050	19.7
	0.100	9.83
	0.200	4.91
	0.500	1.97
1 oz/ft <sup>2</sup>	0.025	19.7
(35µm)	0.050	9.83
	0.100	4.91
	0.200	2.46
	0.500	0.98
2oz/ft <sup>2</sup>	0.025	9.83
(70µm)	0.050	4.91
	0.100	2.46
	0.200	1.23
	0.500	0.49
3oz/ft <sup>2</sup>	0.025	6.5
(106µm)	0.050	3.25
	0.100	1.63
	0.200	0.81
	0.500	0.325

#### **Resistor Design Method**

Three design equations provide a resistor that occupies the minimum area. This method considers current density as it relates to heat dissipation in a surface layer resistor.

(4-1) 
$$\rho_{S}(T) = \frac{\rho \left[1 + \alpha \left(T_{A} + T_{RISE} - 20\right)\right]}{h}$$

where:

 $\begin{array}{l} \rho_{\text{S}}(\text{T}) = \text{sheet resistance at elevated temp. } (\Omega/\Box) \\ \rho = 0.0172 = \text{copper resistivity at } 20^{\circ}\text{C} \ (\Omega \bullet \mu\text{m}) \\ \alpha = 0.00393 = \text{temperature coefficient of } \rho \ (\text{per }^{\circ}\text{C}) \\ \text{T}_{\text{A}} = \text{ambient temperature } (^{\circ}\text{C}) \\ \text{T}_{\text{RISE}} = \text{allowed temperature rise } (^{\circ}\text{C}) \\ \text{h} = \text{copper trace height } (\mu\text{m}, \text{see Table 4-4}) \end{array}$ 

(4-2) 
$$W = \frac{1000I_{MAX}}{\sqrt{\frac{T_{RISE} \div \theta_{SA}}{\rho_{S}(T)}}}$$

40001

where:

w = minimum copper resistor trace width (mils)  $I_{MAX}$  = maximum current for allowed  $T_{RISE}$  (A)  $T_{RISE}$  = allowed temperature rise (°C)  $\theta_{SA}$  = resistor thermal resistance (°C × in<sup>2</sup>/W)  $\rho_s(T)$  = sheet resistance at elevated temp. ( $\Omega/\Box$ ) Note:  $\theta_{SA} \approx 55$  °C • in<sup>2</sup>/W

$$(4-3) \qquad l = \frac{wR}{\rho_{S}(T)}$$

where:

l = resistor length (mils)

w = resistor width (mils)

 $R = desired resistance (\Omega)$ 

 $\rho_s(T)$  = sheet resistance at elevated temp. ( $\Omega/\Box$ ).

PCB Weight	Copper Trac	Copper Trace Height	
(oz/ft <sup>2</sup> )	(mils)	(μm)	
1/2	0.7	17.8	
1	1.4	35.6	
2	2.8	71.1	
3	4.2	106.7	

Table 4-4. Copper Trace Heights

#### **Design Example**

Figure 4-11 is a circuit designed to produce a 3.3V, 10A output from a 5V input. Meeting the design goal of occupying minimal PC board space required minimizing sense resistor area. This resistor is shown as  $R_s$ .

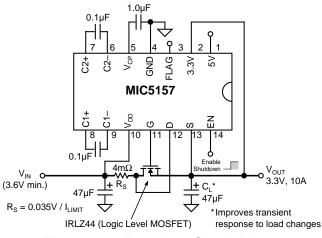


Figure 4-11. Regulator Circuit Diagram

The  $4m\Omega$  current-sensing resistor (R<sub>S</sub>) of Figure 4-11 is designed as follows: (1) based on copper trace height and an allowed temperature rise for the resistor, calculate the sheet resistance using Equation 4-1; (2) based on the maximum current the resistor will have to sustain, calculate its minimum trace width using Equation 4-2; and (3) based on the desired resistance, calculate the required trace length using Equation 4-3.

#### **Calculate Sheet Resistance**

This design uses 1 oz/ft<sup>2</sup> weight PCB material, which has a copper thickness (trace height) of 35.6 $\mu$ m. See Table 4-4. Allowing the resistor to produce a 75°C temperature rise will place it at 100°C (worst case) when operating in a 25°C ambient environment:

 $\rho_{\rm s}({\rm T}) = 635 \times 10^{-6} \,\Omega = 0.635 \,{\rm m}\Omega/\Box.$ 

#### **Calculate Minimum Trace Width**

The design example provides an output current of 5A. Because of resistor tolerance and the currentlimit trip-point specification of the MIC5158 (0.028 to 0.042V), a trip-point of 8.75A is chosen, allowing for as much as 10A of current during the sustained limiting condition:

w = 215.8 mils  $\approx$  216 mils.

#### **Calculate Required Trace Length**

The length of a  $4m\Omega$  resistor is determined via Equation 4-3 as follows:

 $l = 1360.6 \text{ mils} \approx 1361 \text{ mils}.$ 

#### **Resistor Layout**

To avoid errors caused by voltage drops in the power leads, the resistor should include Kelvin sensing leads. Figure 4-12 illustrates a layout incorporating Kelvin sensing leads.

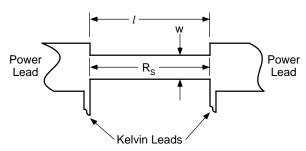


Figure 4-12. Typical Kelvin Resistor Layout

#### **Thermal Considerations**

The previous equations produce a resistance of the desired value at *elevated temperature*. It is important to consider resistance at temperature because copper has a high temperature coefficient. This design method is appropriate for current-sensing resistors because their accuracy should be optimized for the current they are intended to sense.

#### **Resistor Dimensions Spreadsheet**

A spreadsheet is available to ease the calculation process. Its source code, in Lotus 1-2-3 format, is available via e-mail from Micrel. Send a message to apps@micrel.com requesting "SENSERES.WK1"

## Design Aids

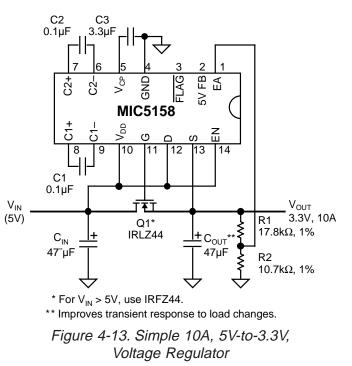
Table 4-4 provides an input needed for Equation 4-1 (trace height), and Figure 3-63 [from Section 3, *Thermal Management*] indicates that 1 in<sup>2</sup> (645 mm<sup>2</sup>) of solder-masked copper in still air has a thermal resistance of 55°C/W. Different situations; e.g., internal layers or plated copper, will have different thermal resistances. Other references include MIL-STD-275E: *Printed Wiring for Electronic Equipment*.

## Highly Accurate Current Limiting

Improving upon the accuracy of the current limit mechanism is possible. Refer to Section 3 for a description of using the Super LDO as a highly accurate adjustable current source.

## Protecting the Super LDO from Long-Term Short Circuits

Foldback current limiting is a useful feature for regulators like the Super LDO that do not have overtemperature shutdown.



A momentary short can increase power dissipation in a MOSFET voltage regulator pass device to a catastrophic level. In the circuit of Figure 4-13, normal Q1 power dissipation is  $I_{OUT} \times V_{DS}$ , or

$$(5-3.3)$$
V × 10A = 17W.

Given the 0.028 $\Omega$  R<sub>DS(ON)</sub> of the IRLZ44, if the output of the power supply is shorted, power dissipation becomes  $(V_{IN}/R_{DS(ON)})^2 \times R_{DS(ON)}$ , or an unworkable 892W. Conservative heat sink design will not help matters!

The Micrel MIC5156/5157/5158 Super LDO™ Regulator Controllers offer two features that can be used to save the pass device. The first feature is a current limit capability (not implemented in Figure 4-13). Output current can be limited at a user-defined value, but the function is not the classic foldback scheme. While fixed-value current limiting can reduce shorted-output power dissipation to a manageable level, the additional dissipation imposed by the short can still threaten the pass device. Power dissipation of a current-limited supply is the full supply voltage multiplied by the current limit of the regulator system:  $5V \times (>)$  10A > 50W. At higher input supply voltages and/or higher current limit levels, power dissipation rises rapidly—a 30V supply limited to 10A has a shortcircuit dissipation of 300W. When considerable voltage is being dropped by the pass device the shortcircuit power dissipation becomes dramatically high.

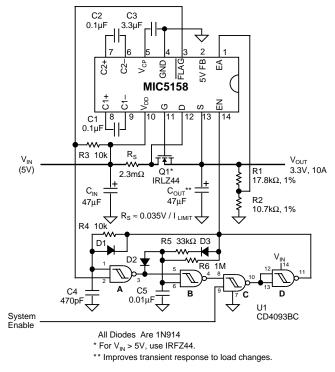
The second feature offered by the MIC5156/ 5157/5158 is an error flag. This is an open-collector output which generates a signal if the output voltage is approximately 6% or more below the intended value. This flag output is asserted logic low in the event of a shorted output, and may be used to control the enable-input pin of the regulator, disabling it upon detection of a low output voltage condition.

#### An Example

Figure 4-14 implements both the current-limit capability and a control scheme for dealing with shorted outputs. The 2.3m $\Omega$  resistor R<sub>S</sub> provides for current limiting at about 15A. Since a shorted output may be momentary, the circuitry built around U1 automatically restarts the regulator when a short is removed. Existence of a shorted output is continually monitored; the system will protect the pass device for an indefinite time. When a short exists the regulator is enabled for a very brief interval and disabled for a much longer interval. Power dissipation is reduced by this drop in duty cycle, which may be empirically designed.

#### **Circuit Description**

Schmitt-trigger NAND-gate A is used to control a gated oscillator (gate B). Resistors R5 and R6, diode D3, and capacitor C5 provide oscillator timing. With the values shown the enable time is about 110ms approximately every 2.25ms. This provides a safe 1:20 ON/OFF ratio (5% duty cycle) for reducing power dissipated by the pass device. Diode D2 keeps C5 discharged until gate A enables the oscillator. This assures that oscillation will begin with a full-width short enable pulse. Different enable and/or disable times may be appropriate for some applications. Enable time is approximately  $k1 \times R5 \times C5$ ; disable time is approximately  $k2 \times R6 \times C5$ . Constants k1 and k2 are determined primarily by the two threshold voltages ( $V_{\tau}$ + and  $V_{\tau}$ -) of Schmitt-trigger gate B. Values for k1 and k2 (empirically derived from a breadboard) are 0.33 and 0.23, respectively. Component tolerances were ignored.





#### **Getting Started**

The protection circuitry provides a system enable input. Use of this input is optional; it should be tied to  $V_{IN}$  if not required. Since the output of gate B is logic high when the oscillator is disabled, a logic-high system enable input enables the MIC5158, which immediately produces a brief logic-low flag output because initially, the output voltage is too low. Since

#### Micrel Semiconductor

the power supply output may or may not be shorted it is desirable to wait and see. The required wait-delay timing is implemented by resistor R4, capacitor C4, and diode D1. The leading-edge of the regulator enable signal is delayed (before application to gate A) for about 4ms, to attempt to span the width of the logic-low flag that is generated during a normal (nonshorted) regulator start-up.

Providing enough delay time to span the time of the flag may not always be practical, especially when starting with high-capacitance loads. If the logic-low flag is longer than the delayed enable input to gate A, the oscillator will cycle through its ON/OFF duty cycle and the circuit will again attempt a normal start-up. This will result in a slowing of the regulator turn-on, but this is not usually objectionable because it reduces turn-on surge currents.

#### Designing With LDO Regulators

After start-up, the logic-high inputs to gate A hold the oscillator off, and the system remains enabled as long as no error flag is generated. If the flag is generated due to a short, the MIC5158 remains enabled only for the time of the oscillator enable pulse and is then immediately disabled for the duration of the oscillator cycle. As long as the short exists, the oscillator runs and the system monitors the flag to detect removal of the short. Meanwhile the MOSFET stays alive, and the system again starts when the short is removed.

# Section 5. Micrel Low-Dropout Regulator Data Sheets

Monolithic Regulators	. 76
MIC2920A/29201/29202/29204 400mA Low-Dropout Voltage Regulator 76	
MIC2937A/29371/29372 750mA Low-Dropout Voltage Regulator	
MIC2940A/2941A 1.25A Low-Dropout Voltage Regulator	
LP2950/LP2951 100mA Low-Dropout Voltage Regulator 102	
MIC2950/2951 150mA Low-Dropout Voltage Regulator 116	
MIC2954 250mA Low-Dropout Voltage Regulator	
MIC29150/29300/29500/29750-Series	
High-Current Low-Dropout Regulators140	
MIC29310/29312 3A Fast-Response LDO Regulator	
MIC29510/29512 5A Fast-Response LDO Regulator	
MIC29710/29712 7.5A Fast-Response LDO Regulator	
MIC39150/39151 1.5A Low-Voltage Low-Dropout Regulator 179	
MIC39300/39301 3A Low-Voltage Low-Dropout Regulator	
MIC5200 100mA Low-Dropout Voltage Regulator 197	
MIC5201 200mA Low-Dropout Voltage Regulator	
MIC5202 Dual 100mA Low-Dropout Voltage Regulator	
MIC5203 80mA Low-Dropout Voltage Regulator	
MIC5205 150mA Low-Noise LDO Voltage Regulator	
MIC5206 150mA Low-Noise LDO Voltage Regulator	
MIC5207 180mA Low-Noise LDO Voltage Regulator	
MIC5208 Dual 50mA LDO Voltage Regulator	
MIC5209 500mA Low-Noise LDO Voltage Regulator	
MIC5210 Dual 150mA LDO Regulator	
MIC5211 Dual µCap™ 50mA LDO Voltage Regulator	
MIC5216 500mA-Peak Output LDO Voltage Regulator	
MIC5219 500mA-Peak Output LDO Voltage Regulator	
MIC5237 500mA Low-Dropout Voltage Regulator	
LDO Regulator Controller ICs	310
MIC5156/5157/5158 Super LDO™ Regulator Controller	



# MIC2920A/29201/29202/29204

400mA Low-Dropout Voltage Regulator

### **General Description**

The MIC2920A family are "bulletproof," efficient voltage regulators with very low dropout voltage (typically 40mV at light loads and 370mV at 250mA), and very low quiescent current (140 $\mu$ A typical). The quiescent current of the MIC2920A increases only slightly in dropout, prolonging battery life. Key MIC2920A features include protection against reversed battery, fold-back current limiting, and automotive "load dump" protection (60V positive transient).

The MIC2920 is available in several configurations. The MIC2920A-x.x devices are three pin fixed voltage regulators available in 3.3V, 4.85V, 5V, and 12V outputs. The MIC29201 is a fixed regulator offering a logic compatible ON/OFF (shutdown) input and an error flag output. This flag may also be used as a power-on reset signal. A logic-compatible shutdown input is provided on the adjustable MIC29202 which allows the regulator to be switched on and off. The MIC29204 8-pin SOIC adjustable regulator includes both shutdown and error flag pins and may be pin-strapped for 5V output or programmed from 1.24V to 26V using two external resistors.

### **Features**

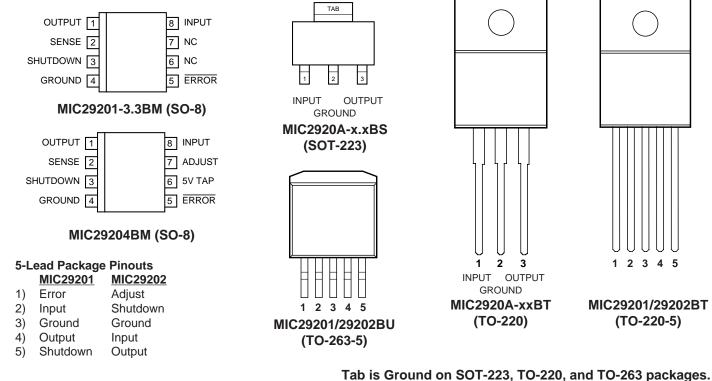
•

- High output voltage accuracy
- Guaranteed 400mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Input withstands –20V reverse battery and 60V positive transients
- Error flag warns of output dropout
- Logic-controlled electronic shutdown
- Output programmable from 1.24V to 26V (MIC29202/MIC29204)
- Available in TO-220, TO-220-5, and surface-mount TO-263-5, SOT-223, and SO-8 packages.

### Applications

- Battery-powered equipment
- Cellular telephones
- Laptop, notebook, and palmtop computers
- PCMCIA V<sub>cc</sub> and V<sub>PP</sub> regulation/switching
- Bar code scanners
- Automotive electronics
- SMPS post-regulators
- Voltage reference
- High-efficiency linear power supplies

### **Pin Configuration**



Ordering Information					
Part Number	Voltage	Temperature Range*	Package		
MIC2920A-3.3BS	3.3V	–40°C to +125°C	SOT-223		
MIC2920A-3.3BT	3.3V	–40°C to +125°C	TO-220		
MIC2920A-4.8BS	4.85V	–40°C to +125°C	SOT-223		
MIC2920A-4.8BT	4.85V	–40°C to +125°C	TO-220		
MIC2920A-5.0BS	5.0V	–40°C to +125°C	SOT-223		
MIC2920A-5.0BT	5.0V	–40°C to +125°C	TO-220		
MIC2920A-12BS	12V	–40°C to +125°C	SOT-223		
MIC2920A-12BT	12V	–40°C to +125°C	TO-220		
MIC29201-3.3BM	3.3V	–40°C to +125°C	SO-8		
MIC29201-3.3BT	3.3V	–40°C to +125°C	TO-220-5		
MIC29201-3.3BU	3.3V	–40°C to +125°C	TO-263-5		
MIC29201-4.8BT	4.85V	–40°C to +125°C	TO-220-5		
MIC29201-4.8BU	4.85V	–40°C to +125°C	TO-263-5		
MIC29201-5.0BT	5.0V	–40°C to +125°C	TO-220-5		
MIC29201-5.0BU	5.0V	–40°C to +125°C	TO-263-5		
MIC29201-12BT	12V	–40°C to +125°C	TO-220-5		
MIC29201-12BU	12V	–40°C to +125°C	TO-263-5		
MIC29202BT	Adj	–40°C to +125°C	TO-220-5		
MIC29202BU	Adj	–40°C to +125°C	TO-263-5		
MIC29204BM	5V and Adj	–40°C to +125°C	SO-8		
MIC29204BN	5V and Adj	–40°C to +125°C	8-pin PDIP		

### Absolute Maximum Ratings

If Military/Aerospace specified devices are required, contact your local Micrel representative/distributor for availability and specifications.

Power Dissipation ..... Internally Limited, Note 1

Lead Temperature (Soldering, 5 seconds) ....... 260°C Storage Temperature Range ........... -65°C to +150°C Operating Junction Temperature Range

–40°C te	o +125°C
Thermal Characteristics:	
SOT–223 θ <sub>μ</sub>	. 15°C/W
TO-220 θ <sub>IC</sub>	3°C/W
TO-263 θ <sub>ic</sub>	3°C/W
8-Pin SOΙČ θ <sub>μ</sub>	
Input Supply Voltage20\	/ to +60V
Operating Input Supply Voltage2	V <sup>†</sup> to 26V
Adjust Input Voltage (Notes 9 and 10)	
–1.5\	/ to +26V
Shutdown Input Voltage0.3\	/ to +30V
Error Comparator Output Voltage0.3	/ to +30V

<sup>†</sup> Across the full operating temperature, the minimum input voltage range for full output current is 4.3V to 26V. Output will remain in-regulation at lower output voltages and low current loads down to an input of 2V at 25°C.

\* Junction temperatures

### **Electrical Characteristics**

Limits in standard typeface are for  $T_J = 25^{\circ}$ C and limits in **boldface** apply over the full operating temperature range. Unless otherwise specified,  $V_{IN} = V_{OUT} + 1V$ ,  $I_L = 1$ mA,  $C_L = 10\mu$ F. Adjustable version are set for an output of 5V. The MIC29202  $V_{SHUTDOWN} \le 0.7V$ . The eight pin MIC29204 is configured with the Adjust pin tied to the 5V Tap, the Output is tied to Output Sense ( $V_{OUT} = 5V$ ), and  $V_{SHUTDOWN} \le 0.7V$ .

Symbol	Parameter	Conditions	Min	Typical	Мах	Units
Vo	Output Voltage	Variation from factory trimmed $V_{OUT}$	-1		1	%
	Accuracy		-2		2	4
		$1\text{mA} \le \text{I}_{\text{L}} \le 400\text{mA}$ , across temp. range	-2.5		2.5	_
		MIC2920A-12 and 29201-12 only	-1.5		1.5 <b>3</b>	
		$1\text{mA} \le I_1 \le 400\text{mA}$ , across temp. range	-3 -4		4	-
$\Delta V_{o}$	Output Voltage	(Note 2)		20	100	ppm/°C
$\frac{\Delta V_o}{\Delta T}$	Temperature Coef.	V <sub>out</sub> > 10V only		80	350	1
Δνο	Line Regulation	$V_{\rm IN} = V_{\rm OUT} + 1V$ to 26V	1	0.03	0.10	%
$\frac{\Delta V_{o}}{V_{o}}$ $\frac{\Delta V_{o}}{V_{o}}$					0.40	
$\Delta V_o$	Load Regulation	$I_{L} = 1$ to 250mA (Note 3)		0.04	0.16	%
Vo					0.30	
$V_{IN} - V_{O}$	Dropout Voltage	I, = 1mA		100	150	mV
IN O	(Note 4)			100	180	
		I, = 100mA		250		
		V <sub>out</sub> > 10V only		350		
		I, = 250mA		370		
		V <sub>OUT</sub> > 10V only		500		
		$I_{L} = 400 \text{mA}$		450	600	
					750	
	Ground Pin Current	I, = 1mA		140	200	μΑ
GND	(Note 5)				300	
		I <sub>1</sub> = 100mA		1.3	2	mA
		-			2.5	
		I <sub>L</sub> = 250mA		5	9	
					12	
		I <sub>L</sub> = 400mA		13	15	
1	Ground Pin	$V_{IN} = 0.5V$ less than designed $V_{OUT}$		180	400	μA
GNDDO	Current at Dropout	$(V_{OUT} \ge 3.3V)$				
	(Note 5)	$I_{o} = 1mA$				
	0			405	1000	
LIMIT	Current Limit	$V_{OUT} = 0V$		425	1000	mA
		(Note 6)			1200	
$\Delta V_{o}$	Thermal Regulation	(Note 7)		0.05	0.2	%/W
$\frac{\Delta V_{o}}{\Delta P_{d}}$	, v					
		C = 10µE		400		μV RMS
e <sub>n</sub>	Output Noise Voltage	$C_{L} = 10 \mu F$		400		
	(10Hz to 100kHz)	C, = 100μF		260		

Parameter	Conditions	Min	Тур	Max	Units
Reference Voltage	MIC29202	1.223 <b>1.210</b>	1.235	1.247 <b>1.260</b>	V
Reference Voltage	MIC29202 (Note 8)	1.204		1.266	V
Reference Voltage	MIC29204	1.210 <b>1.200</b>	1.235	1.260 <b>1.270</b>	V
Reference Voltage	MIC29204 (Note 8)	1.185		1.285	V
Adjust Pin Bias Current			20	40 <b>60</b>	nA
Reference Voltage Temperature Coefficient	(Note 7)		20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C
Error Comparator	MIC29201, MIC29204	•			
Output Leakage Current	V <sub>OH</sub> = 26V		0.01	1.00 <b>2.00</b>	μA
Output Low Voltage	$V_{IN} = 4.5V$ $I_{OL} = 250\mu A$		150	250 <b>400</b>	mV
Upper Threshold Voltage	(Note 9)	40 <b>25</b>	60		mV
Lower Threshold Voltage	(Note 9)		75	95 <b>140</b>	mV
Hysteresis	(Note 9)		15		mV
Shutdown Input	MIC29201, MIC29202, MIC29204	•			
Input Logic Voltage	Low (ON) High (OFF)	2.0	1.3	0.7	V
Shutdown Pin Input Current	V <sub>SHUTDOWN</sub> = 2.4V		30	50 <b>100</b>	μA
	V <sub>SHUTDOWN</sub> = 26V		450	600 <b>750</b>	μΑ
Regulator Output Current in Shutdown	(Note 10)		3	10 <b>20</b>	μA

**General Note:** Devices are ESD protected; however, handling precautions are recommended.

Note 1: Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J_{(MAX)}}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{(MAX)} = (T_{J_{(MAX)}} - T_A) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The junction to ambient thermal resistance of the MIC29204BM is 160°C/W mounted on a PC board.

Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range. Note 2:

Note 3: Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

Dropout Voltage is defined as the input to output differential at which the output voltage drops 100mV below its nominal value Note 4: measured at 1V differential. At low values of programmed output voltage, the minimum input supply voltage of 4.3V over temperature must be taken into account. The MIC2920A operates down to 2V of input at reduced output current at 25°C.

Note 5: Ground pin current is the regulator guiescent current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

Note 6: The MIC2920A features fold-back current limiting. The short circuit (V<sub>out</sub> = 0V) current limit is less than the maximum current with normal output voltage.

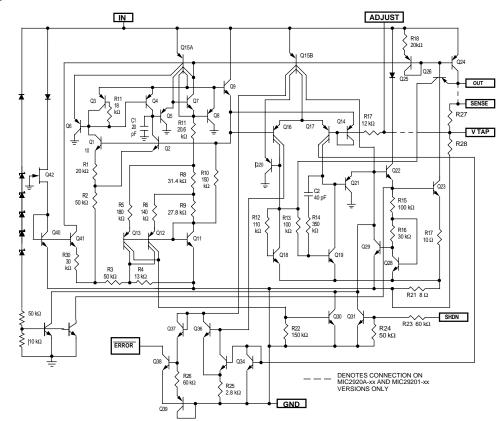
Note 7: Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 200mA load pulse at  $V_{IN}$  = 20V (a 4W pulse) for T = 10ms.

Note 8:

 $V_{REF} \le V_{OUT} \le (V_{IN} - 1 V), 4.3V \le V_{IN} \le 26V, 1 mA < I_L \le 400 mA, T_J \le T_{J MAX.}$ Comparator thresholds are expressed in terms of a voltage differential at the Adjust terminal below the nominal reference voltage Note 9: measured at 6V input. To express these thresholds in terms of output voltage change, multiply by the error amplifier gain = V<sub>OUT</sub> /V<sub>REE</sub> = (R1 + R2)/R2. For example, at a programmed output voltage of 5V, the Error output is guaranteed to go low when the output drops by 95 mV x 5V/1.235 V = 384 mV. Thresholds remain constant as a percent of VOUT as VOUT is varied, with the dropout warning occurring at typically 5% below nominal, 7.7% guaranteed.

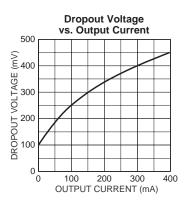
**Note 10:**  $V_{SHUTDOWN} \ge 2V$ ,  $V_{IN} \le 26V$ ,  $V_{OUT} = 0$ , with Adjust pin tied to 5V Tap or to the R1, R2 junction (see Figure 3) with R1  $\ge 150$ k $\Omega$ . **Note 11:** When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

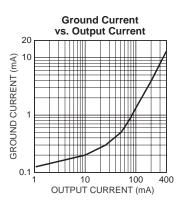
Note 12: Maximum positive supply voltage of 60V must be of limited duration (< 100ms) and duty cycle (< 1%). The maximum continuous supply voltage is 26V.

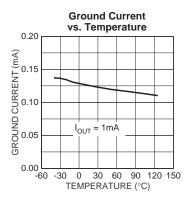


#### Schematic Diagram

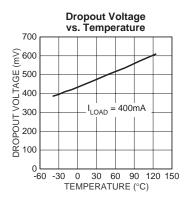
# **Typical Characteristics**

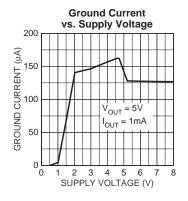






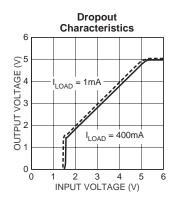
Fixed 3.3V Output Voltage ys. Temperature 3.40 3.38 3.36 3.36 3.34 3.32 3.30 3.32 3.30 5.3.20 5.22 3.20 60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

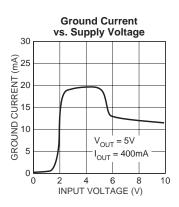




3

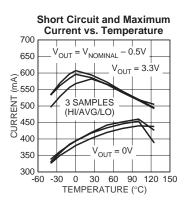
GROUND CURRENT (mA)

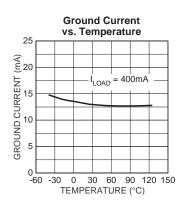


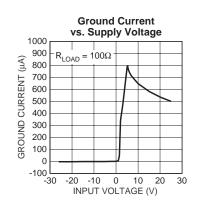


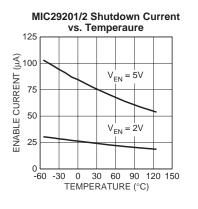
Ground Current vs. Temperature

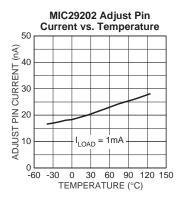
0 -60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

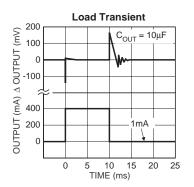


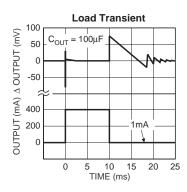


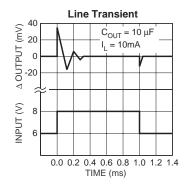


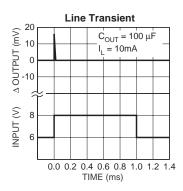


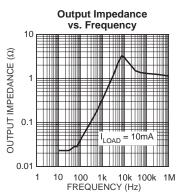


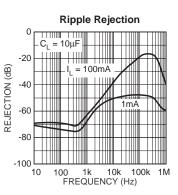












### **Applications Information**

#### **External Capacitors**

A  $10\mu$ F (or greater) capacitor is required between the MIC2920A output and ground to prevent oscillations due to instability. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, so solid tantalums are recommended for operation below  $-25^{\circ}$ C. The important parameters of the capacitor are an effective series resistance of about  $5\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $2.2\mu$ F for current below 10mA or  $1\mu$ F for currents below 1mA. Adjusting the MIC29202/29204 to voltages below 5V runs the error amplifier at lower gains so that more output capacitance is needed. For the worst-case situation of a 500mA load at 1.23V output (Output shorted to Adjust) a 47 $\mu$ F (or greater) capacitor should be used.

The MIC2920A/29201 will remain in regulation with a minimum load of 1mA. When setting the output voltage of the MIC29202/29204 versions with external resistors, the current through these resistors may be included as a portion of the minimum load.

A  $0.1\mu$ F capacitor should be placed from the MIC2920A input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

# Error Detection Comparator Output (MIC29201/MIC29204)

A logic low output will be produced by the comparator whenever the MIC29201/29204 output falls out of regulation by more than approximately 5%. This figure is the comparator's builtin offset of about 75mV divided by the 1.235V reference voltage. (Refer to the block diagram on Page 1). This trip level remains "5% below normal" regardless of the programmed output voltage of the MIC29201/29204. For example, the error flag trip level is typically 4.75V for a 5V output or 11.4V for a 12V output. The out of regulation condition may be due either to low input voltage, extremely high input voltage, current limiting, or thermal limiting.

Figure 1 is a timing diagram depicting the ERROR signal and the regulated output voltage as the MIC29201/29204 input is ramped up and down. The ERROR signal becomes valid (low) at about 1.3V input. It goes high at about 5V input (the input voltage at which  $V_{OUT} = 4.75$ ). Since the MIC29201/29204's dropout voltage is load-dependent (see curve in Typical Performance Characteristics), the input voltage trip point (about 5V) will vary with the load current. The output voltage trip point (approximately 4.75V) does not vary with load.

The error comparator has an NPN open-collector output which requires an external pull-up resistor. Depending on

system requirements, this resistor may be returned to the 5V output or some other supply voltage. In determining a value for this resistor, note that while the output is rated to sink  $250\mu$ A, this sink current adds to battery drain in a low battery condition. Suggested values range from 100k to  $1M\Omega$ . The resistor is not required if this output is unused.

#### Programming the Output Voltage (MIC29202/29204)

The MIC29202/29204 may be programmed for any output voltage between its 1.235V reference and its 26V maximum rating, using an external pair of resistors, as shown in Figure 3.

The complete equation for the output voltage is

$$V_{OUT} = V_{REF} \times \{ 1 + R_1/R_2 \} - |I_{FB}| R_1$$

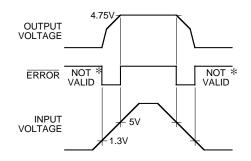
where V<sub>REF</sub> is the nominal 1.235 reference voltage and I<sub>FB</sub> is the Adjust pin bias current, nominally 20nA. The minimum recommended load current of 1µA forces an upper limit of 1.2MΩ on the value of R<sub>2</sub>, if the regulator must work with no load (a condition often found in CMOS in standby), I<sub>FB</sub> will produce a –2% typical error in V<sub>OUT</sub> which may be eliminated at room temperature by trimming R<sub>1</sub>. For better accuracy, choosing R<sub>2</sub> = 100k reduces this error to 0.17% while increasing the resistor program current to 12µA. Since the MIC29202/29204 typically draws 110µA at no load with SHUTDOWN open-circuited, this is a negligible addition. The MIC29204 may be pin-strapped for 5V using the internal voltage divider by tying Pin 1 (output) to Pin 2 (sense) and Pin 7 (Adjust) to Pin 6 (V Tap).

#### Configuring the MIC29201-3.3BM

For the MIC29201-3.3BM, the output (Pin 1) and sense pin (pin 2), *must* be connected to ensure proper operation. They are not connected internally.

#### **Reducing Output Noise**

In reference applications it may be advantageous to reduce the AC noise present at the output. One method is to reduce the regulator bandwidth by increasing the size of the output



\* SEE APPLICATIONS INFORMATION

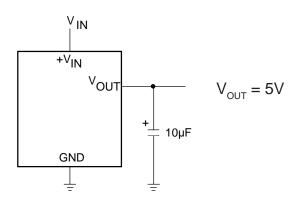
Figure 1. ERROR Output Timing

capacitor. This is relatively inefficient, as increasing the capacitor from 1µF to 220µF only decreases the noise from 430µV to 160µV<sub>RMS</sub> for a 100kHz bandwidth at 5V output. Noise can be reduced fourfold by a bypass capacitor across R<sub>1</sub>, since it reduces the high frequency gain from 4 to unity. Pick  $C_{\text{BYPASS}} \cong \underbrace{1}$ 

BYPASS 
$$\cong \frac{1}{2\pi R_1 \cdot 200 \text{ Hz}}$$

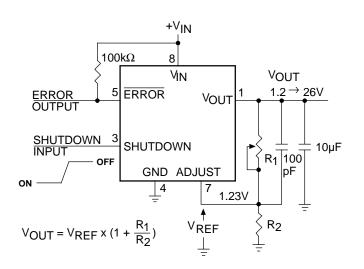
or about 0.01 $\mu$ F. When doing this, the output capacitor must be increased to 10 $\mu$ F to maintain stability. These changes reduce the output noise from 430 $\mu$ V to 100 $\mu$ V rms for a 100kHz bandwidth at 5V output. With the bypass capacitor added, noise no longer scales with output voltage so that improvements are more dramatic at higher output voltages.

### **Typical Applications**



Automotive Applications

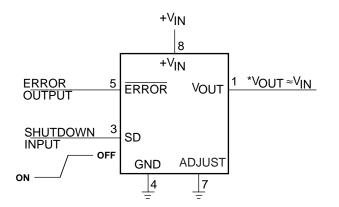
The MIC2920A is ideally suited for automotive applications for a variety of reasons. It will operate over a wide range of input voltages with very low dropout voltages (40mV at light loads), and very low quiescent currents (100µA typical). These features are necessary for use in battery powered systems, such as automobiles. It is a "bulletproof" device with the ability to survive both reverse battery (negative transients up to 20V below ground), and load dump (positive transients up to 60V) conditions. A wide operating temperature range with low temperature coefficients is yet another reason to use these versatile regulators in automotive designs.



NOTE: PINS 2 AND 6 ARE LEFT OPEN

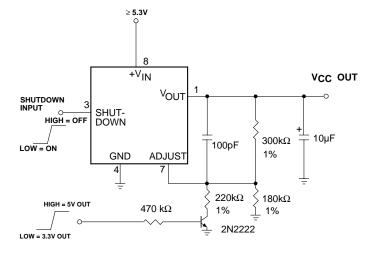
Figure 2. MIC2920A-5.0 Fixed +5V Regulator

Figure 3. MIC29202/29204 Adjustable Regulator. Pinout is for MIC29204.



\*MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT.

#### Figure 4. MIC29204 Wide Input Voltage Range Current Limiter



PIN 3 LOW= ENABLE OUTPUT. Q1 ON = 3.3V, Q1 OFF = 5.0V.

Figure 5. MIC29202/29204 5.0V or 3.3V Selectable Regulator with Shutdown. Pinout is for MIC29204.



# MIC2937A/29371/29372

### 750mA Low-Dropout Voltage Regulator

### **General Description**

The MIC2937A family are "bulletproof" efficient voltage regulators with very low dropout voltage (typically 40mV at light loads and 300mV at 500mA), and very low quiescent current (160 $\mu$ A typical). The quiescent current of the MIC2937A increases only slightly in dropout, thus prolonging battery life. Key MIC2937A features include protection against reversed battery, fold-back current limiting, and automotive "load dump" protection (60V positive transient).

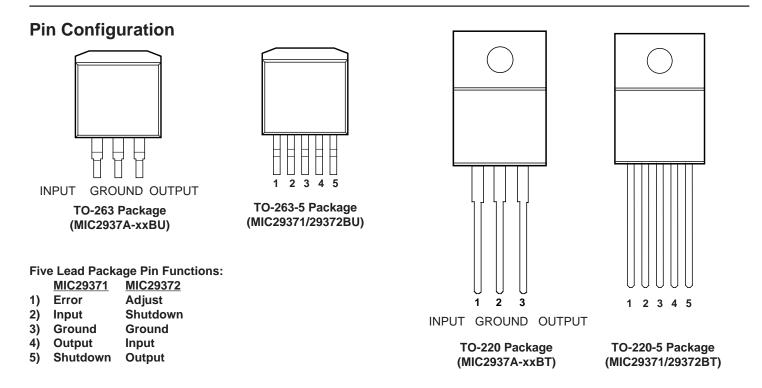
The MIC2937 is available in several configurations. The MIC2937A-xx devices are three pin fixed voltage regulators with 3.3V, 5V, and 12V outputs available. The MIC29371 is a fixed regulator offering logic compatible ON/OFF switching input and an error flag output. This flag may also be used as a power-on reset signal. A logic-compatible shutdown input is provided on the adjustable MIC29372, which enables the regulator to be switched on and off.

#### Features

- High output voltage accuracy
- Guaranteed 750mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Input can withstand –20V reverse battery and +60V positive transients
- Error flag warns of output dropout
- Logic-controlled electronic shutdown
- Output programmable from 1.24V to 26V(MIC29372)
- Available in TO-220, TO-263, TO-220-5, and TO-263-5 packages.

### Applications

- Battery Powered Equipment
- Cellular Telephones
- Laptop, Notebook, and Palmtop Computers
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> Regulation/Switching
- Bar Code Scanners
- Automotive Electronics
- SMPS Post-Regulator/ DC to DC Modules
- High Efficiency Linear Power Supplies



The TAB is Ground on the TO-220 and TO-263 packages.

Ordering Information					
Part Number	Voltage	Temperature Range*	Package		
MIC2937A-3.3BU	3.3	–40°C to +125°C	TO-263-3		
MIC2937A-3.3BT	3.3	–40°C to +125°C	TO-220		
MIC2937A-5.0BU	5.0	–40°C to +125°C	TO-263-3		
MIC2937A-5.0BT	5.0	–40°C to +125°C	TO-220		
MIC2937A-12BU	12	–40°C to +125°C	TO-263-3		
MIC2937A-12BT	12	–40°C to +125°C	TO-220		
MIC29371-3.3BT	3.3	–40°C to +125°C	TO-220-5		
MIC29371-3.3BU	3.3	–40°C to +125°C	TO-263-5		
MIC29371-5.0BT	5.0	–40°C to +125°C	TO-220-5		
MIC29371-5.0BU	5.0	–40°C to +125°C	TO-263-5		
MIC29371-12BT	12	–40°C to +125°C	TO-220-5		
MIC29371-12BU	12	–40°C to +125°C	TO-263-5		
MIC29372BT	Adj	–40°C to +125°C	TO-220-5		
MIC29372BU	Adj	–40°C to +125°C	TO-263-5		

### Absolute Maximum Ratings

If Military/Aerospace specified devices are required, contact your local Micrel representative/distributor for availability and specifications.

	5 1	0
		–40°C to +125°C
	οθ <sub>.IC</sub>	
TO-263	3 θ <sub>JC</sub>	2.5°C/W
	Supply Voltage	
Operati	ing Input Supply Voltage	2V <sup>†</sup> to 26V
Adjust	Input Voltage (Notes 9 and	110)
		1.5V to +26V
Shutdo	wn Input Voltage	0.3V to +30V
Error C	comparator Output Voltage	0.3V to +30V

<sup>†</sup> Across the full operating temperature, the minimum input voltage range for full output current is 4.3V to 26V. Output will remain in-regulation at lower output voltages and low current loads down to an input of 2V at 25°C.

\* Junction temperatures

### **Electrical Characteristics**

Limits in standard typeface are for  $T_J = 25^{\circ}C$  and limits in **boldface** apply over the full operating temperature range. Unless otherwise specified,  $V_{IN} = V_{OUT} + 1V$ ,  $I_L = 5mA$ ,  $C_L = 10\mu$ F. The MIC29372 are programmed for a 5V output voltage, and  $V_{SHUTDOWN} \le 0.6V$  (MIC29271-xx and MIC29372 only).

Symbol	Parameter	Conditions	Min	Typical	Max	Units
Vo	Output Voltage	Variation from factory trimmed V <sub>out</sub>	-1		1	%
	Accuracy		-2		2	_
		$5mA \le I_{L} \le 500mA$	-2.5		2.5	_
		MIC2937A-12 and 29371-12 only:	-1.5		1.5 2	
		$5mA \le I_1 \le 500mA$	-3		<u>3</u> 4	-
ΔVo	Output Voltage	(Note 2)		20	100	ppm/°C
$\Delta T$	Temperature Coef.	Output voltage > 10V		80	350	· ·
$ \frac{\Delta V_{o}}{\Delta T} $ $ \frac{\Delta V_{o}}{V_{o}} $ $ \frac{\Delta V_{o}}{V_{o}} $	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 26V		0.03	0.10 <b>0.40</b>	%
$\Delta V_{0}$	Load Regulation	$I_{L} = 5 \text{ to } 500 \text{mA}$		0.04	0.16	%
V <sub>o</sub>		(Note 3)			0.30	
$V_{IN} - V_{O}$	Dropout Voltage	I <sub>L</sub> = 5mA		80	150	mV
	(Note 4)				180	
		$I_{L} = 100 \text{mA}$		200		
		Output voltage > 10V		240		
		I <sub>L</sub> = 500mA Output voltage > 10V		300 420		
		I, = 750mA		370	600	
					750	
I <sub>GND</sub>	Ground Pin Current	I <sub>L</sub> = 5mA		160	250	μΑ
	(Note 5)				300	
		I <sub>L</sub> = 100mA		1	2.5	mA
		L 500 A			3	
		I <sub>L</sub> = 500mA		8	13	
		I, = 750mA		15	<b>16</b> 25	
		-		15	25	
	Ground Pin	$V_{IN}$ = 0.5V less than designed $V_{OUT}$		200	500	μΑ
	Current at Dropout (Note 5)	$(V_{OUT} \ge 3.3V)$ I <sub>O</sub> = 5mA				
ILIMIT	Current Limit	$V_{OUT} = 0V$ (Note 6)		1.1	1.5 <b>2</b>	A
	Thermal Regulation	(Note 7)		0.05	0.2	%/W
$\frac{\Delta V_{O}}{\Delta P_{D}}$				0.00	0.2	
e <sub>n</sub>	Output Noise Voltage	$C_L = 10\mu F$		400		μV RMS
	(10Hz to 100kHz)	C, = 100μF		260		
	$I_1 = 100 \text{mA}$					
	<u>с</u>					

# Electrical Characteristics (Continued)

MIC29372

			,		
Parameter	Conditions	Min	Typical	Мах	Units
Reference Voltage		1.223 <b>1.210</b>	1.235	1.247 <b>1.260</b>	V V max
Reference Voltage	(Note 8)	1.204		1.266	V
Adjust Pin Bias Current			20	40 <b>60</b>	nA
Reference Voltage Temperature Coefficient	(Note 7)		20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C
Error Comparator	MIC29371				
Output Leakage Current	V <sub>OH</sub> = 26V		0.01	1.00 <b>2.00</b>	μA
Output Low Voltage	V <sub>IN</sub> = 4.5V I <sub>OL</sub> = 250µA		150	250 <b>400</b>	mV
Upper Threshold Voltage	(Note 9)	40 <b>25</b>	60		mV
Lower Threshold Voltage	(Note 9)		75	95 <b>140</b>	mV
Hysteresis	(Note 9)		15		mV
Shutdown Input	MIC29371/MIC29372				
Input Logic Voltage Low (ON)	High (OFF)	2.0	1.3	0.7	V
Shutdown Pin Input Current	V <sub>SHUTDOWN</sub> = 2.4V		30	50 <b>100</b>	μA
	V <sub>SHUTDOWN</sub> = 26V		450	600 <b>750</b>	μA
Regulator Output Current in Shutdown	(Note 10)		3	10 <b>20</b>	μΑ

Note 1: Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J_{(MAX)}}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{(MAX)} = (T_{J_{(MAX)}} - T_A) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown.

Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range. Note 2:

Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to Note 3: heating effects are covered by the thermal regulation specification.

Note 4: Dropout Voltage is defined as the input to output differential at which the output voltage drops 100 mV below its nominal value measured at 1V differential. At low values of programmed output voltage, the minimum input supply voltage of 4.3V over temperature must be taken into account. The MIC2937A operates down to 2V of input at reduced output current at 25°C.

Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus Note 5: the ground pin current.

The MIC2937A family features fold-back current limiting. The short circuit (V<sub>OUT</sub> = 0V) current limit is less than the maximum current Note 6: with normal output voltage.

Note 7: Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 200mA load pulse at  $V_{IN}$  = 20V (a 4W pulse) for T = 10ms.

Note 8:

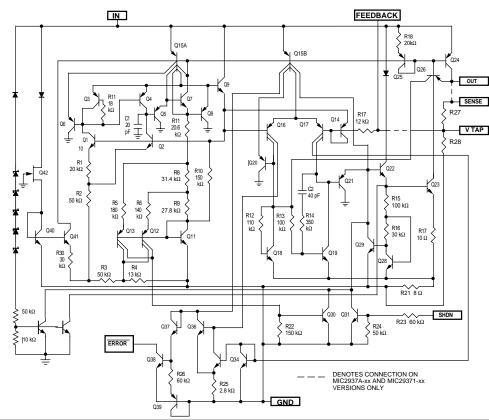
 $V_{REF} \le V_{OUT} \le (V_{IN} - 1 V), 4.3V \le V_{IN} \le 26V, 5mA < I_{L} \le 750 mA, T_{J} \le T_{J MAX.}$ Comparator thresholds are expressed in terms of a voltage differential at the Adjust terminal below the nominal reference voltage Note 9: measured at 6V input (for a 5V regulator). To express these thresholds in terms of output voltage change, multiply by the error amplifier gain = V<sub>OUT</sub> /V<sub>REF</sub> = (R1 + R2)/R2. For example, at a programmed output voltage of 5V, the Error output is guaranteed to go low when the output drops by 95 mV x 5V/1.235 V = 384 mV. Thresholds remain constant as a percent of VOUT as VOUT is varied, with the dropout warning

occurring at typically 5% below nominal, 7.7% guaranteed.

Note 10: Circuit of Figure 3 with R1  $\geq$  150k $\Omega.$  V<sub>SHUTDOWN</sub>  $\geq$  2V and V<sub>IN</sub>  $\leq$  26V,V<sub>OUT</sub> = 0.

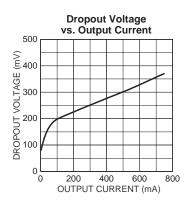
Note 11: When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

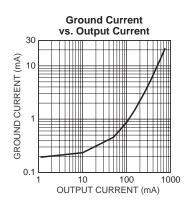
Note 12: Maximum positive supply voltage of 60V must be of limited duration (< 100ms) and duty cycle (< 1%). The maximum continuous supply voltage is 26V.

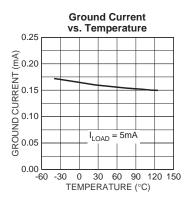


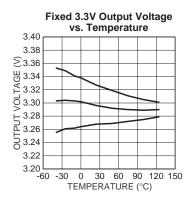
#### Schematic Diagram

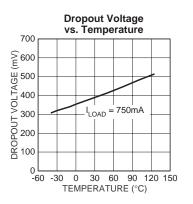
### **Typical Characteristics**

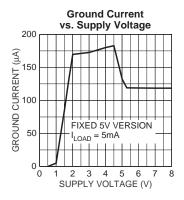


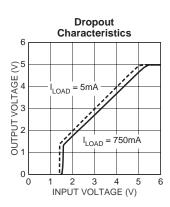


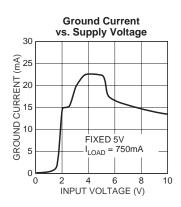








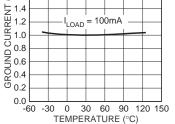




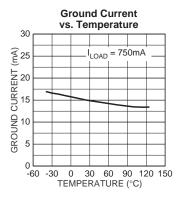
Ground Current vs. Temperature

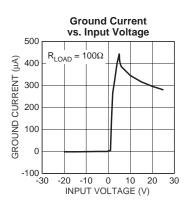
2.0

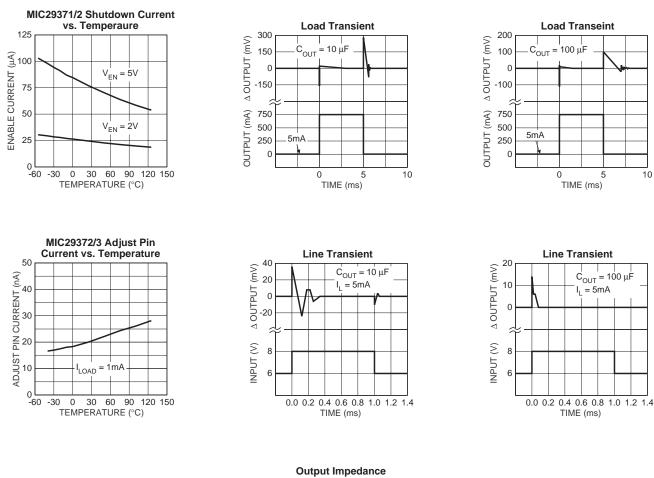
(1.8 E 1.6

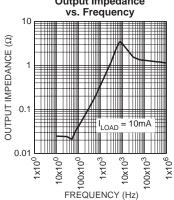


Short Circuit and Maximum Current vs. Temperature 1.4 = V<sub>NOMINAL</sub> - 0.5V OUT 1.2 0.1 8.0 CORRENT (A) 9.0 8.0 9.0 8.0  $V_{OUT} = 0V$ 0.4 FIXED 5V 0.2 VERSION 0.0 -60 -30 0 30 60 90 120 150 TEMPERATURE (°C)









### **Applications Information**

#### **External Capacitors**

A 10 $\mu$ F (or greater) capacitor is required between the MIC2937A output and ground to prevent oscillations due to instability. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about –30°C, so solid tantalums are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.5\mu$ F for current below 10mA or  $0.15\mu$ F for currents below 1 mA. Adjusting the MIC29372 to voltages below 5V runs the error amplifier at lower gains so that more output capacitance is needed. For the worst-case situation of a 750mA load at 1.23V output (Output shorted to Adjust) a 22 $\mu$ F (or greater) capacitor should be used.

The MIC2937A/29371 will remain in regulation with a minimum load of 5mA. When setting the output voltage of the MIC29372 version with external resistors, the current through these resistors may be included as a portion of the minimum load.

A  $0.1\mu$ F capacitor should be placed from the input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

#### Error Detection Comparator Output (MIC29371)

A logic low output will be produced by the comparator whenever the MIC29371 output falls out of regulation by more than approximately 5%. This figure is the comparator's built-in offset of about 75mV divided by the 1.235V reference voltage. (Refer to the block diagram on Page 1). This trip level remains "5% below normal" regardless of the programmed output voltage of the MIC29371. For example, the error flag trip level is typically 4.75V for a 5V output or 11.4V for a 12V output. The out of regulation condition may be due either to low input voltage, extremely high input voltage, current limiting, or thermal limiting.

Figure 1 is a timing diagram depicting the ERROR signal and the regulated output voltage as the MIC29371 input is ramped up and down. The ERROR signal becomes valid (low) at about 1.3V input. It goes high at about 5V input (the input voltage at which  $V_{OUT} = 4.75$ ). Since the MIC29371's dropout voltage is load-dependent (see curve in Typical Performance Characteristics), the input voltage trip point (about 5V) will vary with the load current. The output voltage trip point (approximately 4.75V) does not vary with load. The error comparator has an NPN open-collector output which requires an external pull-up resistor. Depending on system requirements, this resistor may be returned to the 5V output or some other supply voltage. In determining a value for this resistor, note that while the output is rated to sink  $250\mu$ A, this sink current adds to battery drain in a low battery condition. Suggested values range from 100k to  $1M\Omega$ . The resistor is not required if this output is unused.

#### Programming the Output Voltage (MIC29372)

The MIC29372 may programmed for any output voltage between its 1.235V reference and its 26V maximum rating. An external pair of resistors is required, as shown in Figure 3.

The complete equation for the output voltage is

$$V_{OUT} = V_{REF} x \{ 1 + R_1/R_2 \} - |I_{FB}| R_1$$

where V<sub>REF</sub> is the nominal 1.235 reference voltage and I<sub>FB</sub> is the Adjust pin bias current, nominally 20nA. The minimum recommended load current of 1µA forces an upper limit of 1.2MΩ on the value of R<sub>2</sub>, if the regulator must work with no load (a condition often found in CMOS in standby), I<sub>FB</sub> will produce a –2% typical error in V<sub>OUT</sub> which may be eliminated at room temperature by trimming R<sub>1</sub>. For better accuracy, choosing R<sub>2</sub>=100k reduces this error to 0.17% while increasing the resistor program current to 12µA. Since the MIC29372 typically draws 100µA at no load with SHUTDOWN opencircuited, this is a negligible addition.

#### **Reducing Output Noise**

In reference applications it may be advantageous to reduce the AC noise present at the output. One method is to reduce the regulator bandwidth by increasing the size of the output capacitor. This is relatively inefficient, as increasing the capacitor from 1µF to 220µF only decreases the noise from 430µV to 160µV<sub>RMS</sub> for a 100kHz bandwidth at 5V output. Noise can be reduced by a factor of four with the adjustable

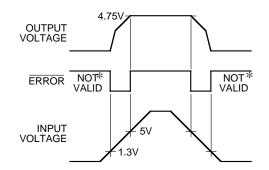




Figure 1. ERROR Output Timing

regulators with a bypass capacitor across  $R_1$ , since it reduces the high frequency gain from 4 to unity. Pick

$$C_{\text{BYPASS}} \cong \frac{1}{2\pi R_1 \cdot 200 \text{ Hz}}$$

or about  $0.01\mu$ F. When doing this, the output capacitor must be increased to  $10\mu$ F to maintain stability. These changes reduce the output noise from  $430\mu$ V to  $100\mu$ V<sub>RMS</sub> for a 100 kHz bandwidth at 5V output. With the bypass capacitor added, noise no longer scales with output voltage so that improvements are more dramatic at higher output voltages.

### **Typical Applications**

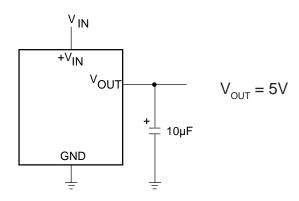


Figure 2. MIC2937A-5.0 Fixed +5V Regulator

VOUT

ADJUST

VOUT ≈ VIN

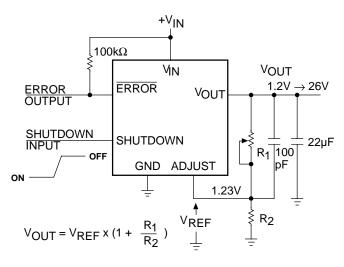
+VIN

VIN

GND

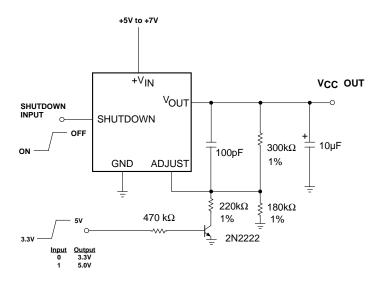
#### Automotive Applications

The MIC2937A is ideally suited for automotive applications for a variety of reasons. It will operate over a wide range of input voltages with very low dropout voltages (40mV at light loads), and very low quiescent currents (100 $\mu$ A typical). These features are necessary for use in battery powered systems, such as automobiles. It is a "bulletproof" device with the ability to survive both reverse battery (negative transients up to 20V below ground), and load dump (positive transients up to 60V) conditions. A wide operating temperature range with low temperature coefficients is yet another reason to use these versatile regulators in automotive designs.



ERROR OUTPUT ON MIC29373 ONLY SHUTDOWN INPUT ON MIC29372 ONLY

#### Figure 3. MIC29372 Adjustable Regulator



\*MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT.

Figure 4. MIC29372 Wide Input Voltage Range Current Limiter

SHUTDOWN PIN LOW= ENABLE OUTPUT. Q1 ON = 3.3V, Q1 OFF = 5.0V.

Figure 5. MIC29372 5.0V or 3.3V Selectable Regulator with Shutdown.



# MIC2940A/2941A

1.25A Low-Dropout Voltage Regulator

### **Preliminary Information**

### **General Description**

The MIC2940A and MIC2941A are "bulletproof" efficient voltage regulators with very low dropout voltage (typically 40mV at light loads and 350mV at 1A), and low quiescent current (240 $\mu$ A typical). The quiescent current of the MIC2940A increases only slightly in dropout, thus prolonging battery life. Key MIC2940A features include protection against reversed battery, fold-back current limiting, and automotive "load dump" protection (60V positive transient).

The MIC2940 is available in both fixed voltage (3.3V, 5V, and 12V) and adjustable voltage configurations. The MIC2940Axx devices are three pin fixed voltage regulators. A logiccompatible shutdown input is provided on the adjustable MIC2941A, which enables the regulator to be switched on and off.

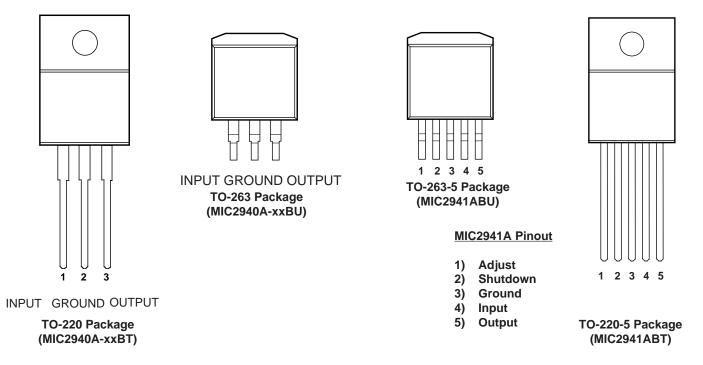
### Features

- High output voltage accuracy
- Guaranteed 1.25A output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Input can withstand –20V reverse battery and +60V positive transients
- Logic-controlled electronic shutdown
- Output programmable from 1.24V to 26V(MIC2941A)
- Available in TO-220, TO-263, TO-220-5, and TO-263-5 packages.

#### **Applications**

- Battery Powered Equipment
- Cellular Telephones
- Laptop, Notebook, and Palmtop Computers
- PCMCIA V<sub>cc</sub> and V<sub>PP</sub> Regulation/Switching
- Bar Code Scanners
- Automotive Electronics
- SMPS Post-Regulator/ DC to DC Modules
- Voltage Reference
- High Efficiency Linear Power Supplies

### **Pin Configuration**



#### The Tab is Ground on TO-220 and TO-263 packages

### Absolute Maximum Ratings

Ordering Information					
Part Number	Voltage	Temperature Range*	Package		
MIC2940A-3.3BT	3.3	–40°C to +125°C	TO-220		
MIC2940A-3.3BU	3.3	–40°C to +125°C	TO-263		
MIC2940A-5.0BT	5.0	–40°C to +125°C	TO-220		
MIC2940A-5.0BU	5.0	–40°C to +125°C	TO-263		
MIC2940A-12BT	12	–40°C to +125°C	TO-220		
MIC2940A-12BU	12	–40°C to +125°C	TO-263		
MIC2941ABT	Adj	–40°C to +125°C	TO-220-5		
MIC2941ABU	Adj	–40°C to +125°C	TO-263-5		

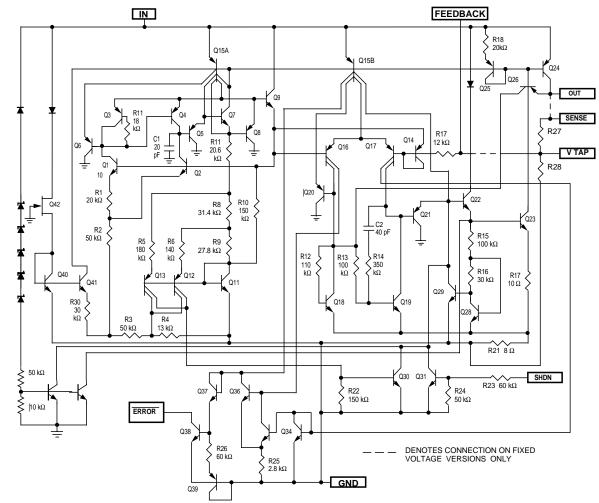
#### \* Junction temperatures

#### If Military/Aerospace specified devices are required, contact your local Micrel representative/distributor for availability and specifications.

Power Dissipation (Note 1) Internally Limited
Lead Temperature (Soldering, 5 seconds) 260°C Storage Temperature Range
–40°C to +125°C
TO-220 θ <sub>JC</sub>
TO-263 θ <sub>ic</sub>
Input Supply Voltage–20V to +60V
Operating Input Supply Voltage 2V <sup>+</sup> to 26V
Adjust Input Voltage (Notes 9 and 10)
-1.5V to +26V
Shutdown Input Voltage0.3V to +30V Error Comparator Output Voltage0.3V to +30V

<sup>†</sup> Across the full operating temperature, the minimum input voltage range for full output current is 4.3V to 26V. Output will remain in-regulation at lower output voltages and low current loads down to an input of 2V at 25°C.

### **Schematic Diagram**



### **Electrical Characteristics**

Limits in standard typeface are for  $T_J = 25^{\circ}C$  and limits in **boldface** apply over the full operating temperature range. Unless otherwise specified,  $V_{IN} = V_{OUT} + 1V$ ,  $I_L = 1000$ mA,  $C_L = 10\mu$ F. The MIC2941A is programmed to output 5V and has  $V_{SHUTDOWN} \le 0.6$ V.

Symbol	Parameter	Conditions	Min	Typical	Max	Units
Vo	Output Voltage		-1		1	%
	Accuracy		-2		2	
		$5 \text{ mA} \leq \text{I}_{\text{L}} \leq 1 \text{A}$	-2.5		2.5	
$\frac{\Delta V_o}{\Delta T}$	Output Voltage Temperature Coef.	(Note 2)		20	100	ppm/°C
$\frac{\Delta V_o}{V_o}$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 26V		0.03	0.10 <b>0.40</b>	%
$\frac{\Delta V_{o}}{V_{o}}$ $\frac{\Delta V_{o}}{V_{o}}$	Load Regulation	$I_{L} = 5mA$ to 1A		0.04	0.16 <b>0.20</b>	%
-		(Note 3)				
$V_{IN} - V_{O}$	Dropout Voltage (Note 4)	I <sub>L</sub> = 5mA		60	150 <b>180</b>	mV
		I <sub>L</sub> = 250mA		200	250 <b>320</b>	
		I <sub>L</sub> = 1000mA		350	450 <b>600</b>	
		I <sub>L</sub> = 1250mA		400	600	
I <sub>GND</sub>	Ground Pin Current (Note 5)	I <sub>L</sub> = 5mA		240	350 <b>500</b>	μΑ
		I <sub>L</sub> = 250mA		3	4.5 <b>6</b>	mA
		I <sub>L</sub> = 1000mA		22	35 <b>45</b>	
		I <sub>L</sub> = 1250mA		35	70	
I <sub>GNDDO</sub>	Ground Pin Current at Dropout (Note 5)	$V_{IN} = 0.5V$ less than designed $V_{OUT}$ ( $V_{OUT} \ge 3.3V$ ) $I_{L} = 5mA$		330	600	μΑ
ILIMIT	Current Limit	$V_{OUT} = 0V$ (Note 6)		1.6	2.4 <b>3</b>	A
$\frac{\Delta V_{o}}{\Delta P_{D}}$	Thermal Regulation	(Note 7)		0.05	0.2	%/W
en	Output Noise Voltage	$C_{L} = 10 \mu F$		400		μV RMS
	(10Hz to 100kHz) $I_{L} = 100mA$	$C_L = 33\mu F$		260		

### Electrical Characteristics (MIC2941A Only)

Parameter	Conditions	Min	Typical	Мах	Units
Reference Voltage		1.223 <b>1.210</b>	1.235	1.247 <b>1.260</b>	V V max
Reference Voltage	(Note 8)	1.204		1.266	V
Adjust Pin Bias Current			20	40 <b>60</b>	nA
Reference Voltage Temperature Coefficient			20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C

#### Shutdown Input

Input Logic Voltage	Low (ON) High (OFF)	2.0	1.3	0.7	V
Shutdown Pin Input Current	$V_{SHUTDOWN} = 2.4V$		30	50 <b>100</b>	μA
	V <sub>SHUTDOWN</sub> = 26V		450	600 <b>750</b>	μA
Regulator Output Current in Shutdown	(Note 10)		3	30 <b>60</b>	μA

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J_{(MAX)}}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_{A}$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{(MAX)} = (T_{J(MAX)} - T_{A}) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown.

Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

**Note 4:** Dropout Voltage is defined as the input to output differential at which the output voltage drops 100 mV below its nominal value measured at 1V differential. At low values of programmed output voltage, the minimum input supply voltage of 4.3V over temperature must be taken into account.

**Note 5:** Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus the ground pin current.

**Note 6:** The MIC2940A features fold-back current limiting. The short circuit ( $V_{OUT} = 0V$ ) current limit is less than the maximum current with normal output voltage.

**Note 7:** Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 200mA load pulse at  $V_{IN} = 20V$  (a 4W pulse) for T = 10ms.

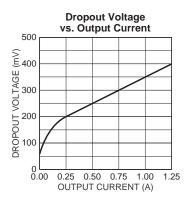
**Note 8:**  $V_{REF} \le V_{OUT} \le (V_{IN} - 1 V), 4.3V \le V_{IN} \le 26V, 5mA < I_{L} \le 1.25A, T_{J} \le T_{J MAX.}$ 

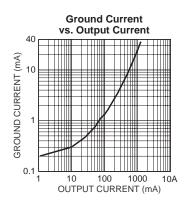
**Note 9:** Circuit of Figure 3 with  $R1 \ge 150k\Omega$ .  $V_{SHUTDOWN} \ge 2 V$  and  $V_{IN} \le 26 V, V_{OUT} = 0$ .

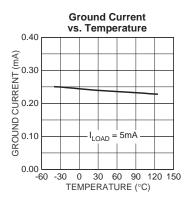
**Note 10:** When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

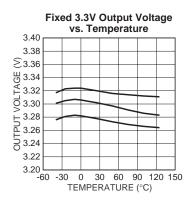
**Note 11:** Maximum positive supply voltage of 60 V must be of limited duration (< 100 ms) and duty cycle ( $\leq$  1%). The maximum continuous supply voltage is 26V.

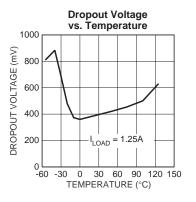
### **Typical Characteristics**

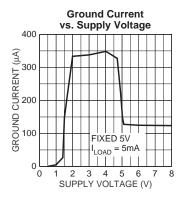












Ground Current

vs. Temperature

 $I_{LOAD} = 100 \text{mÅ}$ 

0.0 -30 0 30 60 90 120 150

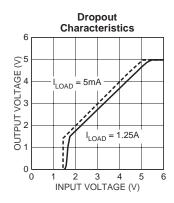
TEMPERATURE (°C)

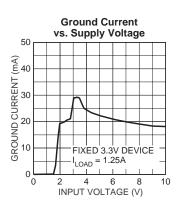
2.0

(¥ ₩ 1.6

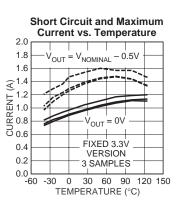
1.4 1.2 1.0 0.8 0.6 0.4 0.2

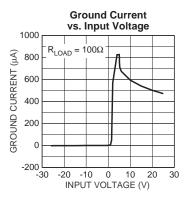
0.2





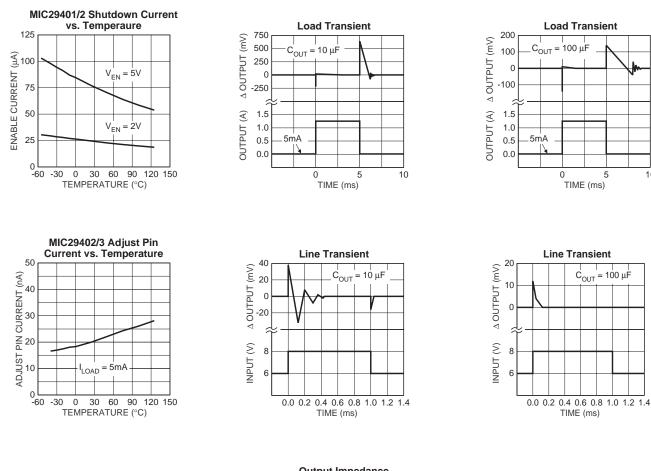
Ground Current vs. Temperature 50 € ₩40 = 1.25A LOAD **GROUND CURRENT** 30 20 10 TEMPERATURE (°C)

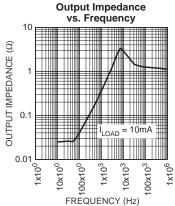




5

10





### **Applications Information**

#### **External Capacitors**

A 10 $\mu$ F (or greater) capacitor is required between the MIC2940A output and ground to prevent oscillations due to instability. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about –30°C, so solid tantalums are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $3.3\mu$ F for current below 100mA or  $2.2\mu$ F for currents below 10 mA. Adjusting the MIC2941A to voltages below 5V runs the error amplifier at lower gains so that more output capacitance is needed. For the worst-case situation of a 1.25A load at 1.23V output (Output shorted to Adjust) a 22 $\mu$ F (or greater) capacitor should be used.

The MIC2940A will remain stable and in regulation with load currents ranging from 5mA on up to the full 1.25A rating. The external resistors of the MIC2941A version may be scaled to draw this minimum load current.

A  $0.22\mu$ F capacitor should be placed from the MIC2940A input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

#### Programming the Output Voltage (MIC2941A)

The MIC2941A may be programmed for any output voltage between its 1.235V reference and its 26V maximum rating. An external pair of resistors is required, as shown in Figure 3.

The complete equation for the output voltage is

$$V_{OUT} = V_{REF} \times \{1 + R_1/R_2\} - |I_{FB}|R_1$$

where V<sub>REF</sub> is the nominal 1.235 reference voltage and I<sub>FB</sub> is the Adjust pin bias current, nominally 20nA. The minimum recommended load current of 1 µA forces an upper limit of 1.2MΩ on the value of R<sub>2</sub>, if the regulator must work with no load (a condition often found in CMOS in standby), I<sub>FB</sub> will produce a –2% typical error in V<sub>OUT</sub> which may be eliminated at room temperature by trimming R<sub>1</sub>. For better accuracy, choosing R<sub>2</sub> = 100kΩ reduces this error to 0.17% while increasing the resistor program current to 12 µA. Since the MIC2941A typically draws 100 µA at no load with SHUTDOWN open-circuited, this is a negligible addition.

#### **Reducing Output Noise**

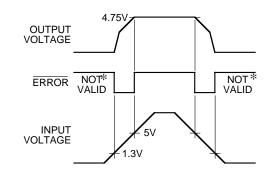
In reference applications it may be advantageous to reduce the AC noise present at the output. One method is to reduce the regulator bandwidth by increasing the size of the output capacitor. This is relatively inefficient, as increasing the capacitor from 1  $\mu$ F to 220  $\mu$ F only decreases the noise from 430 $\mu$ V to 160 $\mu$ V<sub>RMS</sub> for a 100kHz bandwidth at 5V output. Noise can be reduced by a factor of four with the MIC2941A by adding a bypass capacitor across R<sub>1</sub>, since it reduces the high frequency gain from 4 to unity. Pick

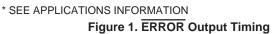
$$C_{\text{BYPASS}} \cong \frac{1}{2\pi R_1 \bullet 200 \text{ Hz}}$$

or about 0.01  $\mu$ F. When doing this, the output capacitor must be increased to 22  $\mu$ F to maintain stability. These changes reduce the output noise from 430  $\mu$ V to 100  $\mu$ V rms for a 100 kHz bandwidth at 5V output. With the bypass capacitor added, noise no longer scales with output voltage so that improvements are more dramatic at higher output voltages.

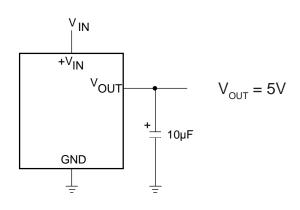
#### **Automotive Applications**

The MIC2940A is ideally suited for automotive applications for a variety of reasons. It will operate over a wide range of input voltages with very low dropout voltages (40mV at light loads), and very low quiescent currents (240µA typical). These features are necessary for use in battery powered systems, such as automobiles. It is a "bulletproof" device with the ability to survive both reverse battery (negative transients up to 20V below ground), and load dump (positive transients up to 60V) conditions. A wide operating temperature range with low temperature coefficients is yet another reason to use these versatile regulators in automotive designs.





## **Typical Applications**



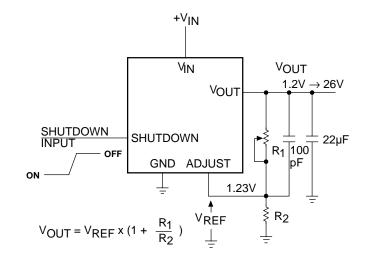
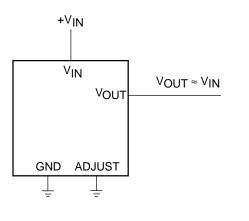


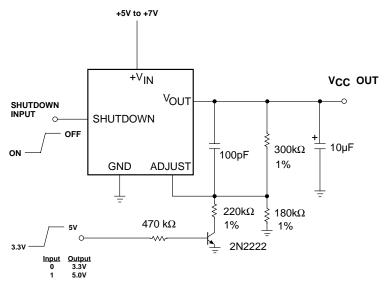
Figure 2. MIC2940A-5.0 Fixed +5V Regulator





\*MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT.

Figure 4. MIC2941A Wide Input Voltage Range Current Limiter



ADJUST PIN LOW= ENABLE OUTPUT. Q1 ON = 3.3V, Q1 OFF = 5.0V.

Figure 5. MIC2941A 5.0V or 3.3V Selectable Regulator with Shutdown.



# LP2950/2951

### 100mA Low-Dropout Voltage Regulator

### **General Description**

The LP2950 and LP2951 are micropower voltage regulators with very low dropout voltage (typically 40mV at light loads and 380mV at 100mA), and very low quiescent current (75 $\mu$ A typical). The quiescent current of the LP2950/LP2951 increases only slightly in dropout, thus prolonging battery life. This feature, among others, makes the LP2950 and LP2951 ideally suited for use in battery-powered systems.

Available in a 3-Pin TO-92 package, the LP2950 is pincompatible with the older 5V regulators. Additional system functions, such as programmable output voltage and logiccontrolled shutdown, are available in the 8-pin DIP and 8-pin SOIC versions of the LP2951.

### Applications

- Automotive Electronics
- Voltage Reference
- Avionics

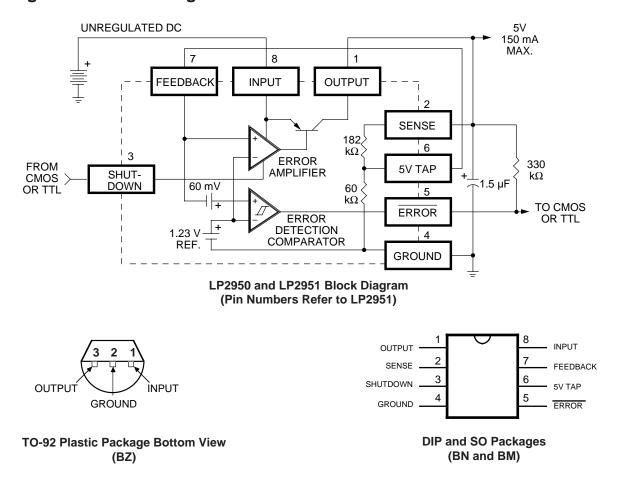
# Block Diagram and Pin Configurations

### **Features**

- High accuracy 5V, guaranteed 100 mA output
- Extremely low quiescent current
- Low-dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Use as regulator or reference
- Needs only 1µF for stability
- Current and thermal limiting

### LP2951 Versions Only

- Error flag warns of output dropout
- Logic-controlled electronic shutdown
- Output programmable from 1.24 to 29V



See MIC2950 for a part with 1) higher output (150 mA), 2) transient protection (60V), and 3) reverse input protection to -20V)

Additional features available with the LP2951 also include an error flag output that warns of a low output voltage, which is often due to failing batteries on the input. This may also be used as a power-on reset. A logic-compatible shutdown input is also available which enables the regulator to be switched on and off. This part may also be pin-strapped for a 5V output, or programmed from 1.24V to 29V with the use of two external resistors.

The LP2950 is available as either an -02 or -03 version. The -02 and -03 versions are guaranteed for junction temperatures from  $-40^{\circ}$ C to  $+125^{\circ}$ C; the -02 version has a tighter output and

reference voltage specification range over temperature. The LP2951 is available as an -01, -02, or -03 version. The -01 version is guaranteed for junction temperatures from  $-55^{\circ}$ C to +150°C, and has slightly different specifications limits over the full operating temperature range.

The LP2950 and LP2951 have a tight initial tolerance (0.5% typical), a very low output voltage temperature coefficient which allows use as a low-power voltage reference, and extremely good load and line regulation (0.05% typical). This greatly reduces the error in the overall circuit, and is the result of careful design techniques and process control.

			1	1
Part Number	Voltage	Temperature Range*	Package	Accuracy
LP2950-02BZ	5.0V	–40°C to +125°C	3-Pin TO-92 plastic	0.5%
LP2950-03BZ	5.0V	–40°C to +125°C	3-Pin TO-92 plastic	1.0%
LP2951-02BM	5.0V	–40°C to +125°C	8-Pin SOIC	0.5%
LP2951-03BM	5.0V	–40°C to +125°C	8-Pin SOIC	1.0%
LP2951-02BN	5.0V	–40°C to +125°C	8-Pin Plastic DIP	0.5%
LP2951-03BN	5.0V	–40°C to +125°C	8-Pin Plastic DIP	1.0%
LP2951-4.8BM	4.85V	–40°C to +125°C	8-Pin SOIC	1.0%

### **Ordering Information**

\* Junction temperatures

### **Absolute Maximum Ratings**

If Military/Aerospace specified devices are required, contact your local Micrel representative/distributor for availability and specifications.

Power dissipation	Internally Limited
Lead Temperature (Soldering, 5 seconds)	260°C
Storage Temperature Range	–65°C to +150°C
Operating Junction Temperature Range (Note 8) LP2951-01 LP2950-02/LP2950-03, LP2951-02/LP2951-03	–55°C to +150°C −40°C to +125°C
Input Supply Voltage	–0.3V to +30V
Feedback Input Voltage (Notes 9 and 10)	-1.5V to +30V
Shutdown Input Voltage (Note 9)	–0.3V to +30V
Error Comparator Output Voltage (Note 9)	–0.3V to +30V
ESD Rating is to be determined.	

Parameter	Condition	Min	Тур	Max	Units
Output Voltage	LP2951-01 (±0.5%)	4.975	5.000	5.025	V
$T_J = 25^{\circ}C$	LP295x-02 (±0.5%)	4.975	5.000	5.025	V
	LP295x-03 (±1%)	4.950	5.000	5.050	V
	LP2951-4.8 (±1%)	4.802	4.850	4.899	V
Output Voltage	LP295x-02 (±0.5%)	4.950		5.050	V
$-25^{\circ}C \le T_{J} \le +85^{\circ}C$	LP295x-03 (±1%)	4.925		5.075	V
	LP2951-4.8 (±1%)	4.777		4.872	V
Output Voltage	LP2951-01 (±0.5%), –55°C to +160°C	4.940		5.060	V
Over Full Temperature Range	LP295x-02 (±0.5%), -40°C to +125°C	4.940		5.060	V
	LP295x-03 (±1%), -40°C to +125°C	4.900		5.100	V
	LP2951-4.8 (±1%), -40°C to +125°C	4.753		4.947	V
Output Voltage	LP2951-01 (±0.5%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA, T <sub>J</sub> $\leq$ T <sub>J(max)</sub>	4.925		5.075	V
Over Load Variation	LP295x-02 (±0.5%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA, T <sub>J</sub> $\leq$ T <sub>J(max)</sub>	4.930		5.070	V
	LP295x-03 (±1%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA, T <sub>J</sub> $\leq$ T <sub>J(max)</sub>	4.880		5.120	V
	LP2951-4.8 (±1%), 100 $\mu$ A ≤ I <sub>L</sub> ≤ 100mA, T <sub>J</sub> ≤ T <sub>J(max)</sub>	4.733		4.967	V
Output Voltage	LP2951-01 (±0.5%), Note 12		20	120	ppm/°C
Temperature Coefficient	LP295x-02 (±0.5%), Note 12		20	100	ppm/°C
	LP295x-03 (±1%), Note 12		50	150	ppm/°C
	LP2951-4.8 (±1%), Note 12		50	150	ppm/°C
Line Regulation	LP2951-01 (±0.5%), Notes 14, 15		0.03	0.10 <b>0.50</b>	% %
	LP295x-02 (±0.5%), Notes 14, 15		0.03	0.10 <b>0.20</b>	% %
	LP295x-03 (±1%), Notes 14, 15		0.04	0.20 <b>0.40</b>	% %
	LP2951-4.8 (±1%), Notes 14, 15		0.04	0.20 <b>0.40</b>	% %
Load Regulation	LP2951-01 (±0.5%), Note 14, 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA		0.04	0.10 <b>0.30</b>	% %
	LP295x-02 (±0.5%), Note 14, 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA		0.04	0.10 <b>0.20</b>	% %
	LP295x-03 (±1%), Note 14, 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA		0.10	0.20 <b>0.30</b>	% %
	LP2951-4.8 (±1%), Note 14, 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 100mA		0.10	0.20 <b>0.30</b>	% %
Dropout Voltage	Note 5, I <sub>L</sub> = 100μA		50	80 <b>150</b>	mV mV
	Note 5, I <sub>L</sub> = 100mA		380	450 <b>600</b>	mV mV
Ground Current	I <sub>L</sub> = 100μA		100	150 <b>200</b>	μA μA
	I <sub>L</sub> = 100mA		8	12 <b>14</b>	mA mA
Dropout Current	$V_{IN} = 4.5V, I_{L} = 100\mu A$		180	250 <b>310</b>	μA μA

Parameter	Condition	Min	Тур	Max	Units
Current Limit	V <sub>OUT</sub> = 0V		160	200 <b>220</b>	mA mA
Thermal Regulation	Note 13		0.05	0.20	%/W
Output Noise	10Hz to 100kHz, $C_L = 1\mu F$		430		$\mu V_{RMS}$
	10Hz to 100kHz, $C_{L} = 200\mu F$		160		$\mu V_{RMS}$
	10Hz to 100kHz, $C_L = 3.3\mu F$ , 0.01 $\mu F$ bypass Feedback to Output		100		μV <sub>RMS</sub>
Reference Voltage	LP2951-01 (±0.5%)	1.220 <b>1.200</b>	1.235	1.250 <b>1.260</b>	V V
	LP295x-02 (±0.5%)	1.220 <b>1.200</b>	1.235	1.250 <b>1.260</b>	V V
	LP295x-03 (±1%)	1.210 <b>1.200</b>	1.235	1.260 <b>1.270</b>	V V
	LP2951-4.8 (±1%)	1.210 <b>1.200</b>	1.235	1.260 <b>1.270</b>	V V
Reference Voltage	LP2951-01 (±0.5%), Note 7	1.190		1.270	V
	LP295x-02 (±0.5%), Note 7	1.190		1.270	V
	LP295x-03 (±1%), Note 7	1.185		1.285	V
	LP2951-4.8 (±1%), Note 7	1.185		1.285	V
Feedback Bias Current			20	40 <b>60</b>	nA nA
Reference Voltage	LP2951-01 (±0.5%), Note 12		20		ppm/°C
	LP295x-02 (±0.5%), Note 12		20		ppm/°C
	LP295x-03 (±1%), Note 12		50		ppm/°C
	LP2951-4.8 (±1%), Note 12		50		ppm/°C
Feedback Bias Current Temperature Coefficient			0.1		nA/°C
Output Leakage Current	V <sub>OH</sub> = 30V		0.01	1.00 <b>2.00</b>	μΑ μΑ
Output Low Voltage (Flag)	$V_{IN} = 4.5V, I_{OL} = 200 \mu A$		150	250 <b>400</b>	mV mV
Upper Threshold Voltage	Note 6	40 <b>25</b>	60		mV mV
Lower Threshold Voltage	Note 6		75	95 <b>140</b>	mV mV
Hysteresis	Note 6		15		mV
Input Logic Voltage	LP2951-01 (±0.5%)		1.3		V
	Low High	2.0		0.6	V V
	LP295x-02 (±0.5%) Low		1.3	0.7	V V
	High	2.0		0.7	V
	LP295x-03 (±1%)		1.3		V
	Low			0.7	
	High	2.0	4.0		V
	LP2951-4.8 (±1%) Low High	2.0	1.3	0.7	V V V

Parameter	Condition	Min	Тур	Max	Units
Shutdown Input Current	V <sub>SHUTDOWN</sub> = 2.4V		30	50 <b>100</b>	μΑ μΑ
	V <sub>SHUTDOWN</sub> = 30V		450	600 <b>750</b>	μΑ μΑ
Regulator Output Current in Shutdown	Note 11		3	10 <b>20</b>	μΑ μΑ

Note 1: Boldface limits apply at temperature extremes.

Note 2: Unless otherwise specified all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V_{IN} = 6V$ ,  $I_L = 100\mu$ A and  $C_L = 1\mu$ F. Additional conditions for the 8-pin versions are Feedback tied to 5V Tap and Output tied to Output Sense ( $V_{OUT} = 5V$ ) and  $V_{SHUTDOWN} \le 0.8V$ .

Note 3: Guaranteed and 100% production tested.

Note 4: Guaranteed but not 100% production tested. These limits are not used to calculate outgoing AQL levels.

Note 5: Dropout voltage is defined as the input to output differential at which the output voltage drops 100mV below its nominal value measured at 1V differential. At very low values of programmed output voltage, the minimum input supply voltage of 2V (2.3V over temperature) must be taken into account.

**Note 6:** Comparator thresholds are expressed in terms of a voltage differential at the Feedback terminal below the nominal reference voltage measured at 6V input. To express these thresholds in terms of output voltage change, multiply by the error amplifier gain = V<sub>OUT</sub> /V<sub>REF</sub> = (R1 + R2)/R2. For example, at a programmed output voltage of 5V, the Error output is guaranteed to go low when the output drops by 95mV x 5V/1.235V = 384mV. Thresholds remain constant as a percent of V<sub>OUT</sub> as V<sub>OUT</sub> is varied, with the dropout warning occurring at typically 5% below nominal, 7.5% guaranteed.

 $\textbf{Note 7:} \quad V_{REF} \leq V_{OUT} \leq (V_{IN}-1~V), \ 2.3V \leq V_{IN} \leq 30V, \ 100\mu A < I_L \leq 100 mA, \ T_J \leq T_{JMAX}.$ 

**Note 8:** The junction-to-ambient thermal resistance of the TO-92 package is 180°C/W with 0.4" leads and 160°C/W with 0.25" leads to a PC board. The thermal resistance of the 8-pin DIP package is 105°C/W junction-to-ambient when soldered directly to a PC board. Junction-to-ambient thermal resistance for the SOIC (M) package is 160°C/W.

Note 9: May exceed input supply voltage.

Note 10: When used in dual-supply systems where the output terminal sees loads returned to a negative supply, the output voltage should be diodeclamped to ground.

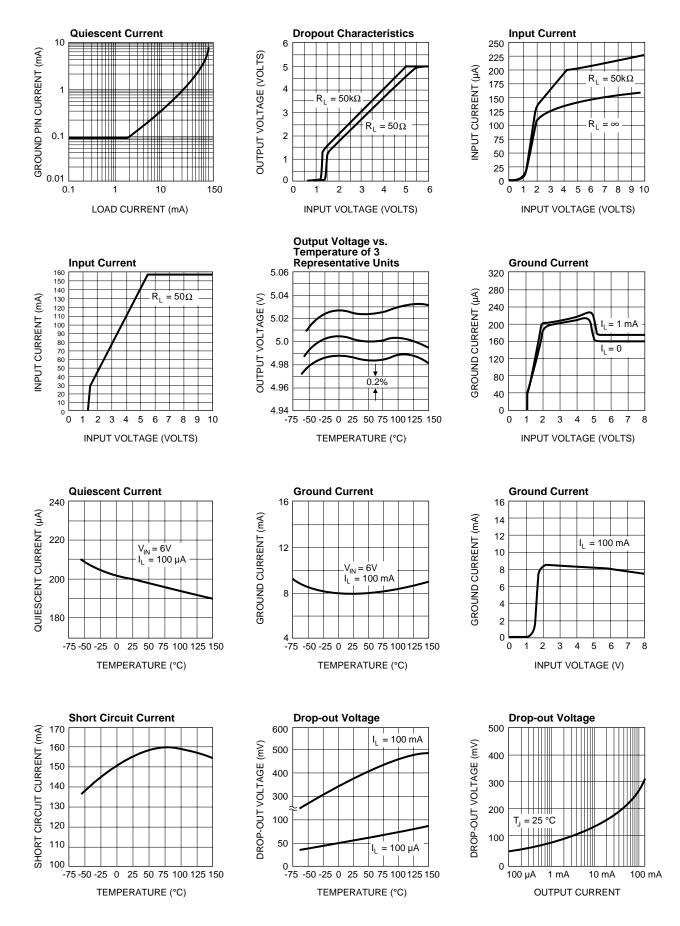
Note 11:  $V_{SHUTDOWN} \ge 2V$ ,  $V_{IN} \le 30$  V,  $V_{OUT} = 0$ , with Feedback pin tied to 5V Tap.

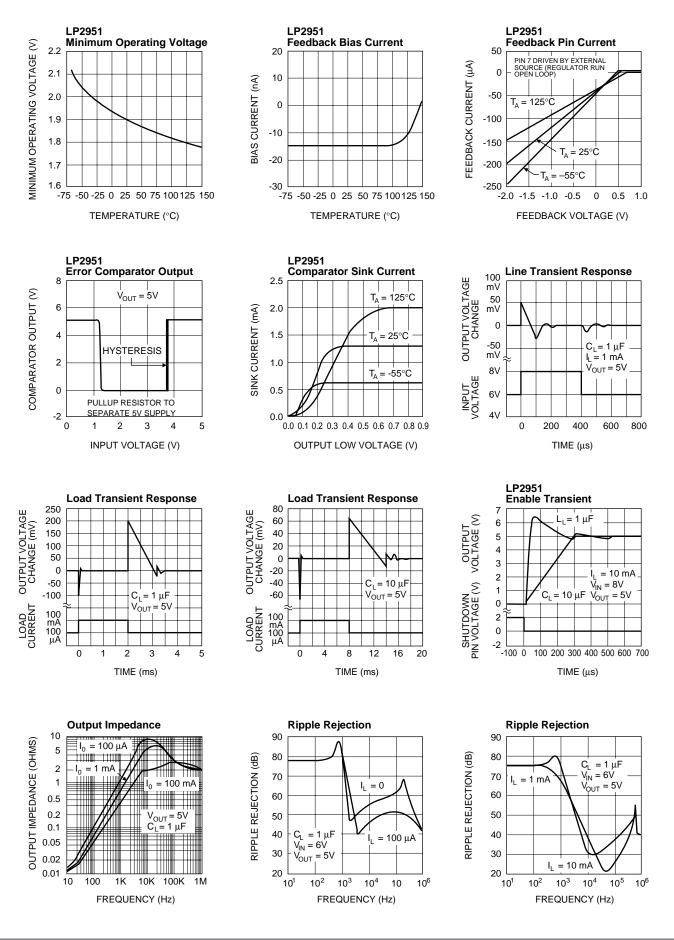
Note 12: Output or reference voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

Note 13: Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 50mA load pulse at  $V_{IN} = 30V$  (1.25W pulse) for t = 10ms.

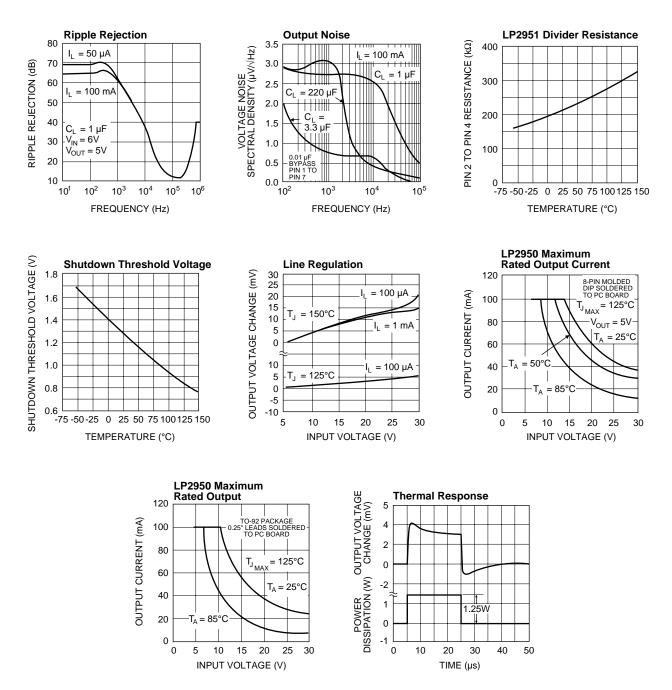
Note 14: Regulation is measured at constant junction temperature, using pulse testing with a low duty cycle. Changes in output voltage due to heating effects are covered in the specification for thermal regulation.

Note 15: Line regulation for the LP2951 is tested at 150°C for  $I_L = 1$ mA. For  $I_L = 100\mu$ A and  $T_J = 125$ °C, line regulation is guaranteed by design to 0.2%. See Typical Performance Characteristics for line regulation versus temperature and load current.





# Typical Performance Characteristics (Continued)



# **Applications Information**

## **External Capacitors**

A 1.0 $\mu$ F (or greater) capacitor is required between the LP2950/ LP2951 output and ground to prevent oscillations due to instability. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about –30°C, so solid tantalum capacitors are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.33\mu$ F for current below 10mA or  $0.1\mu$ F for currents below 1mA. Using the 8-Pin versions at voltages below 5V runs the error amplifier at lower gains so that more output capacitance is needed. For the worst-case situation of a 100mA load at 1.23V output (Output shorted to Feedback) a  $3.3\mu$ F (or greater) capacitor should be used.

The LP2950 will remain stable and in regulation with no load in addition to the internal voltage divider, unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications. When setting the output voltage of the LP2951 version with external resistors, a minimum load of  $1\mu$ A is recommended.

A  $0.1\mu$ F capacitor should be placed from the LP2950/LP2951 input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

Stray capacitance to the LP2951 Feedback terminal (pin 7) can cause instability. This may especially be a problem when using high value external resistors to set the output voltage. Adding a 100pF capacitor between Output and Feedback and increasing the output capacitor to at least  $3.3\mu$ F will remedy this.

## **Error Detection Comparator Output**

A logic low output will be produced by the comparator whenever the LP2951 output falls out of regulation by more than approximately 5%. This figure is the comparator's built-in offset of about 60mV divided by the 1.235V reference voltage. (Refer to the block diagram on Page 1). This trip level remains "5% below normal" regardless of the programmed output voltage of the LP2951. For example, the error flag trip level is typically 4.75V for a 5V output or 11.4V for a 12V output. The out of regulation condition may be due either to low input voltage, current limiting, or thermal limiting.

Figure 1 is a timing diagram depicting the ERROR signal and the regulated output voltage as the LP2951 input is ramped up and down. The ERROR signal becomes valid (low) at about 1.3V input. It goes high at about 5V input (the input voltage at which  $V_{OUT} = 4.75V$ ). Since the LP2951's dropout voltage is load-dependent (see curve in Typical Performance Characteristics), the input voltage trip point (about 5V) will vary with the load current. The output voltage trip point (approximately 4.75V) does not vary with load.

The error comparator has an open-collector output which requires an external pull-up resistor. Depending on system requirements, this resistor may be returned to the 5V output or some other supply voltage. In determining a value for this resistor, note that while the output is rated to sink 400 $\mu$ A, this sink current adds to battery drain in a low battery condition. Suggested values range from 100k to 1M $\Omega$ . The resistor is not required if this output is unused.

#### Programming the Output Voltage (LP2951)

The LP2951 may be pin-strapped for 5V using its internal voltage divider by tying Pin 1 (output) to Pin 2 (SENSE) and Pin 7 (FEEDBACK) to Pin 6 (5V TAP). Alternatively, it may be programmed for any output voltage between its 1.235V reference and its 30V maximum rating. An external pair of resistors is required, as shown in Figure 2.

The complete equation for the output voltage is

$$V_{OUT} = V_{REF} x \{ 1 + R_1/R_2 \} + I_{FB} R_2$$

where V<sub>REF</sub> is the nominal 1.235 reference voltage and I<sub>FB</sub> is the feedback pin bias current, nominally 20 nA. The minimum recommended load current of 1 µA forces an upper limit of 1.2 MΩ on the value of R<sub>2</sub>, if the regulator must work with no load (a condition often found in CMOS in standby), I<sub>FB</sub> will produce a 2% typical error in V<sub>OUT</sub> which may be eliminated at room temperature by trimming R<sub>1</sub>. For better accuracy, choosing R<sub>2</sub> = 100kΩ reduces this error to 0.17% while increasing the resistor program current to 12µA. Since the LP2951 typically draws 60 µA at no load with Pin 2 open-circuited, this is a small price to pay.

#### **Reducing Output Noise**

In reference applications it may be advantageous to reduce the AC noise present at the output. One method is to reduce the regulator bandwidth by increasing the size of the output capacitor. This is the only method by which noise can be reduced on the 3 lead LP2950 and is relatively inefficient, as increasing the capacitor from 1 $\mu$ F to 220 $\mu$ F only decreases the noise from 430 $\mu$ V to 160 $\mu$ V rms for a 100kHz bandwidth at 5V output.

Noise can be reduced fourfold by a bypass capacitor across  $R_1$ , since it reduces the high frequency gain from 4 to unity. Pick

$$C_{BYPASS} \cong \frac{1}{2\pi R_1 \cdot 200 \text{ Hz}}$$

or about 0.01  $\mu$ F. When doing this, the output capacitor must be increased to 3.3  $\mu$ F to maintain stability. These changes reduce the output noise from 430 $\mu$ V to 100 $\mu$ V rms for a 100kHz bandwidth at 5V output. With the bypass capacitor added, noise no longer scales with output voltage so that improvements are more dramatic at higher output voltages. Figure 1. ERROR Output Timing

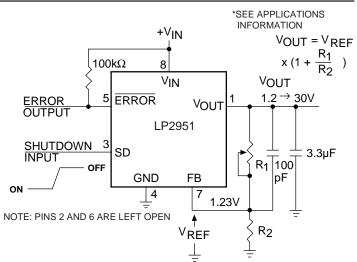
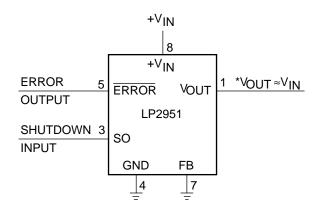


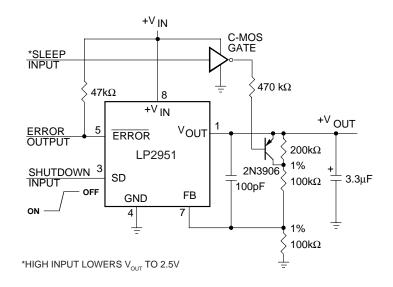
Figure 2. Adjustable Regulator

# **Typical Applications**

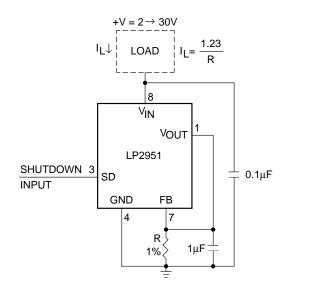


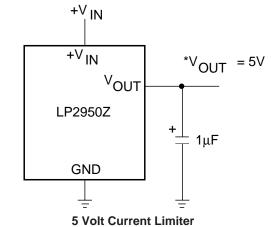
\*MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT. CURRENT LIMIT IS TYPICALLY 160mA.

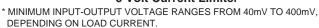
#### Wide Input Voltage Range Current Limiter



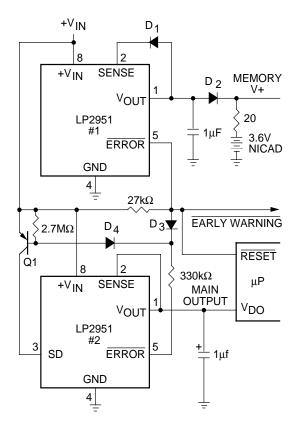
#### 5 V Regulator with 2.5 V Sleep Function







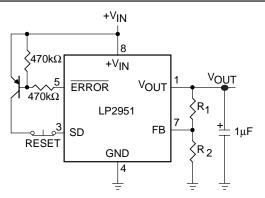




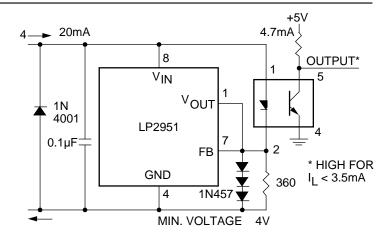
#### **Regulator with Early Warning and Auxiliary Output**

- EARLY WARNING FLAG ON LOW INPUT VOLTAGE
- MAIN OUTPUT LATCHES OFF AT LOWER INPUT VOLTAGES
- BATTERY BACKUP ON AUXILIARY OUTPUT

OPERATION: REG. #1'S  $V_{\text{OUT}}$  IS PROGRAMMED ONE DIODE DROP ABOVE 5 V. ITS ERROR FLAG BECOMES ACTIVE WHEN  $V_{\text{IN}} \leq 5.7$  V. WHEN  $V_{\text{IN}}$  DROPS BELOW 5.3 V, THE ERROR FLAG OF REG. #2 BECOMES ACTIVE AND VIA Q1 LATCHES THE MAIN OUTPUT OFF. WHEN  $V_{\text{IN}}$  AGAIN EXCEEDS 5.7 V REG. #1 IS BACK IN REGULATION AND THE EARLY WARNING SIGNAL RISES, UNLATCHING REG. #2 VIA D3.

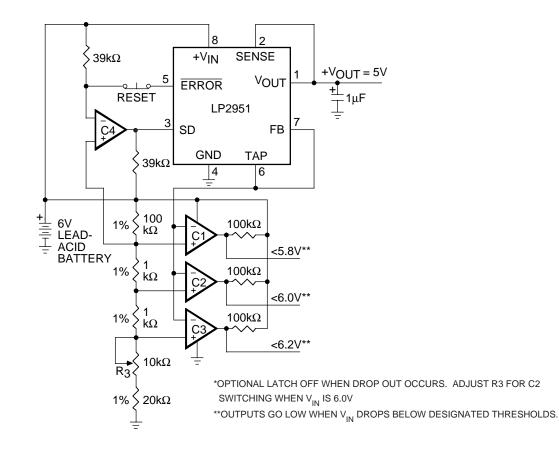


Latch Off When Error Flag Occurs

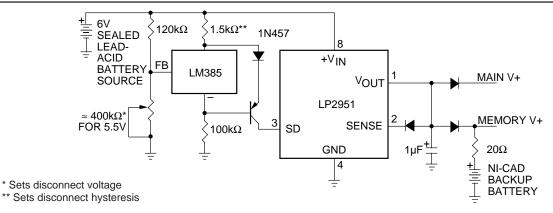


Micrel

Open Circuit Detector for 4mA to 20mA Current Loop

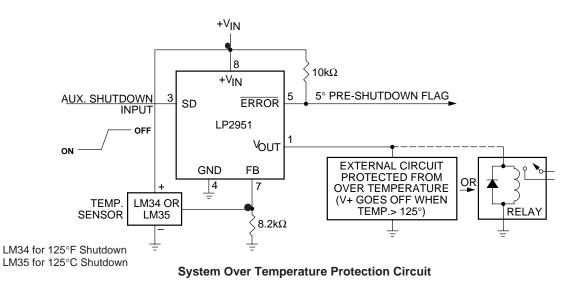




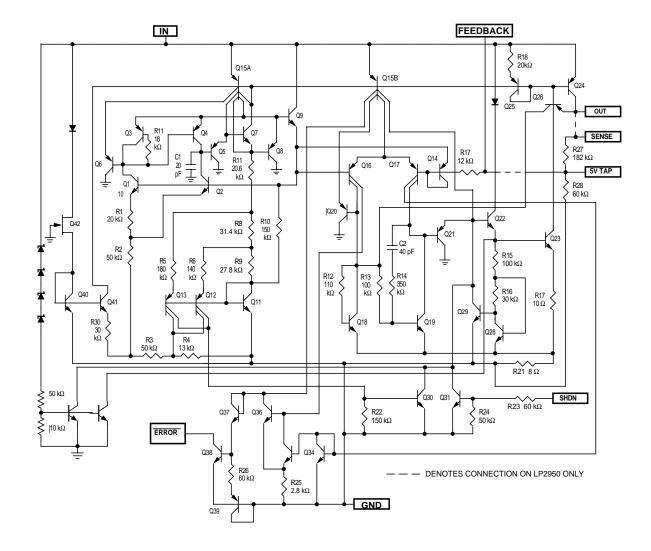


Low Battery Disconnect

For values shown, Regulator shuts down when  $V_{IN}$  < 5.5 V and turns on again at 6.0 V. Current drain in disconnected mode is 150 $\mu$ A.



Section 5: Data Sheets





# MIC2950/2951

#### 150mA Low-Dropout Voltage Regulator

## **General Description**

The MIC2950 and MIC2951 are "bulletproof" micropower voltage regulators with very low dropout voltage (typically 40mV at light loads and 250mV at 100mA), and very low quiescent current. Like their predecessors, the LP2950 and LP2951, the quiescent current of the MIC2950/MIC2951 increases only slightly in dropout, thus prolonging battery life. The MIC2950/MIC2951 are pin for pin compatible with the LP2950/LP2951, but offer lower dropout, lower quiescent current, reverse battery, and automotive load dump protection.

The key additional features and protection offered include higher output current (150mA), positive transient protection for up to 60V (load dump), and the ability to survive an unregulated input voltage transient of -20V below ground (reverse battery).

The plastic DIP and SOIC versions offer additional system functions such as programmable output voltage and logic controlled shutdown. The 3-pin TO-92 MIC2950 is pin-compatible with the older 5V regulators.

These system functions also include an error flag output that warns of a low output voltage, which is often due to failing batteries on the input. This may also be used as a power-on reset. A logic-compatible shutdown input is also available which enables the regulator to be switched on and off. This part may also be pin-strapped for a 5 V output, or programmed from 1.24 V to 29 V with the use of two external resistors.

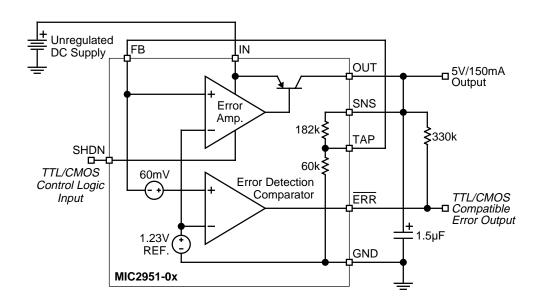
#### **Features**

- High accuracy 3.3, 4.85, or 5V, guaranteed 150mA output
- Extremely low quiescent current
- Low-dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Use as regulator or reference
- Needs only 1.5µF for stability
- Current and thermal limiting
- Unregulated DC input can withstand –20V reverse battery and +60V positive transients
- Error flag warns of output dropout (MIC2951)
- Logic-controlled electronic shutdown (MIC2951)
- Output programmable from 1.24V to 29V (MIC2951)

#### Applications

- Automotive Electronics
- Battery Powered Equipment
- Cellular Telephones
- SMPS Post-Regulator
- Voltage Reference
- Avionics
- High Efficiency Linear Power Supplies

## **Block Diagram**



#### MIC2950/2951

The MIC2950 is available as either an -05 or -06 version. The -05 and -06 versions are guaranteed for junction temperatures from  $-40^{\circ}$ C to  $+125^{\circ}$ C; the -05 version has a tighter output and reference voltage specification range over temperature. The MIC2951 is available as an -01, -02, or -03 version. The -01 version is guaranteed for junction temperatures from  $-55^{\circ}$ C to  $+150^{\circ}$ C, and has slightly different specifications limits over the full operating temperature range.

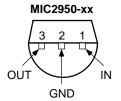
The MIC2950 and MIC2951 have a tight initial tolerance (0.5% typical), a very low output voltage temperature coefficient which allows use as a low-power voltage reference, and extremely good load and line regulation (0.04% typical). This greatly reduces the error in the overall circuit, and is the result of careful design techniques and process control.

# **Ordering Information**

Part Number	Voltage	Accuracy	Temperature Range*	Package
MIC2950-05BZ	5.0V	0.5%	–40°C to +125°C	TO-92
MIC2950-06BZ	5.0V	1.0%	–40°C to +125°C	TO-92
MIC2951-02BM	5.0V	0.5%	–40°C to +125°C	8-pin SOIC
MIC2951-03BM	5.0V	1.0%	–40°C to +125°C	8-pin SOIC
MIC2951-02BN	5.0V	0.5%	–40°C to +125°C	8-pin plastic DIP
MIC2951-03BN	5.0V	1.0%	–40°C to +125°C	8-pin plastic DIP
MIC2951-03BMM	5.0V	1.0%	–40°C to +125°C	8-lead MM8™
MIC2951-3.3BM	3.3V	1.0%	–40°C to +125°C	8-pin SOIC
MIC2951-4.8BM	4.85V	1.0%	–40°C to +125°C	8-pin SOIC

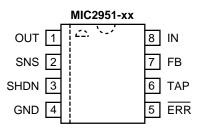
\* junction temperature

## **Pin Configuration**



TO-92 (Z) (Bottom View)

## **Pin Description**



#### DIP (N), SOIC (M), MM8™ (MM) (Top View)

Pin # MIC2950	Pin # MIC2951	Pin Name	Pin Function
3	1	OUT	Regulated Output
	2	SNS	Sense (Input): Output-voltage sensing end of internal voltage divider for fixed 5V operation. Not used in adjustable configuration.
	3	SHDN	Shutdown/Enable (Input): TTL compatible input. High = shutdown, low or open = enable.
2	4	GND	Ground
	5	ERR	Error Flag (Output): Active low, open-collector output (low = error, floating = normal).
	6	TAP	3.3V/4.85/5V Tap: Output of internal voltage divider when the regulator is configured for fixed operation. Not used in adjustable configuration.
	7	FB	Feedback (Input): 1.235V feedback from internal voltage divider's TAP (for fixed operation) or external resistor network (adjustable configuration).
1	8	IN	Unregulated Supply Input
Section 5	: Data Sheet	ts	117 Designing With LDO Regulators

# **Absolute Maximum Ratings**

Input Suppy Voltage (V <sub>IN</sub> ) <b>Note 2</b> –20V to +60V
Feedback Input Voltage (V <sub>FB</sub> ) Note 3, 41.5V to +26V
Shutdown Input Voltage (V <sub>SHDN</sub> ) Note 3 –0.3V to +30V
Power Dissipation ( $P_D$ ) <b>Note 1</b> Internally Limited
Storage Temperature –65°C to + 150°C
Lead Temperature (soldering, 5 sec.) 260°C

# **Operating Ratings**

Input Supply Voltage (VIN) +2.0V to +	-30V
Junction Temperature (T <sub>J</sub> ) No	ote 1
MIC2951-0155°C to +15	50°C
MIC2950-05/MIC2950-0640°C to +12	25°C
MIC2951-02/MIC2950-0340°C to +12	25°C

# **Electrical Characteristics** Note 5, 6 $T_A = 25^{\circ}C$ except as noted.

Parameter	Condition	Min	Тур	Max	Units
Output Voltage	MIC2951-01 (±0.5%)	4.975	5.000	5.025	V
T <sub>J</sub> = 25°C	MIC295x-02/-05 (±0.5%)	4.975	5.000	5.025	V
	MIC295x-03/-06 (±1%)	4.950	5.000	5.050	V
	MIC2951-3.3 (±1%)	3.267	3.300	3.333	V
	MIC2951-4.8 (±1%)	4.802	4.850	4.899	V
Output Voltage	MIC295x-02/-05 (±0.5%)	4.950		5.050	V
$-25^{\circ}\text{C} \le \text{T}_{\text{J}} \le +85^{\circ}\text{C}$	MIC295x-03/-06 (±1%)	4.925		5.075	V
	MIC2951-3.3 (±1%)	3.251		3.350	V
	MIC2951-4.8 (±1%)	4.777		4.872	V
Output Voltage	MIC2951-01 (±0.5%), -55°C to +160°C	4.940		5.060	V
Over Full Temperature Range	MIC295x-02/-05 (±0.5%), -40°C to +125°C	4.940		5.060	V
	MIC295x-03/-06 (±1%), -40°C to +125°C	4.900		5.100	V
	MIC2951-3.3 (±1%), -40°C to +125°C	3.234		3.366	V
	MIC2951-4.8 (±1%), -40°C to +125°C	4.753		4.947	V
Output Voltage	MIC2951-01 (±0.5%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 150mA, T <sub>J</sub> $\leq$ T <sub>J(max)</sub>	4.925		5.075	V
Over Load Variation	MIC295x-02/-05 (±0.5%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 150mA, T <sub>J</sub> $\leq$ T <sub>J(max)</sub>	4.930		5.070	V
	MIC295x-03/-06 (±1%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 150mA, T <sub>J</sub> $\leq$ T <sub>J(max)</sub>	4.880		5.120	V
	MIC2951-3.3 (±1%), $100\mu A \le I_L \le 150 mA$ , $T_J \le T_{J(max)}$	3.221		3.379	V
	MIC2951-4.8 (±1%), $100\mu A \le I_L \le 150 mA$ , $T_J \le T_{J(max)}$	4.733		4.967	V
Output Voltage	MIC2951-01 (±0.5%), Note 7		20	120	ppm/°C
Temperature Coefficient	MIC295x-02/-05 (±0.5%), Note 7		20	100	ppm/°C
	MIC295x-03/-06 (±1%), Note 7		50	150	ppm/°C
	MIC2951-3.3 (±1%), Note 7		50	150	ppm/°C
	MIC2951-4.8 (±1%), Note 7		50	150	ppm/°C
Line Regulation	MIC2951-01 (±0.5%), Note 8, 9		0.03	0.10 <b>0.50</b>	% %
	MIC295x-02/-05 (±0.5%), Note 8, 9		0.03	0.10 <b>0.20</b>	% %
	MIC295x-03/-06 (±1%), Note 8, 9		0.04	0.20 <b>0.40</b>	% %
	MIC2951-3.3 (±1%), Note 8, 9		0.04	0.20 <b>0.40</b>	% %
	MIC2951-4.8 (±1%), Note 8, 9		0.04	0.20 <b>0.40</b>	% %

Parameter	Condition	Min	Тур	Max	Units
Load Regulation	MIC2951-01 (±0.5%), 100 $\mu$ A ≤ I <sub>L</sub> ≤ 150mA, Note 8		0.04	0.10 <b>0.30</b>	% %
	MIC295x-02/-05 (±0.5%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 150mA, Note 8		0.04	0.10 <b>0.20</b>	% %
	MIC295x-03/-06 (±1%), 100 $\mu$ A $\leq$ I <sub>L</sub> $\leq$ 150mA, Note 8		0.10	0.20 <b>0.30</b>	% %
	MIC2951-3.3 (±1%), $100\mu A \le I_L \le 150mA$ , Note 8		0.10	0.20 <b>0.30</b>	% %
	MIC2951-4.8 (±1%), 100 $\mu$ A ≤ I <sub>L</sub> ≤ 150mA, Note 8		0.10	0.20 <b>0.30</b>	% %
Dropout Voltage	MIC295x-01/-02/-03/-05/-06, I <sub>L</sub> = 100µA, Note 10		40	80 <b>140</b>	mV mV
	MIC295x-01/-02/-03/-05/-06, I <sub>1</sub> = 100mA, Note 10		250	300	mV
	MIC295x-01/-02/-03/-05/-06, I <sub>L</sub> = 150mA, Note 10		300	450 <b>600</b>	mV mV
	MIC2951-3.3 (±1%), I <sub>L</sub> = 100μA, Note 10		40	80 <b>150</b>	mV mV
	MIC2951-3.3 (±1%), I <sub>L</sub> = 100mA, Note 10		250	350	mV
	MIC2951-3.3 (±1%), I <sub>L</sub> = 150mA, Note 10		320	450 <b>600</b>	mV mV
	MIC2951-4.8 (±1%), I <sub>L</sub> = 100µA, Note 10		40	80 <b>140</b>	mV mV
	MIC2951-4.8 (±1%), I <sub>L</sub> = 100mA, Note 10		250	300	mV
	MIC2951-4.8 (±1%), I <sub>L</sub> = 150mA, Note 10		300	450 <b>600</b>	mV mV
Ground Current	MIC295x-01/-02/-03/-05/-06, I <sub>L</sub> = 100µA		120	180 <b>300</b>	μA μA
	MIC295x-01/-02/-03/-05/-06, I <sub>L</sub> = 100mA		1.7	2.5 <b>3.5</b>	mA mA
	MIC295x-01/-02/-03/-05/-06, I <sub>L</sub> = 150mA		4	6 <b>8</b>	mA mA
	MIC2951-3.3 (±1%), I <sub>L</sub> = 100μA		100	180 <b>300</b>	μΑ μΑ
	MIC2951-3.3 (±1%), I <sub>L</sub> = 100mA		1.7	2.5	mA
	MIC2951-3.3 (±1%), I <sub>L</sub> = 150mA		4	6 <b>10</b>	mA mA
	MIC2951-4.8 (±1%), I <sub>L</sub> = 100μA		120	180 <b>300</b>	μΑ μΑ
	MIC2951-4.8 (±1%), I <sub>L</sub> = 100mA		1.7	2.5 <b>3.5</b>	mA mA
	MIC2951-4.8 (±1%), I <sub>L</sub> = 150mA		4	6 <b>8</b>	mA mA
Dropout Ground Current	MIC2951-01 (±0.5%), V <sub>IN</sub> = 4.5V, I <sub>L</sub> = 100μA		280	400	μA μA
	MIC295x-02/-03/-05/-06 (±0.5%), V <sub>IN</sub> = 4.5V, I <sub>L</sub> = 100μA		280	350 <b>400</b>	μΑ μΑ
	MIC2951-3.3 (±1%), V <sub>IN</sub> = 3.0V, I <sub>L</sub> = 100μA		150	350 <b>400</b>	μΑ μΑ
	MIC2951-4.8 (±1%), V <sub>IN</sub> = 4.3V, I <sub>L</sub> = 100μA		280	350 <b>400</b>	μΑ μΑ

MIC2950/2951

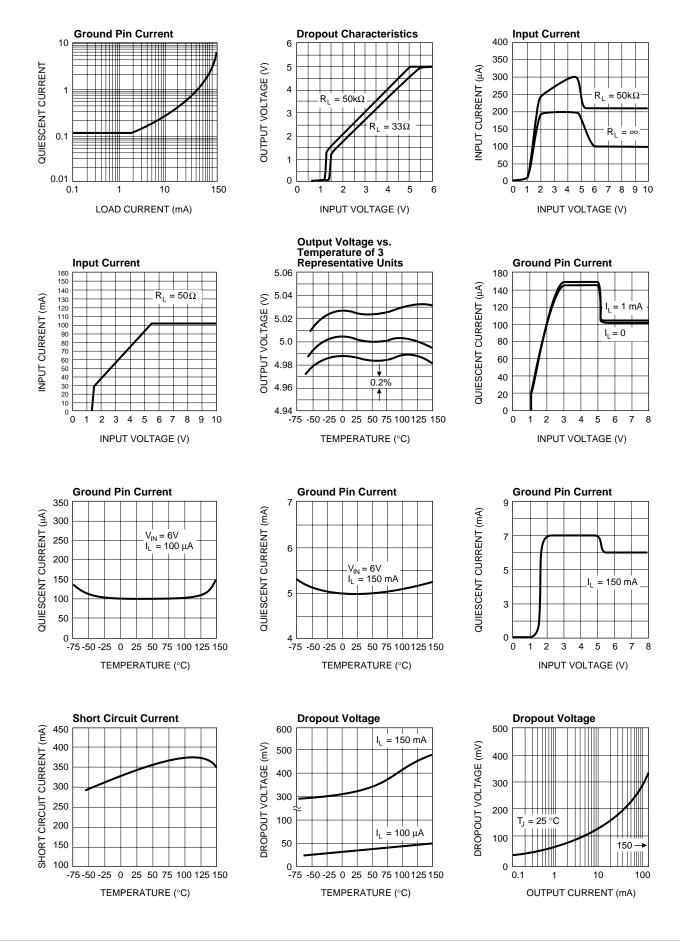
Parameter	Condition	Min	Тур	Max	Units
Current Limit	$V_{OUT} = 0V$		300	400 <b>450</b>	mA mA
Thermal Regulation	Note 11		0.05	0.20	%/W
Output Noise	10Hz to 100kHz, $C_{L} = 1.5 \mu F$		430		μV <sub>RMS</sub>
	10Hz to 100kHz, $C_{L} = 200\mu F$		160		μV <sub>RMS</sub>
	10Hz to 100kHz, C <sub>L</sub> = 3.3μF, 0.01μF bypass Feedback to Output		100		μV <sub>RMS</sub>
Reference Voltage	MIC2951-01 (±0.5%)	1.220 <b>1.200</b>	1.235	1.250 <b>1.260</b>	V V
	MIC295x-02/-05 (±0.5%)	1.220 <b>1.200</b>	1.235	1.250 <b>1.260</b>	V V
	MIC295x-03/-06 (±1%)	1.210 <b>1.200</b>	1.235	1.260 <b>1.270</b>	V V
	MIC2951-3.3 (±1%)	1.210 <b>1.200</b>	1.235	1.260 <b>1.270</b>	V V
	MIC2951-4.8 (±1%)	1.210 <b>1.200</b>	1.235	1.260 <b>1.270</b>	V V
Reference Voltage	MIC2951-01 (±0.5%), Note 12	1.190		1.270	V
	MIC295x-02/-05 (±0.5%), Note 12	1.190		1.270	V
	MIC295x-03/-06 (±1%), Note 12	1.185		1.285	V
	MIC2951-3.3 (±1%), Note 12	1.185		1.285	V
	MIC2951-4.8 (±1%), Note 12	1.185		1.285	V
Feedback Bias Current			20	40 <b>60</b>	nA nA
Reference Voltage	MIC2951-01 (±0.5%), Note 7		20		ppm/°C
Temperature Coefficient	MIC295x-02/-05 (±0.5%), Note 7		20		ppm/°C
	MIC295x-03/-06 (±1%), Note 7		50		ppm/°C
	MIC2951-3.3 (±1%), Note 7		50		ppm/°C
	MIC2951-4.8 (±1%), Note 7		50		ppm/°C
Feedback Bias Current Temperature Coefficient			0.1		nA/°C
Error Comparator (Flag) Output Leakage Current	V <sub>OH</sub> = 30V		0.01	1.00 <b>2.00</b>	μΑ μΑ
Error Comparator (Flag) Output Low Voltage	V <sub>IN</sub> = 4.5V, I <sub>OL</sub> = 200μA		150	250 <b>400</b>	mV mV
Error Comparator Upper Threshold Voltage	Note 13	40 <b>25</b>	60		mV mV
Error Comparator Lower Threshold Voltage	Note 13		75	95 <b>140</b>	mV mV
Error Comparator Hysteresis	Note 13		15		mV

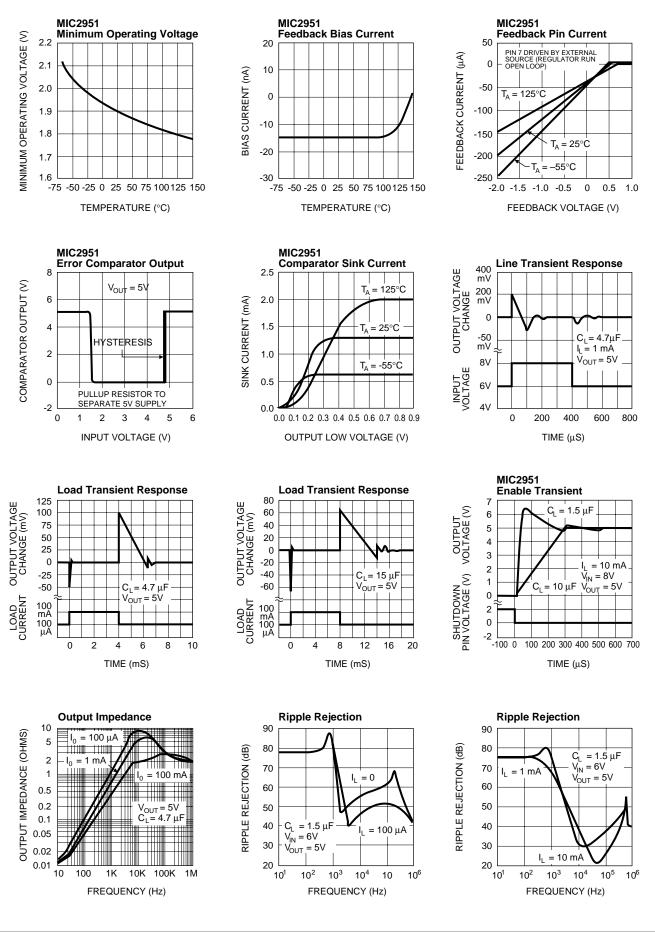
Parameter	Condition	Min	Тур	Max	Units
Shutdown Input Logic Voltage	MIC2951-01 (±0.5%) Low High	2.0	1.3	0.6	V V V
	MIC295x-02/-05 (±0.5%) Low High	2.0	1.3	0.7	V V V
	MIC295x-03/-06 (±1%) Low High	2.0	1.3	0.7	V V V
	MIC2951-3.3 (±1%) Low High	2.0	1.3	0.7	V V V
	MIC2951-4.8 (±1%) Low High	2.0	1.3	0.7	V V V
Shutdown Input Current	V <sub>SHUTDOWN</sub> = 2.4V		30	50 <b>100</b>	μΑ μΑ
	V <sub>SHUTDOWN</sub> = 30V		450	600 <b>750</b>	μΑ μΑ
Regulator Output Current in Shutdown	Note 4		3	10 <b>20</b>	μΑ μΑ

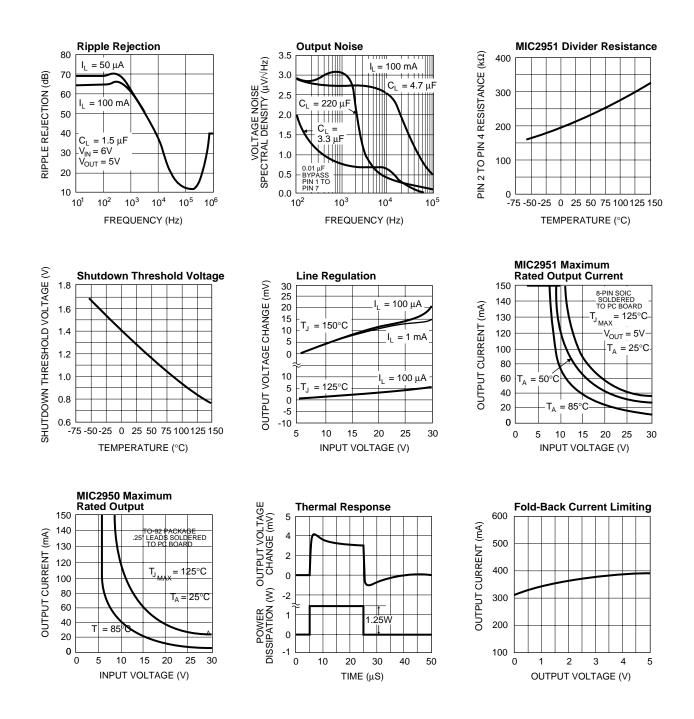
General Note: Devices are ESD protected; however, handling precautions are recommended.

- Note 1: The junction-to-ambient thermal resistance of the TO-92 package is 180°C/W with 0.4" leads and 160°C/W with 0.25" leads to a PC board. The thermal resistance of the 8-pin DIP package is 105°C/W junction-to-ambient when soldered directly to a PC board. Junction-to-ambient thermal resistance for the SOIC (M) package is 160°C/W. Junction-to-ambient thermal resistance for the SOIC (M) package is 160°C/W.
- Note 2: The maximum positive supply voltage of 60V must be of limited duration (≤100ms) and duty cycle (≤1%). The maximum continuous supply voltage is 30V.
- Note 3: When used in dual-supply systems where the output terminal sees loads returned to a negative supply, the output voltage should be diodeclamped to ground.
- Note 4:  $V_{SHUTDOWN} \ge 2V$ ,  $V_{IN} \le 30$  V,  $V_{OUT} = 0$ , with Feedback pin tied to 5V Tap.
- **Note 5:** Boldface limits apply at temperature extremes.
- Note 6: Unless otherwise specified all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V_{IN} = 6V$ ,  $I_L = 100\mu$ A and  $C_L = 1\mu$ F. Additional conditions for the 8-pin versions are Feedback tied to 5V Tap and Output tied to Output Sense ( $V_{OUT} = 5V$ ) and  $V_{SHUTDOWN} \le 0.8V$ .
- Note 7: Output or reference voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.
- Note 8: Regulation is measured at constant junction temperature, using pulse testing with a low duty cycle. Changes in output voltage due to heating effects are covered in the specification for thermal regulation.
- **Note 9:** Line regulation for the MIC2951 is tested at 150°C for  $I_L = 1mA$ . For  $I_L = 100\mu A$  and  $T_J = 125°C$ , line regulation is guaranteed by design to 0.2%. See Typical Performance Characteristics for line regulation versus temperature and load current.
- Note 10: Dropout voltage is defined as the input to output differential at which the output voltage drops 100mV below its nominal value measured at 1V differential. At very low values of programmed output voltage, the minimum input supply voltage of 2V (2.3V over temperature) must be taken into account.
- Note 11: Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 50mA load pulse at V<sub>IN</sub> = 30V (1.25W pulse) for t = 10ms.
- **Note 12:**  $V_{REF} \le V_{OUT} \le (V_{IN} 1 V), 2.3V \le V_{IN} \le 30V, 100\mu A < I_{L} \le 150m A, T_{J} \le T_{JMAX}.$
- Note 13: Comparator thresholds are expressed in terms of a voltage differential at the Feedback terminal below the nominal reference voltage measured at 6V input. To express these thresholds in terms of output voltage change, multiply by the error amplifier gain = V<sub>OUT</sub> /V<sub>REF</sub> = (R1 + R2)/R2. For example, at a programmed output voltage of 5V, the Error output is guaranteed to go low when the output drops by 95mV x 5V/1.235V = 384mV. Thresholds remain constant as a percent of V<sub>OUT</sub> as V<sub>OUT</sub> is varied, with the dropout warning occurring at typically 5% below nominal, 7.5% guaranteed.

# **Typical Characteristics**







# **Applications Information**

#### **Automotive Applications**

The MIC2950/2951 are ideally suited for automotive applications for a variety of reasons. They will operate over a wide range of input voltages, have very low dropout voltages (40mV at light loads), and very low quiescent currents. These features are necessary for use in battery powered systems, such as automobiles. They are also "bulletproof" devices; with the ability to survive both reverse battery (negative transients up to 20V below ground), and load dump (positive transients up to 60V) conditions. A wide operating temperature range with low temperature coefficients is yet another reason to use these versatile regulators in automotive designs.

#### **External Capacitors**

A 1.5  $\mu$ F (or greater) capacitor is required between the MIC2950/MIC2951 output and ground to prevent oscillations due to instability. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, so solid tantalums are recommended for operation below  $-25^{\circ}$ C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.5\mu$ F for current below 10mA or  $0.15\mu$ F for currents below 1 mA. Using the 8-pin versions at voltages below 5V runs the error amplifier at lower gains so that more output capacitance is needed. For the worst-case situation of a 150mA load at 1.23V output (Output shorted to Feedback) a 5 $\mu$ F (or greater) capacitor should be used.

The MIC2950 will remain stable and in regulation with no load in addition to the internal voltage divider, unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications. When setting the output voltage of the MIC2951 version with external resistors, a minimum load of  $1\mu$ A is recommended.

A  $0.1\mu$ F capacitor should be placed from the MIC2950/ MIC2951 input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

Stray capacitance to the MIC2951 Feedback terminal (pin 7) can cause instability. This may especially be a problem when using high value external resistors to set the output voltage. Adding a 100pF capacitor between Output and Feedback and increasing the output capacitor to at least  $3.3\mu$ F will remedy this.

#### **Error Detection Comparator Output**

A logic low output will be produced by the comparator whenever the MIC2951 output falls out of regulation by more than approximately 5%. This figure is the comparator's built-in offset of about 60mV divided by the 1.235V reference voltage. (Refer to the block diagram on Page 1). This trip level remains "5% below normal" regardless of the programmed output voltage of the MIC2951. For example, the error flag trip level is typically 4.75V for a 5V output or 11.4V for a 12V output. The out of regulation condition may be due either to low input voltage, current limiting, thermal limiting, or overvoltage on input (over  $\cong$  40V).

Figure 1 is a timing diagram depicting the ERROR signal and the regulated output voltage as the MIC2951 input is ramped up and down. The ERROR signal becomes valid (low) at about 1.3V input. It goes high at about 5V input (the input voltage at which  $V_{OUT} = 4.75$ —for 5.0V applications). Since the MIC2951's dropout voltage is load-dependent (see curve in Typical Performance Characteristics), the input voltage trip point (about 5V) will vary with the load current. The output voltage trip point does not vary with load.

The error comparator has an open-collector output which requires an external pull-up resistor. Depending on system requirements, this resistor may be returned to the output or some other supply voltage. In determining a value for this resistor, note that while the output is rated to sink  $200\mu$ A, this sink current adds to battery drain in a low battery condition. Suggested values range from 100k to  $1M\Omega$ . The resistor is not required if this output is unused.

#### Programming the Output Voltage (MIC2951)

The MIC2951 may be pin-strapped for 5V (or 3.3V or 4.85V) using its internal voltage divider by tying Pin 1 (output) to Pin 2 (sense) and Pin 7 (feedback) to Pin 6 (5V Tap). Alternatively, it may be programmed for any output voltage between its 1.235V reference and its 30V maximum rating. An external pair of resistors is required, as shown in Figure 2.

The complete equation for the output voltage is

$$V_{OUT} = V_{REF} \times \{ 1 + R_1/R_2 \} + I_{FB} R_1$$

where V<sub>REF</sub> is the nominal 1.235 reference voltage and I<sub>FB</sub> is the feedback pin bias current, nominally–20nA. The minimum recommended load current of 1 µA forces an upper limit of 1.2MΩ on the value of R<sub>2</sub>, if the regulator must work with no load (a condition often found in CMOS in standby), I<sub>FB</sub> will produce a 2% typical error in V<sub>OUT</sub> which may be eliminated at room temperature by trimming R<sub>1</sub>. For better accuracy, choosing R<sub>2</sub> = 100k reduces this error to 0.17% while increasing the resistor program current to 12 µA.

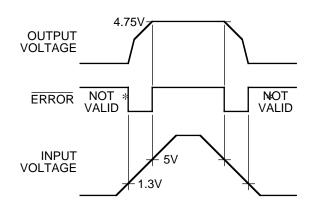
#### **Reducing Output Noise**

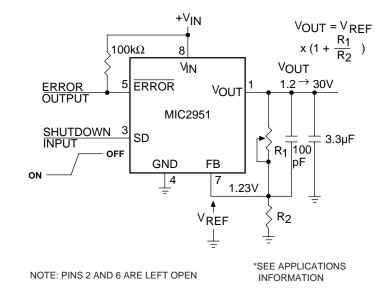
In some applications it may be advantageous to reduce the AC noise present at the output. One method is to reduce the regulator bandwidth by increasing the size of the output capacitor. This is the only method by which noise can be reduced on the 3 lead MIC2950 and is relatively inefficient, as increasing the capacitor from 1µF to 220µF only decreases the noise from 430µV to 160µV rms for a 100kHz bandwidth at 5V output.

Noise can be reduced fourfold by a bypass capacitor across  $R_1$ , since it reduces the high frequency gain from 4 to unity. Pick:

$$C_{\text{BYPASS}} \cong \frac{1}{2\pi R_1 \bullet 200 \text{ Hz}}$$

or about 0.01  $\mu F.$  When doing this, the output capacitor must be increased to 3.3  $\mu F$  to maintain stability. These changes reduce the output noise from 430  $\mu V$  to 100  $\mu V$  rms for a 100 kHz bandwidth at 5V output. With the bypass capacitor added, noise no longer scales with output voltage so that improvements are more dramatic at higher output voltages.



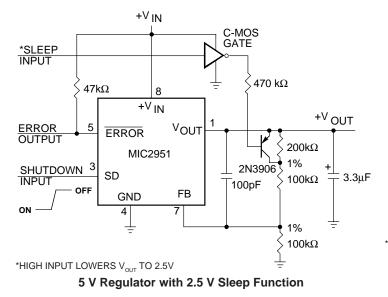


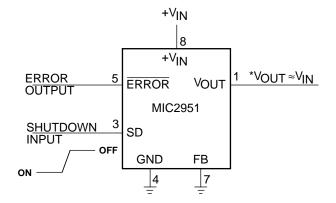
\* SEE APPLICATIONS INFORMATION



Figure 2. Adjustable Regulator

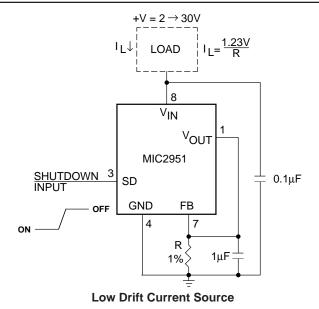
## **Typical Applications**

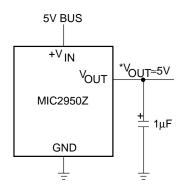




\*MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT.

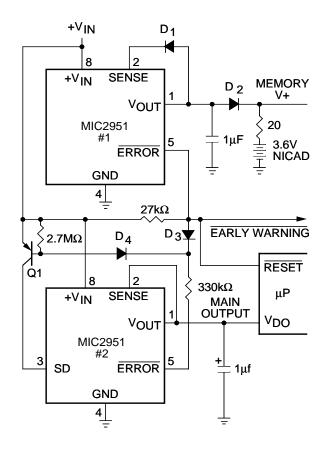
Wide Input Voltage Range Current Limiter





#### **5 Volt Current Limiter**

\* MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT.



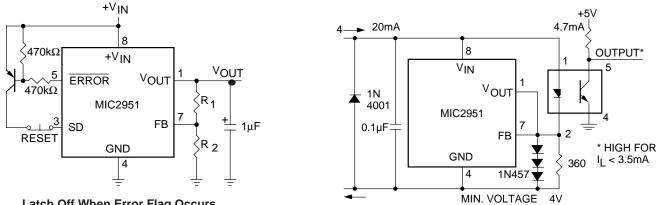
#### **Regulator with Early Warning and Auxiliary Output**

• EARLY WARNING FLAG ON LOW INPUT VOLTAGE

- MAIN OUTPUT LATCHES OFF AT LOWER INPUT VOLTAGES
- BATTERY BACKUP ON AUXILIARY OUTPUT

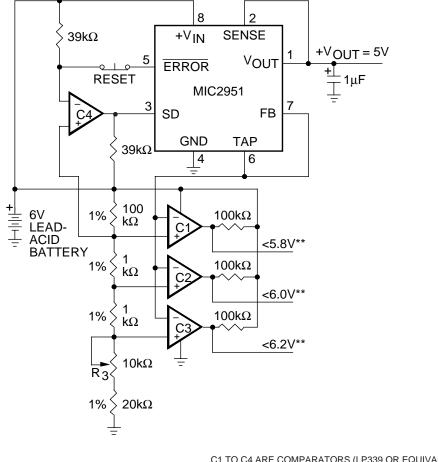
OPERATION: REG. #1'S V<sub>OUT</sub> IS PROGRAMMED ONE DIODE DROP ABOVE 5 V. ITS ERROR FLAG BECOMES ACTIVE WHEN V<sub>IN</sub>  $\leq$  5.7 V. WHEN V<sub>IN</sub> DROPS BELOW 5.3 V, THE ERROR FLAG OF REG. #2 BECOMES ACTIVE AND VIA Q1 LATCHES THE MAIN OUTPUT OFF. WHEN V<sub>IN</sub> AGAIN EXCEEDS 5.7 V REG. #1 IS BACK IN REGULATION AND THE EARLY WARNING SIGNAL RISES, UNLATCHING REG. #2 VIA D3.

Micrel



Latch Off When Error Flag Occurs

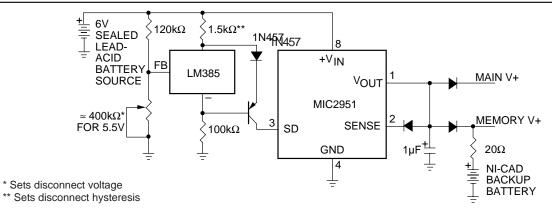
Open Circuit Detector for 4mA to 20mA Current Loop



C1 TO C4 ARE COMPARATORS (LP339 OR EQUIVALENT) \*OPTIONAL LATCH OFF WHEN DROP OUT OCCURS. ADJUST R3 FOR C2 SWITCHING WHEN V<sub>IN</sub> IS 6.0V

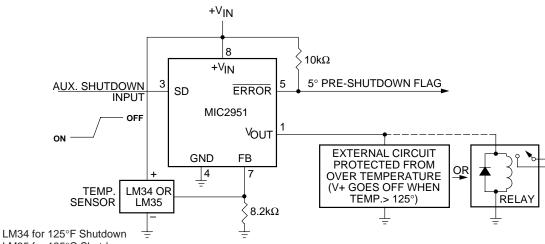
\*\*OUTPUTS GO LOW WHEN  ${\rm V}_{\rm IN}$  DROPS BELOW DESIGNATED THRESHOLDS.

#### **Regulator with State-of-Charge Indicator**





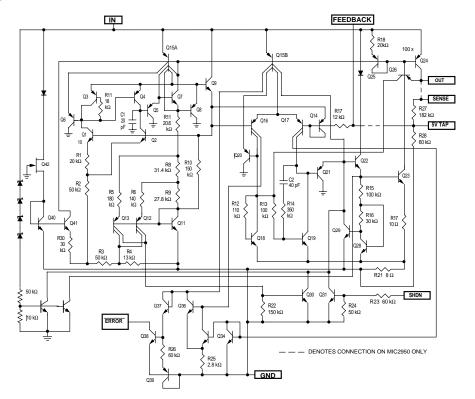
For values shown, Regulator shuts down when  $V_{IN}$  < 5.5 V and turns on again at 6.0 V. Current drain in disconnected mode is 150µA.



LM35 for 125°C Shutdown

System Over-Temperature Protection Circuit

## **Schematic Diagram**





# **MIC2954**

## 250mA Low-Dropout Voltage Regulator

## **General Description**

The MIC2954 is a "bulletproof" efficient voltage regulator with very low dropout voltage (typically 40mV at light loads and 375mV at 250mA), and low quiescent current (120 $\mu$ A typical). The quiescent current of the MIC2954 increases only slightly in dropout, thus prolonging battery life. Key MIC2954 features include protection against reversed battery, fold-back current limiting, and automotive load dump protection (60V positive transient).

The MIC2954-07/08BM is an adjustable version that includes an error flag output that warns of a low output voltage, which is often due to failing batteries on the input. This may also be used as a power-on reset. A logic-compatible shutdown input is provided which enables the regulator to be switched on and off. This part may be pin-strapped for 5V output, or programmed from 1.24 V to 29 V with the use of two external resistors.

The MIC2954 is available in two voltage tolerances,  $\pm 0.5\%$  maximum and  $\pm 1\%$  maximum. Both are guaranteed for junction temperatures from  $-40^{\circ}$ C to  $+125^{\circ}$ C.

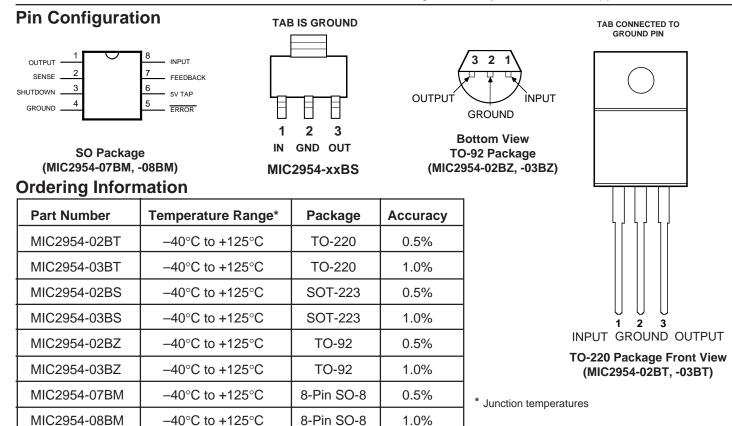
The MIC2954 has a very low output voltage temperature coefficient and extremely good load and line regulation (0.04% typical).

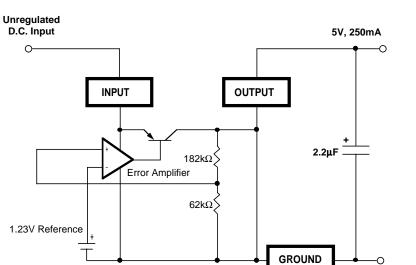
#### **Features**

- High accuracy 5V, guaranteed 250mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Input can withstand –20V reverse battery and +60V positive transients
- Error flag warns of output dropout
- Logic-controlled electronic shutdown
- Output programmable from 1.24V to 29V (MIC2954-07/08BM)
- Available in TO-220, TO-92, and Surface Mount SOT-223 and SO-8 packages.

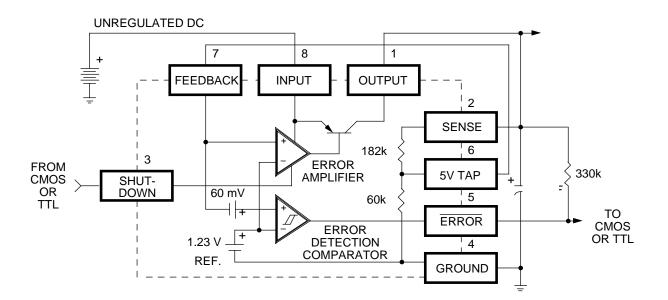
#### Applications

- Battery Powered Equipment
- Cellular Telephones
- Laptop, Notebook, and Palmtop Computers
- PCMCIA V<sub>cc</sub> and V<sub>PP</sub> Regulation/Switching
- Bar Code Scanners
- Automotive Electronics
- SMPS Post-Regulator/ DC to DC Modules
- Voltage Reference
- High Efficiency Linear Power Supplies





## MIC2954-07BM & 2954-08BM Block Diagram



## **Absolute Maximum Ratings**

If Military/Aerospace specified devices are required, contact your local Micrel representative/distributor for availability and specifications.

Power Dissipation (Note 1)	Internally Limited	Input Supply Voltage	-20V to +60V
Lead Temperature (Soldering, 5 seconds)	260°C	Feedback Input Voltage (Notes 10 and 11)	-1.5V to +26V
Storage Temperature Range	−65°C to +150°C	Shutdown Input Voltage	-0.3V to +30V
Operating Junction Temperature Range	−40°C to +125°C	Error Comparator Output Voltage	-0.3V to +30V

## **Electrical Characteristics**

Limits in standard typeface are for  $T_J = 25^{\circ}C$  and limits in **boldface** apply over the full operating temperature range. Unless otherwise specified,  $V_{IN} = 6V$ ,  $I_L = 1mA$ ,  $C_L = 2.2\mu$ F. The MIC2954-07BM,-08BM Feedback pin is tied to the 5V Tap and Output is tied to Output Sense ( $V_{OUT} = 5V$ ) and  $V_{SHUTDOWN} \le 0.6V$ .

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					MIC2954	-02/-07	MIC2954	4-03/-08	
$ \begin{array}{ c c c c c c } \hline \begin{tabular}{ c c c c c } \hline \begin{tabular}{ c c c c c c c } \hline \begin{tabular}{ c c c c c c c } \hline \begin{tabular}{ c c c c c c c } \hline \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Symbol	Parameter	Conditions	Typical	Min	Max	Min	Max	Units
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Vo	Output Voltage		5.0	4.975	5.025	4.950	5.050	V
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					4.940	5.060	4.900	5.100	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			$1mA \le I_{L} \le 250mA$	5.0	4.930	5.070	4.880	5.120	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$\Delta V_{o}$	Output Voltage	(Note 2)	20		100		150	ppm/°C
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\Delta T$	Temperature Coef.							
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\Delta V_o$	Line Regulation	$V_{IN} = 6V \text{ to } 26V$	0.03		0.10		0.20	%
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Vo			(Note 3)				0.40	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\Delta V_o$	Load Regulation	$I_{L} = 1$ to 250mA	0.04		0.16		0.20	%
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Vo					0.20		0.30	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			(Note 4)						
$ \begin{array}{ c c c c c c c } &  l_{L} = 50\text{mA} & 220 & 250 & 250 & 420 & 420 & 420 & 420 & 420 & 420 & 420 & 420 & 420 & 420 & 450 & 450 & 450 & 450 & 450 & 450 & 450 & 450 & 450 & 450 & 600 &$	$V_{IN} - V_{O}$	Dropout Voltage	$I_L = 1mA$	60		100		100	mV
$ \begin{array}{ c c c c c c c } & & & & & & & & & & & & & & & & & & &$		(Note 5)				150		150	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			I <sub>L</sub> = 50mA	220		250		250	
$ \begin{array}{ c c c c c c c } & & & & & & & & & & & & & & & & & & &$						420		420	
$ \begin{array}{ c c c c c c c } & I_{L} = 250 \text{ MA} & 375 & 450 & 450 & 600$			I <sub>L</sub> = 100mA	250		300		300	
$ \begin{array}{ c c c c c c } \hline I_{GND} & Ground Pin Current (Note 6) & I_{L} = 1mA & 140 & 200 & 200 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 300 & 10 & 1$						450		450	
$\begin{split} & I_{\text{GND}} & \begin{array}{c} \text{Ground Pin Current} \\ (\text{Note 6}) & I_{L} = 1\text{mA} \\ I_{L} = 5\text{omA} \\ I_{L} = 5\text{omA} \\ I_{L} = 5\text{omA} \\ I_{L} = 100\text{mA} \\ I_{L} = 100\text{mA} \\ I_{L} = 100\text{mA} \\ I_{L} = 25\text{omA} \\ I_{L} = 100\text{omA} \\ I$			I <sub>L</sub> = 250mA	375		450		450	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $						600		600	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	I <sub>GND</sub>	Ground Pin Current	I <sub>L</sub> = 1mA	140		200		200	μA
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		(Note 6)				300		300	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			I <sub>L</sub> = 50mA	0.5		1		1	mA
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $						2		2	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			I <sub>L</sub> = 100mA	1.7		2.5		2.5	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $						3.5		3.5	
$I_{GNDDO} = \begin{bmatrix} Ground Pin \\ Current at Dropout \\ (Note 6) \end{bmatrix} V_{IN} = 4.5V = \begin{bmatrix} 180 \\ -$			I <sub>L</sub> = 250mA	5		9		9	
$\frac{V_{\text{NODO}}}{(\text{Note 6})} = \frac{V_{\text{Note 6}}}{(\text{Note 6})} = \frac{V_{\text{OUT}}}{(\text{Note 7})} = \frac{V_{\text{OUT}}}{(\text{Note 8})} = V_{\text{OUT$						12		12	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		Ground Pin	V <sub>IN</sub> = 4.5V	180		300		300	μA
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		Current at Dropout							
$\frac{\Delta V_{o}}{\Delta P_{D}}$ Thermal Regulation (Note 8) $0.05$ $0.2$ $0$		(Note 6)							
$\Delta V_{0}$ $\Delta P_{D}$ Thermal Regulation(Note 7)800800 $\Delta V_{0}$ $\Delta P_{D}$ Thermal Regulation(Note 8) $0.05$ $0.2$ $0.2$ $0.2$ $\%/W$ $e_{n}$ Output Noise Voltage (10Hz to 100kHz) $I_{L}$ = 100mA $C_{L} = 2.2\mu$ F $400$ $I_{L} = 33\mu$ F $260$ $I_{L} = 100m$ A $I_{L} = 100m$ A $I_{L} = 33\mu$ F $I_{L} = 100m$ A $I_{L} = 100m$ A<	I <sub>limit</sub>	Current Limit	$V_{OUT} = 0V$			750		750	mA
$\begin{array}{c c c c c c c c c c c c c c c c c c c $						800		800	
$e_{n} \qquad Output Noise \qquad C_{L} = 2.2 \mu F \qquad 400 \qquad \qquad$	$\Delta V_{o}$	Thermal Regulation	(Note 8)	0.05		0.2		0.2	%/W
$e_{n} \qquad Output Noise \qquad C_{L} = 2.2 \mu F \qquad 400 \qquad \qquad$	$\overline{\Delta P_{D}}$								
Voltage $(10Hz to 100kHz)$ $C_{L} = 33\mu F$ 260 $I_{L} = 100mA$ 260         260		Output Noise	$C_{L} = 2.2 \mu F$	400					μV RMS
I <sub>L</sub> = 100mA		Voltage							
I <sub>L</sub> = 100mA		(10Hz to 100kHz)	C <sub>L</sub> = 33μF	260					
			-						
Section 5: Data Sheets 132 Designing With LDO Regulators		L							

		МІ	C2954-07	BM	MIC2954-08BM			
Parameter	Conditions	Тур.	Min	Max	Тур.	Min	Max	Units
Reference Voltage		1.235	1.220 <b>1.200</b>	1.250 <b>1.260</b>	1.235	1.210 <b>1.200</b>	1.260 <b>1.270</b>	V V max
Reference Voltage	(Note 9)		1.190	1.270		1.185	1.285	V
Feedback Pin Bias Current		20		40 <b>60</b>	20		40 <b>60</b>	nA
Reference Voltage Temperature Coefficient	(Note 8)	20			50			ppm/°C
Feedback Pin Bias Current Temperature Coefficient		0.1			0.1			nA/°C
Error Comparator								
Output Leakage Current	V <sub>OH</sub> = 30V	0.01		1.00 <b>2.00</b>	0.01		1.00 <b>2.00</b>	μA
Output Low Voltage	V <sub>IN</sub> = 4.5V I <sub>OL</sub> = 400µA	150		250 <b>400</b>	150		250 <b>400</b>	mV
Upper Threshold Voltage	(Note 10)	60	40 <b>25</b>		60	40 <b>25</b>		mV
Lower Threshold Voltage	(Note 10)	75		95 <b>140</b>	75		95 <b>140</b>	mV
Hysteresis	(Note 10)	15			15			mV
Shutdown Input				•	•		1	
Input Logic Voltage	Low (ON) High (OFF)	1.3	2.0	0.7	1.3	2.0	0.7	V
Shutdown Pin Input Current	V <sub>SHUTDOWN</sub> = 2.4V	30		50 <b>100</b>	30		50 <b>100</b>	μΑ
	V <sub>SHUTDOWN</sub> = 30V	450		600 <b>750</b>	450		600 <b>750</b>	μA
Regulator Output Current in Shutdown	(Note 11)	3		10 <b>20</b>	3		10 <b>20</b>	μΑ

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J,(MAX)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_{A}$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{(MAX)} = (T_{J(MAX)} - T_{A}) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The junction to ambient thermal resistance of the MIC2954BM is 160°C/W mounted on a PC board. (See MIC2954BM Thermal Characteristics section for further information. **Note 2:** Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

**Note 3:** Line regulation for the MIC2954 is tested at 125°C for  $I_L = 1 \text{ mA}$ . For  $I_L = 100 \mu \text{A}$  and  $T_J = 125°C$ , line regulation is guaranteed by design to 0.2%. See Typical Performance Characteristics for line regulation versus temperature and load current.

**Note 4:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

**Note 5:** Dropout Voltage is defined as the input to output differential at which the output voltage drops 100 mV below its nominal value measured at 1V differential. At very low values of programmed output voltage, the minimum input supply voltage of 2 V (2.3 V over temperature) must be taken into account.

**Note 6:** Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus the ground pin current.

**Note 7:** The MIC2954 features fold-back current limiting. The short circuit ( $V_{OUT} = 0V$ ) current limit is less than the maximum current with normal output voltage.

**Note 8:** Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 200mA load pulse at  $V_{IN} = 20V$  (a 4W pulse) for T = 10ms.

 $\textbf{Note 9:} \quad \ \ V_{\mathsf{REF}} \leq V_{\mathsf{OUT}} \leq (V_{\mathsf{IN}} - 1 \ \mathsf{V}), \ 2.3 \mathsf{V} \leq V_{\mathsf{IN}} \leq 30\mathsf{V}, \ 100 \ \mu\mathsf{A} < \mathsf{I}_{\mathsf{L}} \leq 250 \ \mathsf{mA}, \ \mathsf{T}_{\mathsf{J}} \leq \mathsf{T}_{\mathsf{J} \ \mathsf{MAX}}.$ 

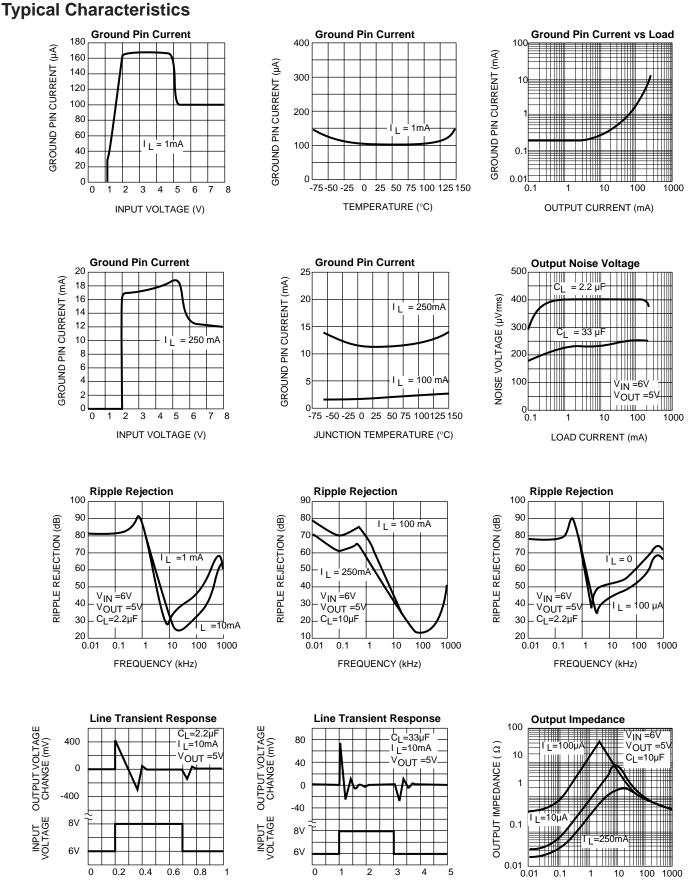
**Note 10:** Comparator thresholds are expressed in terms of a voltage differential at the Feedback terminal below the nominal reference voltage measured at 6V input. To express these thresholds in terms of output voltage change, multiply by the error amplifier gain =  $V_{OUT}$  / $V_{REF}$  = (R1 + R2)/R2. For example, at a programmed output voltage of 5V, the Error output is guaranteed to go low when the output drops by 95 mV x 5V/1.235 V = 384 mV. Thresholds remain constant as a percent of VOUT as VOUT is varied, with the dropout warning occurring at typically 5% below nominal, 7.5% guaranteed.

Note 11:  $V_{SHUTDOWN} \ge 2 V, V_{IN} \le 30 V, V_{OUT} = 0$ , with Feedback pin tied to 5V Tap.

**Note 12:** When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

**Note 13:** Maximum positive supply voltage of 60 V must be of limited duration (< 100 ms) and duty cycle ( $\leq$  1%). The maximum continuous supply voltage is 30 V.

**Note 14:** Thermal resistance ( $\theta_{JC}$ ) of the TO-220 package is 2.5°C/W, and 15°C/W for the SOT-223. Thermal resistance ( $\theta_{JA}$ ) of the TO-92 package is 180°C/W with 0.4" leads and 160°C/W with 0.25" leads.

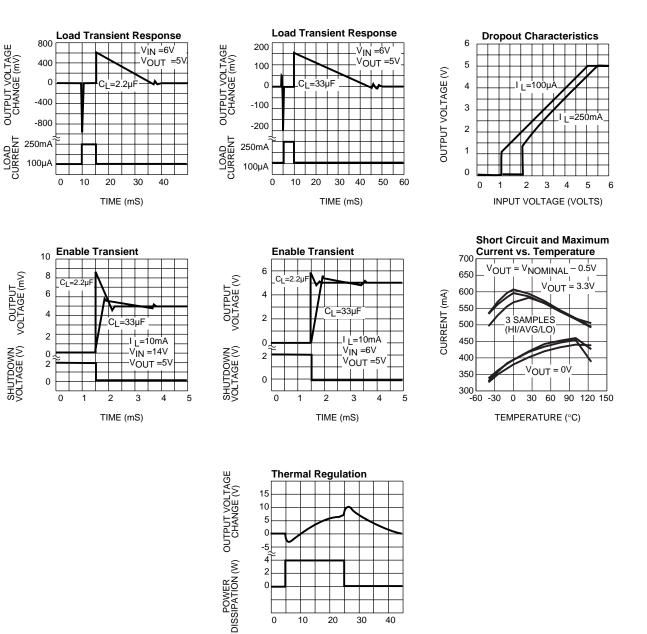


TIME (mS)

135

TIME (mS)

FREQUENCY (kHz)



0

10

20

TIME (mS)

30

40

## **Applications Information**

#### **External Capacitors**

A 2.2 $\mu$ F (or greater) capacitor is required between the MIC2954 output and ground to prevent oscillations due to instability. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, so solid tantalums are recommended for operation below  $-25^{\circ}$ C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.5\mu$ F for current below 10mA or  $0.15\mu$ F for currents below 1 mA. Adjusting the MIC2954-07BM/-08BM to voltages below 5V runs the error amplifier at lower gains so that more output capacitance is needed. For the worst-case situation of a 250mA load at 1.23V output (Output shorted to Feedback) a  $5\mu$ F (or greater) capacitor should be used.

The MIC2954 will remain in regulation with a minimum load of 1mA. When setting the output voltage of the MIC2954-07BM/ -08BM version with external resistors, the current through these resistors may be included as a portion of the minimum load.

A  $0.1\mu$ F capacitor should be placed from the MIC2954 input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

# Error Detection Comparator Output (MIC2954-07BM/-08BM)

A logic low output will be produced by the comparator whenever the MIC2954BM output falls out of regulation by more than approximately 5%. This figure is the comparator's built-in offset of about 60mV divided by the 1.235V reference voltage. (Refer to the block diagram on Page 1). This trip level remains "5% below normal" regardless of the programmed output voltage of the MIC2954-07BM/-08BM. For example, the error flag trip level is typically 4.75V for a 5V output or 11.4V for a 12V output. The out of regulation condition may be due either to low input voltage, current limiting, or thermal limiting.

Figure 1 is a timing diagram depicting the ERROR signal and the regulated output voltage as the MIC2954-07BM/-08BM input is ramped up and down. The ERROR signal becomes valid (low) at about 1.3V input. It goes high at about 5V input (the input voltage at which  $V_{OUT} = 4.75$ ). Since the MIC2954-07BM/-08BM's dropout voltage is load-dependent (see curve in Typical Performance Characteristics), the input voltage trip point (about 5V) will vary with the load current. The output voltage trip point (approximately 4.75V) does not vary with load.

The error comparator has an open-collector output which requires an external pull-up resistor. Depending on system requirements, this resistor may be returned to the 5V output or some other supply voltage. In determining a value for this resistor, note that while the output is rated to sink 400 $\mu$ A, this sink current adds to battery drain in a low battery condition. Suggested values range from 100k to 1M $\Omega$ . The resistor is not required if this output is unused.

# Programming the Output Voltage (MIC2954-07BM/-08BM)

The MIC2954-07BM/-08BM may be pin-strapped for 5V using its internal voltage divider by tying Pin 1 (output) to Pin 2 (sense) and Pin 7 (feedback) to Pin 6 (5V Tap). Alternatively, it may be programmed for any output voltage between its 1.235V reference and its 30V maximum rating. An external pair of resistors is required, as shown in Figure 3.

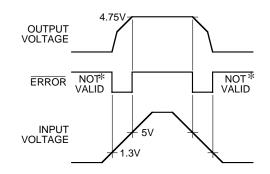
The complete equation for the output voltage is

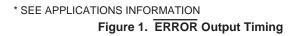
$$V_{OUT} = V_{REF} x \{ 1 + R_1/R_2 \} + I_{FB} R_1$$

where V<sub>REF</sub> is the nominal 1.235 reference voltage and I<sub>FB</sub> is the feedback pin bias current, nominally -20nA. The minimum recommended load current of 1 µA forces an upper limit of 1.2MΩ on the value of R<sub>2</sub>, if the regulator must work with no load (a condition often found in CMOS in standby), I<sub>FB</sub> will produce a 2% typical error in V<sub>OUT</sub> which may be eliminated at room temperature by trimming R<sub>1</sub>. For better accuracy, choosing R<sub>2</sub> = 100k reduces this error to 0.17% while increasing the resistor program current to 12 µA. Since the MIC2954-07BM/-08BM typically draws 60 µA at no load with Pin 2 open-circuited, this is a negligible addition.

#### **Reducing Output Noise**

In reference applications it may be advantageous to reduce the AC noise present at the output. One method is to reduce the regulator bandwidth by increasing the size of the output capacitor. This is relatively inefficient, as increasing the capacitor from 1  $\mu F$  to 220  $\mu F$  only decreases the noise from 430  $\mu V$  to 160  $\mu V_{\text{RMS}}$  for a 100 kHz bandwidth at 5V output.



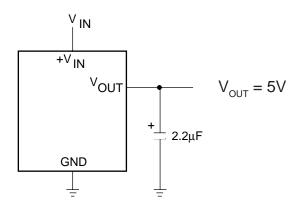


Noise can be reduced fourfold by a bypass capacitor across  $R_1$ , since it reduces the high frequency gain from 4 to unity. Pick:

$$C_{BYPASS} \cong \frac{1}{2\pi R_1 \cdot 200 \text{ Hz}}$$

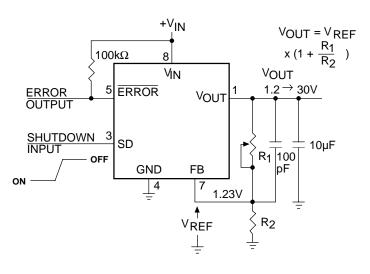
or about 0.01  $\mu$ F. When doing this, the output capacitor must be increased to 3.3  $\mu$ F to maintain stability. These changes reduce the output noise from 430  $\mu$ V to 100  $\mu$ V rms for a 100 kHz bandwidth at 5V output. With the bypass capacitor added, noise no longer scales with output voltage so that improvements are more dramatic at higher output voltages.

## **Typical Applications**



Automotive Applications

The MIC2954 is ideally suited for automotive applications for a variety of reasons. It will operate over a wide range of input voltages with very low dropout voltages (40mV at light loads), and very low quiescent currents (75µA typical). These features are necessary for use in battery powered systems, such as automobiles. It is a "bulletproof" device with the ability to survive both reverse battery (negative transients up to 20V below ground), and load dump (positive transients up to 60V) conditions. A wide operating temperature range with low temperature coefficients is yet another reason to use these versatile regulators in automotive designs.

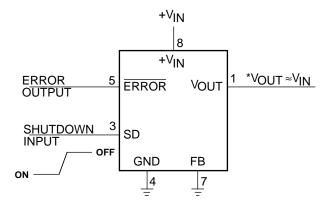


NOTE: PINS 2 AND 6 ARE LEFT OPEN

\*SEE APPLICATIONS INFORMATION

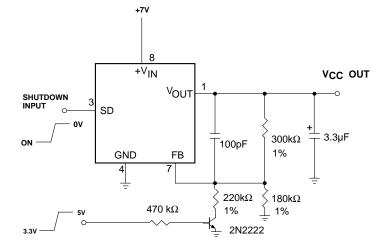
Figure 2. MIC2954 Fixed +5V Regulator

Figure 3. MIC2954-07BM/-08BM Adjustable Regulator



\*MINIMUM INPUT-OUTPUT VOLTAGE RANGES FROM 40mV TO 400mV, DEPENDING ON LOAD CURRENT.

Figure 4. MIC2954-07BM/-08BM Wide Input Voltage Range Current Limiter



PIN 3 LOW= ENABLE OUTPUT. Q1 ON = 3.3V, Q1 OFF = 5.0V.

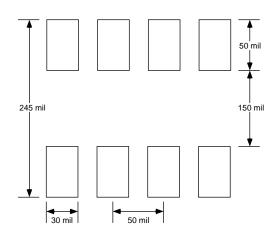
Figure 5. MIC2954-07BM/-08BM 5.0V or 3.3V Selectable Regulator with Shutdown.

## MIC2954-07BM/-08BMThermal Calculations

#### Layout Considerations

The MIC2954-07BM/-08BM (8-Pin Surface Mount Package) has the following thermal characteristics when mounted on a single layer copper-clad printed circuit board.

Pad Layout (minimum recommended geometry)



PC Board Dielectric Material	θ <sub>JA</sub>
FR4	160°C/W
Ceramic	120°C/W

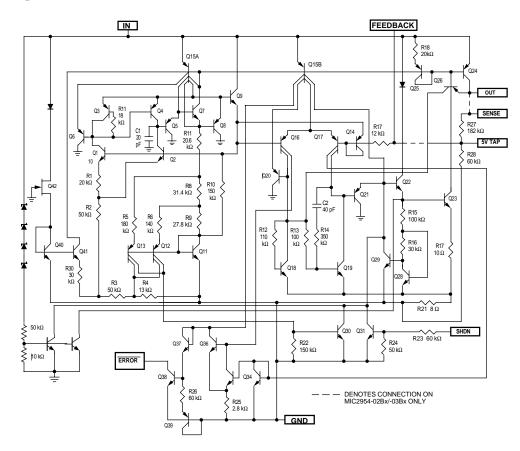
Multi-layer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

Our calculations will use the "worst case" value of  $160^{\circ}$ C/W, which assumes no ground plane, minimum trace widths, and a FR4 material board.

#### Nominal Power Dissipation and Die Temperature

The MIC2954-07BM/-08BM at a 55°C ambient temperature will operate reliably at up to 440mW power dissipation when mounted in the "worst case" manner described above. This power level is equivalent to a die temperature of 125°C, the recommended maximum temperature for non-military grade silicon integrated circuits.

## **Schematic Diagram**





# MIC29150/29300/29500/29750 Series

**High-Current Low-Dropout Regulators** 

## **General Description**

The MIC29150/29300/29500/29750 are high current, high accuracy, low-dropout voltage regulators. Using Micrel's proprietary Super ßeta PNP<sup>™</sup> process with a PNP pass element, these regulators feature 300mV to 370mV (full load) dropout voltages and very low ground current. Designed for high current loads, these devices also find applications in lower current, extremely low dropout-critical systems, where their tiny dropout voltage and ground current values are important attributes.

The MIC29150/29300/29500/29750 are fully protected against overcurrent faults, reversed input polarity, reversed lead insertion, overtemperature operation, and positive and negative transient voltage spikes. Five pin fixed voltage versions feature logic level ON/OFF control and an error flag which signals whenever the output falls out of regulation. Flagged states include low input voltage (dropout), output current limit, overtemperature shutdown, and extremely high voltage spikes on the input.

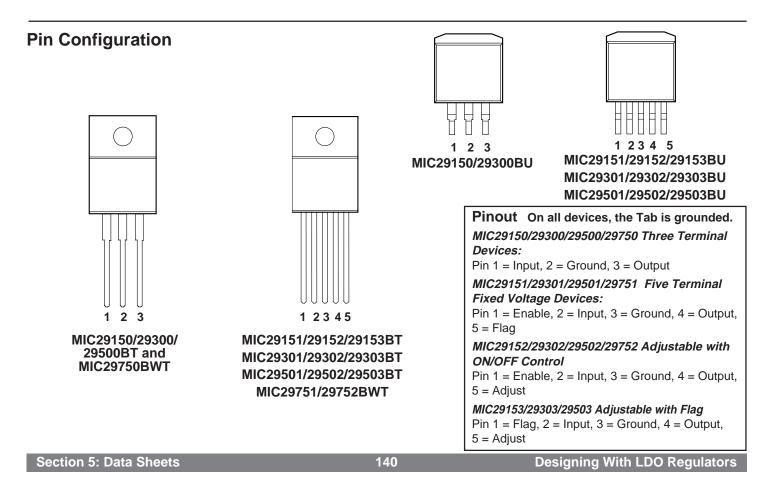
On the MIC29xx1 and MIC29xx2, the ENABLE pin may be tied to V<sub>IN</sub> if it is not required for ON/OFF control. The MIC29150/29300/29500 are available in 3- and 5-pin TO-220 and surface mount TO-263 packages. The MIC29750 7.5A regulators are available in 3- and 5-pin TO-247 packages.

#### Features

- Low Ground Current
- Accurate 1% Guaranteed Tolerance
- Extremely Fast Transient Response
- Reverse-battery and "Load Dump" Protection
- Zero-Current Shutdown Mode (5-Pin versions)
- Error Flag Signals Output Out-of-Regulation (5-Pin versions)
- Also Characterized For Smaller Loads With Industry-Leading Performance Specifications
- Fixed Voltage and Adjustable Versions

### **Applications**

- Battery Powered Equipment
- High-Efficiency "Green" Computer Systems
- Automotive Electronics
- High-Efficiency Linear Power Supplies
- High-Efficiency Post-Regulator For Switching Supply



### **Ordering Information**

MIC29150-3.3BT         -40 to +125°C         3.3         1.5A         TO-220           MIC29150-5.0BT         -40 to +125°C         5.0         1.5A         TO-220           MIC29150-12BT         -40 to +125°C         3.3         1.5A         TO-263           MIC29150-3.3BU         -40 to +125°C         5.0         1.5A         TO-263           MIC29150-3.3BU         -40 to +125°C         12         1.5A         TO-263           MIC29150-12BU         -40 to +125°C         3.3         1.5A         TO-263           MIC29151-3.3BT         -40 to +125°C         3.3         1.5A         TO-220-5           MIC29151-5.0BT         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-12BT         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         4.0         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         3.0A         TO-	Part Number	Temp. Range*	Volts	Current	Package
MIC29150-12BT         -40 to +125°C         12         1.5A         TO-220           MIC29150-3.3BU         -40 to +125°C         3.3         1.5A         TO-263           MIC29150-5.0BU         -40 to +125°C         5.0         1.5A         TO-263           MIC29150-12BU         -40 to +125°C         12         1.5A         TO-263           MIC29151-12BT         -40 to +125°C         3.3         1.5A         TO-220-5           MIC29151-5.0BT         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-5.0BT         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29300-3.3BT         -40 to +125°C         3.0A         TO	MIC29150-3.3BT	–40 to +125°C	3.3	1.5A	TO-220
MIC29150-3.3BU         -40 to +125°C         3.3         1.5A         TO-263           MIC29150-5.0BU         -40 to +125°C         5.0         1.5A         TO-263           MIC29150-12BU         -40 to +125°C         12         1.5A         TO-263           MIC29151-3.3BT         -40 to +125°C         3.3         1.5A         TO-220-5           MIC29151-5.0BT         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-5.0BT         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29153BU         -40 to +125°C         5.0         3.0A <td>MIC29150-5.0BT</td> <td>–40 to +125°C</td> <td>5.0</td> <td>1.5A</td> <td>TO-220</td>	MIC29150-5.0BT	–40 to +125°C	5.0	1.5A	TO-220
MIC29150-5.0BU         -40 to +125°C         5.0         1.5A         TO-263           MIC29150-12BU         -40 to +125°C         12         1.5A         TO-263           MIC29151-3.3BT         -40 to +125°C         3.3         1.5A         TO-220-5           MIC29151-3.3BT         -40 to +125°C         5.0         1.5A         TO-220-5           MIC29151-5.0BT         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-3.3BT         -40 to +125°C         12         3.0A <td>MIC29150-12BT</td> <td>–40 to +125°C</td> <td>12</td> <td>1.5A</td> <td>TO-220</td>	MIC29150-12BT	–40 to +125°C	12	1.5A	TO-220
MIC29150-12BU         -40 to +125°C         12         1.5A         TO-263           MIC29151-3.3BT         -40 to +125°C         3.3         1.5A         TO-220-5           MIC29151-5.0BT         -40 to +125°C         5.0         1.5A         TO-220-5           MIC29151-12BT         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29300-3.3BT         -40 to +125°C         3.0         A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A	MIC29150-3.3BU	–40 to +125°C	3.3	1.5A	TO-263
MIC29151-3.3BT         -40 to +125°C         3.3         1.5A         TO-220-5           MIC29151-5.0BT         -40 to +125°C         5.0         1.5A         TO-220-5           MIC29151-12BT         -40 to +125°C         12         1.5A         TO-220-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29153BU         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         12         3.0A	MIC29150-5.0BU	–40 to +125°C	5.0	1.5A	TO-263
MIC29151-5.0BT         -40 to +125°C         5.0         1.5A         TO-220-5           MIC29151-12BT         -40 to +125°C         12         1.5A         TO-220-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.0         TO-220         MIC29300-3.3BT         -40 to +125°C         3.0         TO-263           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC293	MIC29150-12BU	–40 to +125°C	12	1.5A	TO-263
MIC29151-12BT         -40 to +125°C         12         1.5A         TO-220-5           MIC29151-3.3BU         -40 to +125°C         3.3         1.5A         TO-263-5           MIC29151-5.0BU         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-5.0BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-5.0BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         5.0         3.0A	MIC29151-3.3BT	–40 to +125°C	3.3	1.5A	TO-220-5
MIC29151-3.3BU       -40 to +125°C       3.3       1.5A       TO-263-5         MIC29151-5.0BU       -40 to +125°C       5.0       1.5A       TO-263-5         MIC29151-12BU       -40 to +125°C       12       1.5A       TO-263-5         MIC29152BT       -40 to +125°C       Adj       1.5A       TO-263-5         MIC29152BU       -40 to +125°C       Adj       1.5A       TO-263-5         MIC29152BU       -40 to +125°C       Adj       1.5A       TO-263-5         MIC29153BT       -40 to +125°C       Adj       1.5A       TO-263-5         MIC29153BU       -40 to +125°C       Adj       1.5A       TO-263-5         MIC29300-3.3BT       -40 to +125°C       3.3       3.0A       TO-220         MIC29300-3.3BT       -40 to +125°C       5.0       3.0A       TO-220         MIC29300-5.0BT       -40 to +125°C       12       3.0A       TO-263         MIC29300-3.3BU       -40 to +125°C       3.3       3.0A       TO-263         MIC29300-3.3BU       -40 to +125°C       12       3.0A       TO-263         MIC29300-3.3BU       -40 to +125°C       5.0       3.0A       TO-263         MIC29301-3.3BT       -40 to +125°C       5.0 <td< td=""><td>MIC29151-5.0BT</td><td>–40 to +125°C</td><td>5.0</td><td>1.5A</td><td>TO-220-5</td></td<>	MIC29151-5.0BT	–40 to +125°C	5.0	1.5A	TO-220-5
MIC29151-5.0BU         -40 to +125°C         5.0         1.5A         TO-263-5           MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-5.0BT         -40 to +125°C         12         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.0         A <t< td=""><td>MIC29151-12BT</td><td>–40 to +125°C</td><td>12</td><td>1.5A</td><td>TO-220-5</td></t<>	MIC29151-12BT	–40 to +125°C	12	1.5A	TO-220-5
MIC29151-12BU         -40 to +125°C         12         1.5A         TO-263-5           MIC29152BT         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-3.3BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         3.0         A         TO-263           MIC29300-3.3BU         -40 to +125°C         3.0         A         TO-263           MIC29300-12BU         -40 to +125°C         3.0         A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.0         A         TO-22	MIC29151-3.3BU	–40 to +125°C	3.3	1.5A	TO-263-5
MIC29152BT         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-5.0BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         3.0         A         <	MIC29151-5.0BU	–40 to +125°C	5.0	1.5A	TO-263-5
MIC29152BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29153BT         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-5.0BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         3.3         3.0A	MIC29151-12BU	–40 to +125°C	12	1.5A	TO-263-5
MIC29153BT         -40 to +125°C         Adj         1.5A         TO-220-5           MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-3.0BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-5.0BT         -40 to +125°C         12         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         5.0         3.0A	MIC29152BT	–40 to +125°C	Adj	1.5A	TO-220-5
MIC29153BU         -40 to +125°C         Adj         1.5A         TO-263-5           MIC29300-3.3BT         -40 to +125°C         3.3         3.0A         TO-220           MIC29300-5.0BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-3.3BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.0         A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         3.0         A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         3.0A         TO-263-5 </td <td>MIC29152BU</td> <td>–40 to +125°C</td> <td>Adj</td> <td>1.5A</td> <td>TO-263-5</td>	MIC29152BU	–40 to +125°C	Adj	1.5A	TO-263-5
MIC29300-3.3BT       -40 to +125°C       3.3       3.0A       TO-220         MIC29300-5.0BT       -40 to +125°C       5.0       3.0A       TO-220         MIC29300-12BT       -40 to +125°C       12       3.0A       TO-220         MIC29300-3.3BU       -40 to +125°C       3.3       3.0A       TO-263         MIC29300-3.3BU       -40 to +125°C       3.3       3.0A       TO-263         MIC29300-5.0BU       -40 to +125°C       5.0       3.0A       TO-263         MIC29300-12BU       -40 to +125°C       12       3.0A       TO-263         MIC29301-3.3BT       -40 to +125°C       3.3       3.0A       TO-220-5         MIC29301-3.3BT       -40 to +125°C       3.3       3.0A       TO-220-5         MIC29301-3.3BT       -40 to +125°C       5.0       3.0A       TO-220-5         MIC29301-3.3BU       -40 to +125°C       12       3.0A       TO-220-5         MIC29301-3.3BU       -40 to +125°C       12       3.0A       TO-263-5         MIC29301-3.3BU       -40 to +125°C       3.3       3.0A       TO-263-5         MIC29301-3.3BU       -40 to +125°C       5.0       3.0A       TO-263-5         MIC29301-3.3BU       -40 to +125°C       5.	MIC29153BT	–40 to +125°C	Adj	1.5A	TO-220-5
MIC29300-5.0BT         -40 to +125°C         5.0         3.0A         TO-220           MIC29300-12BT         -40 to +125°C         12         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-5.0BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         5.0         3.0A	MIC29153BU	–40 to +125°C	Adj	1.5A	TO-263-5
MIC29300-12BT         -40 to +125°C         12         3.0A         TO-220           MIC29300-3.3BU         -40 to +125°C         3.3         3.0A         TO-263           MIC29300-5.0BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-263-5 </td <td>MIC29300-3.3BT</td> <td>–40 to +125°C</td> <td>3.3</td> <td>3.0A</td> <td>TO-220</td>	MIC29300-3.3BT	–40 to +125°C	3.3	3.0A	TO-220
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	MIC29300-5.0BT	–40 to +125°C	5.0	3.0A	TO-220
MIC29300-5.0BU         -40 to +125°C         5.0         3.0A         TO-263           MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj	MIC29300-12BT	–40 to +125°C	12	3.0A	TO-220
MIC29300-12BU         -40 to +125°C         12         3.0A         TO-263           MIC29301-3.3BT         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-263-5	MIC29300-3.3BU	–40 to +125°C	3.3	3.0A	TO-263
MIC29301-3.3BT         -40 to +125°C         3.3         3.0A         TO-220-5           MIC29301-5.0BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-263-5	MIC29300-5.0BU	–40 to +125°C	5.0	3.0A	TO-263
MIC29301-5.0BT         -40 to +125°C         5.0         3.0A         TO-220-5           MIC29301-12BT         -40 to +125°C         12         3.0A         TO-220-5           MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-263-5	MIC29300-12BU	–40 to +125°C	12	3.0A	TO-263
MIC29301-12BT       -40 to +125°C       12       3.0A       TO-220-5         MIC29301-3.3BU       -40 to +125°C       3.3       3.0A       TO-263-5         MIC29301-5.0BU       -40 to +125°C       5.0       3.0A       TO-263-5         MIC29301-12BU       -40 to +125°C       12       3.0A       TO-263-5         MIC29302BT       -40 to +125°C       12       3.0A       TO-263-5         MIC29302BT       -40 to +125°C       Adj       3.0A       TO-220-5         MIC29302BU       -40 to +125°C       Adj       3.0A       TO-263-5         MIC29302BU       -40 to +125°C       Adj       3.0A       TO-263-5         MIC29302BU       -40 to +125°C       Adj       3.0A       TO-220-5         MIC29303BT       -40 to +125°C       Adj       3.0A       TO-220-5	MIC29301-3.3BT	–40 to +125°C	3.3	3.0A	TO-220-5
MIC29301-3.3BU         -40 to +125°C         3.3         3.0A         TO-263-5           MIC29301-5.0BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-220-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-263-5	MIC29301-5.0BT	–40 to +125°C	5.0	3.0A	TO-220-5
MIC29301-5.0BU         -40 to +125°C         5.0         3.0A         TO-263-5           MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-220-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-263-5	MIC29301-12BT	–40 to +125°C	12	3.0A	TO-220-5
MIC29301-12BU         -40 to +125°C         12         3.0A         TO-263-5           MIC29302BT         -40 to +125°C         Adj         3.0A         TO-220-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-220-5	MIC29301-3.3BU	–40 to +125°C	3.3	3.0A	TO-263-5
MIC29302BT         -40 to +125°C         Adj         3.0A         TO-220-5           MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-220-5	MIC29301-5.0BU	-40 to +125°C	5.0	3.0A	TO-263-5
MIC29302BU         -40 to +125°C         Adj         3.0A         TO-263-5           MIC29303BT         -40 to +125°C         Adj         3.0A         TO-220-5	MIC29301-12BU	-40 to +125°C	12	3.0A	TO-263-5
MIC29303BT -40 to +125°C Adj 3.0A TO-220-5	MIC29302BT	-40 to +125°C	Adj	3.0A	TO-220-5
-	MIC29302BU	–40 to +125°C	Adj	3.0A	TO-263-5
MIC29303BU -40 to +125°C Adj 3.0A TO-263-5	MIC29303BT	-40 to +125°C	Adj	3.0A	TO-220-5
	MIC29303BU	-40 to +125°C	Adj	3.0A	TO-263-5

Part Number	Temp. Range*	Volts	Current	Package
MIC29500-3.3BT	–40 to +125°C	3.3	5.0A	TO-220
MIC29500-5.0BT	–40 to +125°C	5.0	5.0A	TO-220
MIC29501-3.3BT	–40 to +125°C	3.3	5.0A	TO-220-5
MIC29501-5.0BT	–40 to +125°C	5.0	5.0A	TO-220-5
MIC29501-3.3BU	–40 to +125°C	3.3	5.0A	TO-263-5
MIC29501-5.0BU	–40 to +125°C	5.0	5.0A	TO-263-5
MIC29502BT	–40 to +125°C	Adj	5.0A	TO-220-5
MIC29502BU	–40 to +125°C	Adj	5.0A	TO-263-5
MIC29503BT	–40 to +125°C	Adj	5.0A	TO-220-5
MIC29503BU	–40 to +125°C	Adj	5.0A	TO-263-5
MIC29750-3.3BWT	–40 to +125°C	3.3	7.5A	TO-247-3
MIC29750-5.0BWT	–40 to +125°C	5.0	7.5A	TO-247-3
MIC29751-3.3BWT	–40 to +125°C	3.3	7.5A	TO-247-5
MIC29751-5.0BWT	–40 to +125°C	5.0	7.5A	TO-247-5
MIC29752BWT	–40 to +125°C	Adj	7.5A	TO-247-5

\* Junction Temperature

MIC29xx0 versions are 3-terminal fixed voltage devices. MIC29xx1 are fixed voltage devices with ENABLE and ERROR flag. MIC29xx2 are adjustable regulators with ENABLE control. MIC29xx3 are adjustables with an ERROR flag.

## **Absolute Maximum Ratings**

Power Dissipation	Internally Limited
Lead Temperature (Soldering, 5 seconds	s) 260°C
Storage Temperature Range	–65°C to +150°C
Input Supply Voltage (Note 1)	–20V to +60V

## **Operating Ratings**

Operating Junction Temperature40°	C to +125°C
Maximum Operating Input Voltage	26V
TO-220 θ <sub>.IC</sub>	2°C/W
TO-263 θ <sub>IC</sub>	2°C/W
TO-263 $\theta_{JC}$ TO-247 $\theta_{JC}$	1.5°C/W

## **Electrical Characteristics**

All measurements at  $T_J = 25^{\circ}$ C unless otherwise noted. **Bold** values are guaranteed across the operating temperature range. Adjustable versions are programmed to 5.0V.

Parameter	Condition	Min	Тур	Max	Units
Output Voltage	I <sub>O</sub> = 10mA	-1		1	%
	$10\text{mA} \le \text{I}_{O} \le \text{I}_{FL}$ , $(\text{V}_{OUT} + 1\text{V}) \le \text{V}_{IN} \le 26\text{V}$ (Note 2)	-2		2	%
Line Regulation	$I_0 = 10mA$ , $(V_{OUT} + 1V) \le V_{IN} \le 26V$		0.06	0.5	%
Load Regulation	$V_{IN} = V_{OUT} + 5V$ , $10mA \le I_{OUT} \le I_{FULL \ LOAD}$ (Note 2, 6)		0.2	1	%
ΔV <sub>o</sub> ΔT	Output Voltage (Note 6) Temperature Coef.		20	100	ppm/°C
Dropout Voltage	$\begin{array}{c} \Delta V_{OUT} = -1\%, \mbox{ (Note 3)} \\ MIC29150 & I_O = 100mA \\ & I_O = 750mA \\ & I_O = 1.5A \\ MIC29300 & I_O = 100mA \\ & I_O = 1.5A \\ & I_O = 3A \\ MIC29500 & I_O = 250mA \\ & I_O = 2.5A \\ & I_O = 5A \\ MIC29750 & I_O = 250mA \\ & I_O = 4A \\ & I_O = 7.5A \end{array}$		80 220 350 80 250 370 125 250 370 80 270 425	200 600 175 600 250 600 200 600	mV
Ground Current	$ \begin{array}{ll} MIC29150 & I_{O} = 750mA,  V_{IN} = V_{OUT} + 1V \\ I_{O} = 1.5A \\ MIC29300 & I_{O} = 1.5A,  V_{IN} = V_{OUT} + 1V \\ I_{O} = 3A \\ MIC29500 & I_{O} = 2.5A,  V_{IN} = V_{OUT} + 1V \\ I_{O} = 5A \\ MIC29750 & I_{O} = 4A,  V_{IN} = V_{OUT} + 1V \\ I_{O} = 7.5A \end{array} $		8 22 10 37 15 70 35 120	20 35 50 75	mA mA mA mA
I <sub>GNDDO</sub> Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than specified $V_{OUT}$ . $I_{OUT} = 10$ mA MIC29150 MIC29300 MIC29500 MIC29750		0.9 1.7 2.1 3.1		mA mA mA mA
Current Limit	$ \begin{array}{lll} \mbox{MIC29150} & V_{OUT} = 0V \mbox{ (Note 4)} \\ \mbox{MIC29300} & V_{OUT} = 0V \mbox{ (Note 4)} \\ \mbox{MIC29500} & V_{OUT} = 0V \mbox{ (Note 4)} \\ \mbox{MIC29750} & V_{OUT} = 0V \mbox{ (Note 4)} \\ \end{array} $		2.1 4.5 7.5 9.5	3.5 5.0 10.0 15	A A A A
e <sub>n</sub> , Output Noise Voltage (10Hz to 100kHz) I <sub>L</sub> = 100mA	$C_L = 10\mu F$ $C_L = 33\mu F$		400 260		μV RMS

#### Electrical Characteristics (Continued) Reference MIC29xx2/MIC29xx3

Reference	WIG29XX2/WIG29XX3				
Parameter	Conditions	Min	Typical	Max	Units
Reference Voltage		1.228 <b>1.215</b>	1.240	1.252 <b>1.265</b>	V V max
Reference Voltage	(Note 8)	1.203		1.277	V
Adjust Pin Bias Current			40	80 <b>120</b>	nA
Reference Voltage Temperature Coefficient	(Note 7)		20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C

#### Flag Output (Error Comparator) MIC29xx1/29xx3

Output Leakage Current	$V_{OH} = 26V$		0.01	1.00 <b>2.00</b>	μA
Output Low Voltage	Device set for 5V. $V_{IN} = 4.5V$ $I_{OL} = 250\mu A$		220	300 <b>400</b>	mV
Upper Threshold Voltage	Device set for 5V (Note 9)	40 <b>25</b>	60		mV
Lower Threshold Voltage	Device set for 5V (Note 9)		75	95 <b>140</b>	mV
Hysteresis	Device set for 5V (Note 9)		15		mV

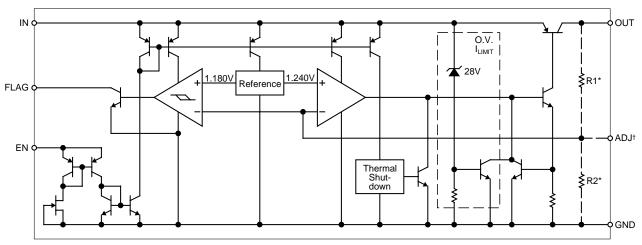
#### ENABLE Input MIC29xx1/MIC29xx2

Input Logic Voltage Low (OFF) High (ON)		2.4		0.8	V
Enable Pin Input Current	V <sub>EN</sub> = 26V		100	600 <b>750</b>	μA
	V <sub>EN</sub> =0.8V			1 <b>2</b>	μA
Regulator Output Current in Shutdown	(Note 10)		10	500	μΑ

#### Notes

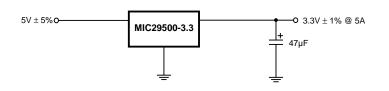
- Note 1: Maximum positive supply voltage of 60V must be of limited duration (<100msec) and duty cycle (<1%). The maximum continuous supply voltage is 26V.
- Note 2: Full Load current (I<sub>FL</sub>) is defined as 1.5A for the MIC29150, 3A for the MIC29300, 5A for the MIC29500, and 7.5A for the MIC29750 families.
- Note 3: Dropout voltage is defined as the input-to-output differential when the output voltage drops to 99% of its nominal value with V<sub>OUT</sub> + 1V applied to V<sub>IN</sub>
- Note 4:  $V_{IN} = V_{OUT (nominal)} + 1V$ . For example, use  $V_{IN} = 4.3V$  for a 3.3V regulator or use 6V for a 5V regulator. Employ pulse-testing procedures to minimize temperature rise.
- Note 5: Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus the ground pin current.
- Note 6: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.
- Note 7: Thermal regulation is defined as the change in output voltage at a time T after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 200mA load pulse at V<sub>IN</sub> = 20V (a 4W pulse) for T = 10ms.
- Note 8:  $V_{REF} \le V_{OUT} \le (V_{IN} 1 \ V), 2.3V \le V_{IN} \le 26V, 10mA < I_L \le I_{FL}, T_J \le T_{J \ MAX.}$
- **Note 9:** Comparator thresholds are expressed in terms of a voltage differential at the Adjust terminal below the nominal reference voltage measured at 6V input. To express these thresholds in terms of output voltage change, multiply by the error amplifier gain =  $V_{OUT} / V_{REF} = (R1 + R2)/R2$ . For example, at a programmed output voltage of 5V, the Error output is guaranteed to go low when the output drops by 95 mV x 5V/1.240 V = 384 mV. Thresholds remain constant as a percent of  $V_{OUT}$  as  $V_{OUT}$  is varied, with the dropout warning occurring at typically 5% below nominal, 7.7% guaranteed.
- Note 10:  $V_{EN} \le 0.8V$  and  $V_{IN} \le 26V$ ,  $V_{OUT} = 0$ .
- Note 11: When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

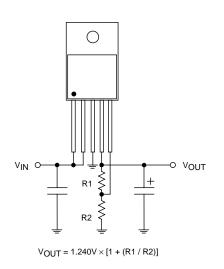
## **Block Diagram**



\* Feedback network in fixed versions only
 † Adjustable version only

## **Typical Applications**

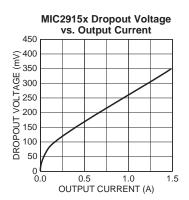


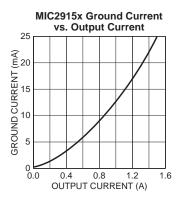


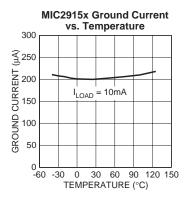
#### Figure 1. Fixed output voltage.

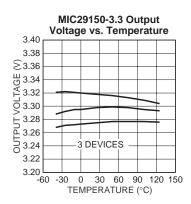
Figure 2. Adjustable output voltage configuration. For best results, the total series resistance should be small enough to pass the minimum regulator load current.

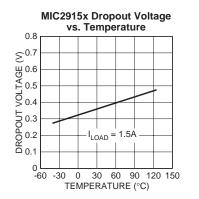
# **Typical Characteristics MIC2915x**

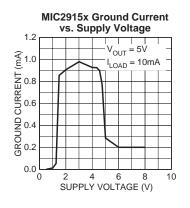












MIC2915x Ground Current

vs. Temperature

= 250mA

TEMPERATURE (°C)

30 60 90 120 150

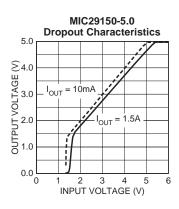
LOAD

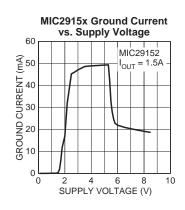
0.0 -60 -30 0

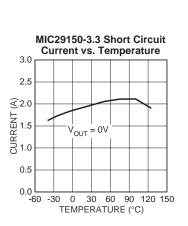
2.5

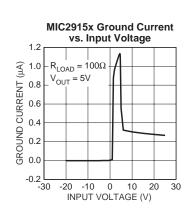
€ 2.0

GROUND CURRENT ( 9.0 1.0 0.5

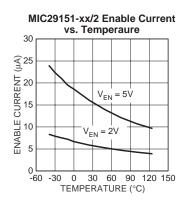


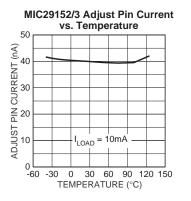


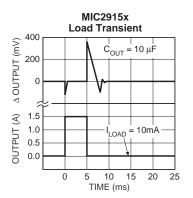


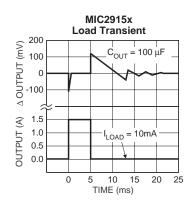


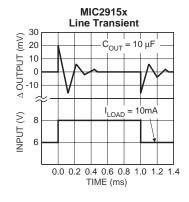


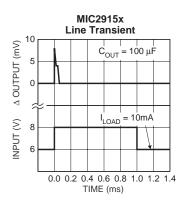








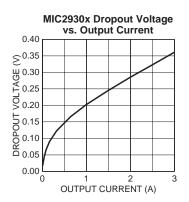


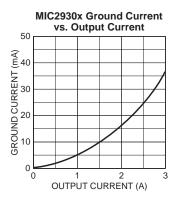


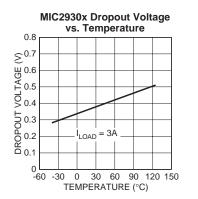
MIC2915x Output Impedance ys. Frequency

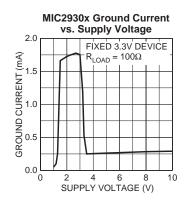
146

# **Typical Characteristics MIC2930x**









MIC2930x Ground Current

vs. Temperature

 $I_{OUT} = 250 \text{mA}$ 

TEMPERATURE (°C)

2.0

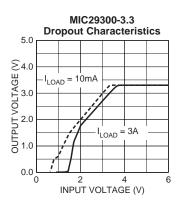
1.5

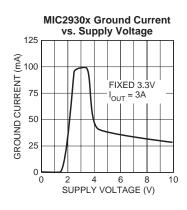
1.0

0.5

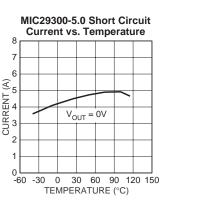
0.0 -60 -30 0

**GROUND CURRENT (mA)** 

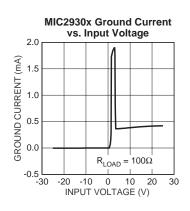




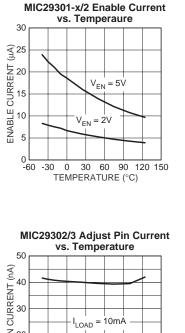
MIC2930x Ground Current vs. Temperature

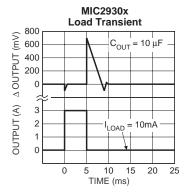


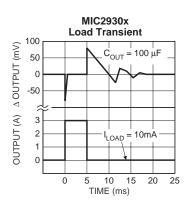
30 60 90 120 150

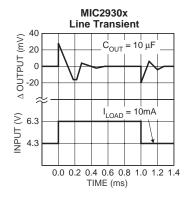


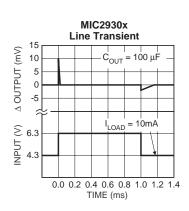
TEMPERATORE (C)



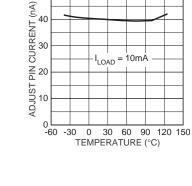




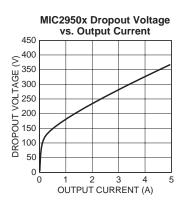


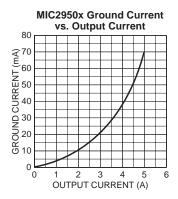


 $\underset{(t)}{\text{MIC2930x Output Impedance vs. Frequency}}{(t)} \underbrace{\underset{(t)}{10}}_{0.01} \underbrace{\underset{(t)}{10}}_$ 



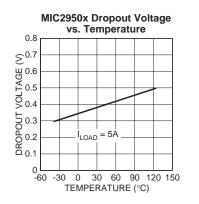
# **Typical Characteristics MIC2950x**

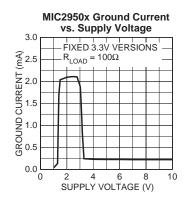




MIC2950x Ground Current vs. Temperature 0.5 € 10.4 GROUND CURRENT 0.3 0.0  $I_{OUT} = 10 \text{mÅ}$ 0.0 -30 0 30 60 90 120 150 TEMPERATURE (°C)

MIC29500-3.3 Output Voltage vs. Temperature 3.40 3.38 ≥3.36 B 3.34 B 3.32 V 3.32 > 1.28 1.28 3.28 3.26 3.24 3.22 3.20 30 60 90 120 150 -60 -30 0 TEMPERATURE (°C)





MIC2950x Ground Current

vs. Temperature

I<sub>OUT</sub> = 500mA

TEMPERATURE (°C)

MIC2950x-5.0 Short Circuit

Current vs. Temperature

 $V_{OUT} = 0V$ 

30 60 90 120 150

30 60 90 120 150

4

3

0 -60 -30

10

9

8

7

6 5

4 3

2

1

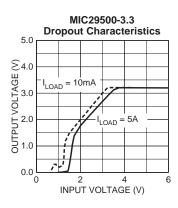
0

-30 0 -60

CURRENT (A)

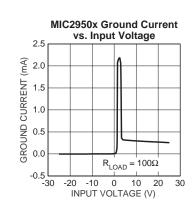
0

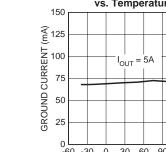
**GROUND CURRENT** (mA)



MIC2950x Ground Current vs. Supply Voltage 125 € 100 **GROUND CURRENT** 75 50 FIXED 3.3V VERSION 25  $I_{LOAD} = 5A$ 0 0 2 3 4 5 SUPPLY VOLTAGE (V)

MIC2950x Ground Current vs. Temperature 150  $I_{OUT} = 5A$ 0 L -60 -30 0 30 60 90 120 150

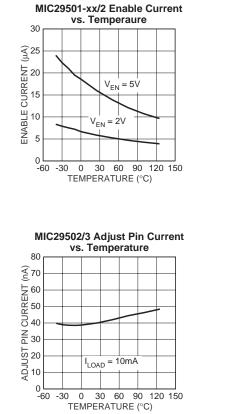


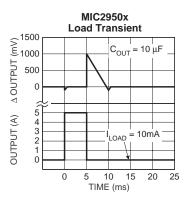


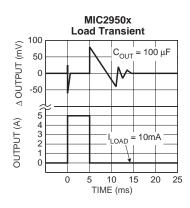
TEMPERATURE (°C)

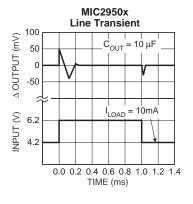
**Section 5: Data Sheets** 

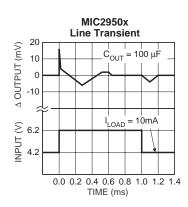
TEMPERATURE (°C)





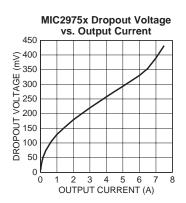


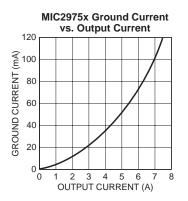




 $\underset{(t)}{\text{MIC2950x Output Impedance}}_{vs. Frequency}$ 

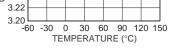
# **Typical Characteristics MIC2975x**

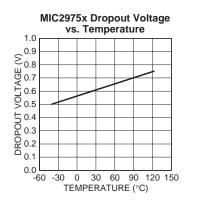


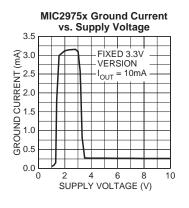


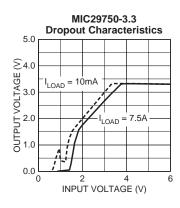
MIC2975x Ground Current vs. Temperature 0.5 € 2.0  $I_{OUT} = 10 \text{mÅ}$ 0.0 ∟ -60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

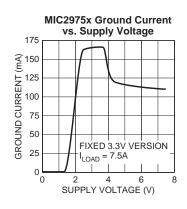
MIC29750-3.3 Output Voltage vs. Temperature 3.40 3.38 ≥3.36 B 3.34 B 3.32 V 3.32 > 1.28 1.28 3.28 3.26 3.24 



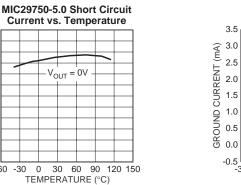


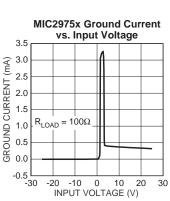




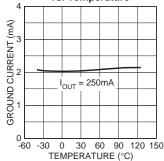


MIC2975x Ground Current vs. Temperature 200 **GROUND CURRENT (mA)** 150  $I_{OUT} = 7.5A$ 100 50 0 L -60 -30 0 30 60 90 120 150 TEMPERATURE (°C)





MIC2975x Ground Current vs. Temperature



12

11

10

9

4 3

2

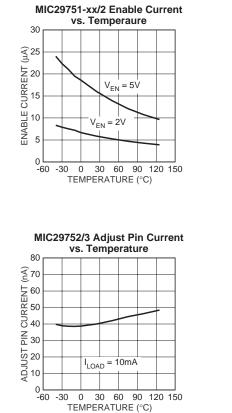
1

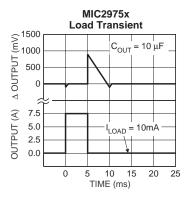
0

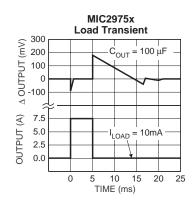
-60

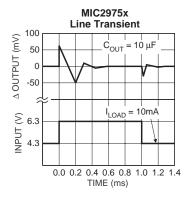
-30 0

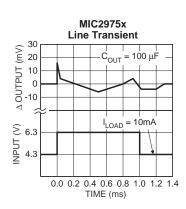
CURRENT (A)











MIC2975x Output Impedance ys. Frequency

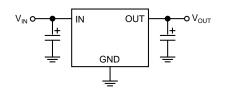
### **Applications Information**

The MIC29150/29300/29500/29750 are high performance low-dropout voltage regulators suitable for all moderate to high-current voltage regulator applications. Their 300mV to 400mV dropout voltage at full load make them especially valuable in battery powered systems and as high efficiency noise filters in "post-regulator" applications. Unlike older NPN-pass transistor designs, where the minimum dropout voltage is limited by the base-emitter voltage drop and collector-emitter saturation voltage, dropout performance of the PNP output of these devices is limited merely by the low  $V_{CF}$  saturation voltage.

A trade-off for the low dropout voltage is a varying base drive requirement. But Micrel's Super ßeta PNP<sup>™</sup> process reduces this drive requirement to merely 1% of the load current.

The MIC29150–29750 family of regulators is fully protected from damage due to fault conditions. Current limiting is provided. This limiting is linear; output current under overload conditions is constant. Thermal shutdown disables the device when the die temperature exceeds the 125°C maximum safe operating temperature. Transient protection allows device (and load) survival even when the input voltage spikes between –20V and +60V. When the input voltage exceeds about 35V to 40V, the overvoltage sensor temporarily disables the regulator. The output structure of these regulators allows voltages in excess of the desired output voltage to be applied without reverse current flow. MIC29xx1 and MIC29xx2 versions offer a logic level ON/OFF control: when disabled, the devices draw nearly zero current.

An additional feature of this regulator family is a common pinout: a design's current requirement may change up or down yet use the same board layout, as all of these regulators have identical pinouts.



# Figure 3. Linear regulators require only two capacitors for operation.

#### Thermal Design

Linear regulators are simple to use. The most complicated design parameters to consider are thermal characteristics. Thermal design requires the following application-specific parameters:

- Maximum ambient temperature, T<sub>A</sub>
- Output Current, I<sub>OUT</sub>
- Output Voltage, V<sub>OUT</sub>
- Input Voltage, V<sub>IN</sub>

Section 5: Data Sheets

$$P_{D} = I_{OUT} \left( 1.01 V_{IN} - V_{OUT} \right)$$

Where the ground current is approximated by 1% of  $\rm I_{OUT}.$  Then the heat sink thermal resistance is determined with this formula:

$$\theta_{SA} = \frac{T_{J MAX} - T_{A}}{P_{D}} - \left(\theta_{JC} + \theta_{CS}\right)$$

Where  $T_{J\;MAX} \leq 125^{\circ}C$  and  $\theta_{CS}$  is between 0 and 2°C/W.

The heat sink may be significantly reduced in applications where the minimum input voltage is known and is large compared with the dropout voltage. Use a series input resistor to drop excessive voltage and distribute the heat between this resistor and the regulator. The low dropout properties of Micrel Super ßeta PNP regulators allow very significant reductions in regulator power dissipation and the associated heat sink without compromising performance. When this technique is employed, a capacitor of at least  $0.1\mu$ F is needed directly between the input and regulator ground.

Please refer to Application Note 9 and Application Hint 17 for further details and examples on thermal design and heat sink specification.

#### **Capacitor Requirements**

For stability and minimum output noise, a capacitor on the regulator output is necessary. The value of this capacitor is dependent upon the output current; lower currents allow smaller capacitors. MIC29150—29750 regulators are stable with the following minimum capacitor values at full load:

Device	Full Load Capacitor
MIC29150	10μF
MIC29300	10μF
MIC29500	10μF
MIC29750	22μF

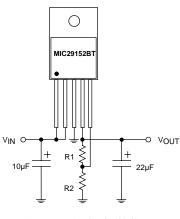
This capacitor need not be an expensive low ESR type: aluminum electrolytics are adequate. In fact, extremely low ESR capacitors may contribute to instability. Tantalum capacitors are recommended for systems where fast load transient response is important.

Where the regulator is powered from a source with a high AC impedance, a  $0.1\mu$ F capacitor connected between Input and GND is recommended. This capacitor should have good characteristics to above 250kHz.

#### **Minimum Load Current**

The MIC29150–29750 regulators are specified between finite loads. If the output current is too small, leakage currents dominate and the output voltage rises. The following minimum load current swamps any expected leakage current across the operating temperature range:

#### Adjustable Regulator Design



 $V_{OUT} = 1.235V \times [1 + (R1 / R2)]$ 

#### Figure 4. Adjustable Regulator with Resistors

The adjustable regulator versions, MIC29xx2 and MIC29xx3, allow programming the output voltage anywhere between 1.25V and the 26V maximum operating rating of the family.

Two resistors are used. Resistors can be quite large, up to  $1M\Omega$ , because of the very high input impedance and low bias current of the sense comparator: The resistor values are calculated by:

$$R_1 = R_2 \left( \frac{V_{OUT}}{1.240} - 1 \right)$$

Where  $V_0$  is the desired output voltage. Figure 4 shows component definition. Applications with widely varying load currents may scale the resistors to draw the minimum load current required for proper operation (see above).

#### **Error Flag**

MIC29xx1 and MIC29xx3 versions feature an Error Flag, which looks at the output voltage and signals an error condition when this voltage drops 5% below its expected value. The error flag is an open-collector output that pulls low under fault conditions. It may sink 10mA. Low output voltage signifies a number of possible problems, including an overcurrent fault (the device is in current limit) and low input voltage. The flag output is inoperative during overtemperature shutdown conditions.

#### Enable Input

MIC29xx1 and MIC29xx2 versions feature an enable (EN) input that allows ON/OFF control of the device. Special design allows "zero" current drain when the device is disabled—only microamperes of leakage current flows. The EN input has TTL/CMOS compatible thresholds for simple interfacing with logic, or may be directly tied to  $\leq$  30V. Enabling the regulator requires approximately 20µA of current.



# MIC29310/29312

#### **3A Fast-Response LDO Regulator**

#### **Preliminary Information**

### **General Description**

The MIC29310 and MIC29312 are high-current, high-accuracy, low-dropout voltage regulators featuring fast transient recovery from input voltage surges and output load current changes. These regulators use a PNP pass element that features Micrel's proprietary Super ßeta PNP<sup>™</sup> process.

The MIC29310/2 is available in two versions: the three-pin fixed output MIC29310 and the five pin adjustable output voltage MIC29312. All versions are fully protected against overcurrent faults, reversed input polarity, reversed lead insertion, overtemperature operation, and positive and negative transient voltage spikes.

A TTL compatible enable (EN) control pin supports external on/off control. If on/off control is not required, the device may be continuously enabled by connecting EN to IN.

The MIC29310/2 is available in the standard three and five pin TO-220 package with an operating junction temperature range of  $0^{\circ}$ C to +125°C.

For applications requiring even lower dropout voltage, input voltage greater than 16V, or an error flag, see the MIC29300/29301/29302/29303.

### Features

- Fast transient response
- 3A current over full temperature range
- 600mV dropout voltage at full load
- Low ground current
- Accurate 1% guaranteed tolerance
- "Zero" current shutdown mode (MIC29312)
- Fixed voltage and adjustable versions

#### Applications

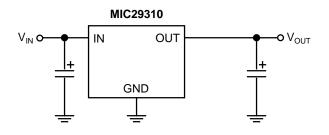
- Pentium<sup>™</sup> and Power PC<sup>™</sup> processor supplies
- High-efficiency "green" computer systems
- High-efficiency linear power supplies
- High-efficiency switching supply post regulator
- Battery-powered equipment

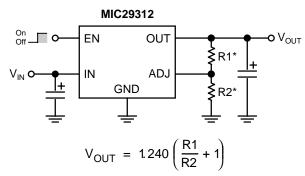
#### **Ordering Information**

Part Number	Temp. Range*	Voltage	Current	Package
MIC29310-3.3BT	0°C to +125°C	3.3V	3.0A	TO-220-3
MIC29310-5.0BT	0°C to +125°C	5.0V	3.0A	TO-220-3
MIC29312BT	0°C to +125°C	Adj.	3.0A	TO-220-5

Junction Temperature

### **Typical Application**





\* For best performance, total series resistance (R1 + R2) should be small enough to pass the minimum regulator load current of 10mA.

**Fixed Regulator Configuration** 

#### Adjustable Regulator Configuration

### **Pin Configuration**



On all devices, the Tab is grounded.

### Pin Description 3-Pin TO-220 (MIC29310)

Pin Number	Pin Name	Pin Function	
1	IN	Unregulated Input: +16V maximum supply.	
2	GND	Ground: Internally connected to tab (ground).	
3	OUT	Regulated Output	

#### 5-Pin TO-220 (MIC29312)

Pin Number	Pin Name	Pin Function	
1	EN Enable (Input): Logic-level ON/OFF control.		
2	IN Unregulated Input: +16V maximum supply.		
3	GND	GND Ground: Internally connected to tab (ground).	
4	OUT	Regulated Output	
5	ADJ	Output Voltage Adjust: 1.240V feedback from external resistive divider.	

### **Absolute Maximum Ratings**

Input Supply Voltage (Note 1)	–20V to +20V
Power Dissipation	Internally Limited
Storage Temperature Range	–65°C to +150°C
Lead Temperature (Soldering, 5 sec.)	260°C

### **Operating Ratings**

Operating Junction Temperature	0°C to +125°C
θ <sub>JC</sub> (TO-220)	2°C/W
θ <sub>JA</sub> (TO-220)	55°C/W

### **Electrical Characteristics**

All measurements at  $T_J = 25^{\circ}C$  unless otherwise noted. **Bold** values are guaranteed across the operating temperature range.

Parameter	Condition	Min	Тур	Max	Units
Output Voltage	$10\text{mA} \le \text{I}_{\text{O}} \le \text{I}_{\text{FL}}, (\text{V}_{\text{OUT}} + 1\text{V}) \le \text{V}_{\text{IN}} \le 8\text{V} \text{ (Note 2)}$			2	%
Line Regulation	$I_{O} = 10 \text{mA}, (V_{OUT} + 1 \text{V}) \le V_{IN} \le 16 \text{V}$		0.06	0.5	%
Load Regulation	$V_{IN} = V_{OUT} + 1V$ , $10mA \le I_{OUT} \le I_{FULL \ LOAD}$ (Notes 2, 6)		0.2	1	%
$\Delta V_O / \Delta T$	Output Voltage Temperature Coefficient (Note 6)		20	100	ppm/°C
Dropout Voltage	$ \Delta V_{OUT} = -1\%, \text{ (Note 3)} \\ \text{MIC29310/29312 } I_{O} = 100\text{mA} \\ I_{O} = 750\text{mA} \\ I_{O} = 1.5\text{A} \\ I_{O} = 3\text{A} \\ \end{tabular} $		80 220 330 600	200 1000	mV mV mV mV
Ground Current	MIC29310/29312 $I_0 = 750$ mA, $V_{IN} = V_{OUT} + 1V$ $I_0 = 1.5A$ $I_0 = 3A$		5 15 60	20 150	mA mA mA
I <sub>GNDDO</sub> Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than specified $V_{OUT}$ . $I_{OUT} = 10$ mA		2	3	mA
Current Limit	MIC29310/29312 V <sub>OUT</sub> = 0V (Note 4)	3.0	3.8		A
Minimum Load Current			7	10	mA
e <sub>n</sub> , Output Noise Voltage (10Hz to 100kHz) I <sub>L</sub> = 100mA	$C_{L} = 10\mu F$ $C_{L} = 33\mu F$		400 260		$\mu V_{RMS} \ \mu V_{RMS}$

#### Reference (MIC29312 only)

Reference Voltage	$10\text{mA} \le \text{I}_{O} \le \text{I}_{FL}, \text{ V}_{OUT} + 1\text{V} \le \text{V}_{IN} \le 8\text{V} \text{ (Note 2)}$	1.215		1.265	V <sub>MAX</sub>
Adjust Pin Bias Current			40	80 <b>120</b>	nA nA
Reference Voltage Temperature Coefficient	(Note 7)		20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C

Parameter	Conditions	Mi	Typical	Мах	Units
Enable Input (MIC29312 only)	·				
Input Logic Voltage	Low (Off) High (On)	2.4		0.8	V V
Enable (EN) Pin Input Current	V <sub>EN</sub> = V <sub>IN</sub>		15	30 <b>75</b>	μA μA
	V <sub>EN</sub> = 0.8V		-	2 <b>4</b>	μΑ μΑ
Regulator Output Current in Shutdown	(Note 8)		10	20	μΑ μΑ

General Note: Devices are ESD sensitive. Handling precautions recommended.

Note 1: The maximum continuous supply voltage is 16V.

Note 2: Full Load current is defined as 3A for the MIC29310/29312. For testing,  $V_{OUT}$  is programmed to 5V.

Note 3: Dropout voltage is defined as the input-to-output differential when the output voltage drops to 99% of its nominal value with V<sub>OUT</sub> + 1V applied to V<sub>IN</sub>.

**Note 4:** For this test,  $V_{IN}$  is the larger of 8V or  $V_{OUT}$  + 3V.

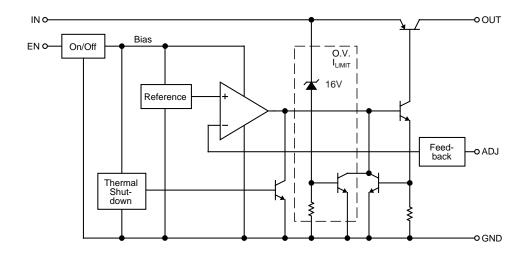
Note 5: Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus the ground pin current.

Note 6: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

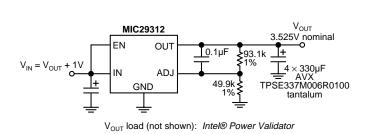
 $\textbf{Note 7:} \quad V_{REF} \leq V_{OUT} \leq (V_{IN}-1~V),~2.4V \leq V_{IN} \leq 16V,~10mA < I_L \leq I_{FL},~T_J \leq T_{J~MAX.}$ 

 $\label{eq:VEN} \mbox{Note 8:} \quad V_{EN} \leq 0.8 \mbox{V and } V_{IN} \leq 8 \mbox{V}, \ V_{OUT} = 0.$ 

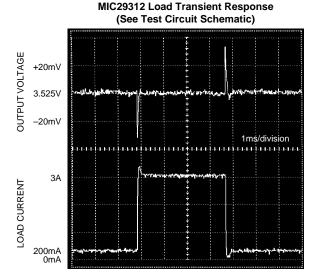
### **Block Diagram**

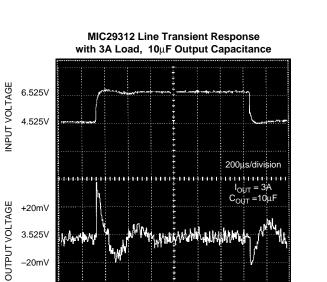


# **Typical Characteristics**

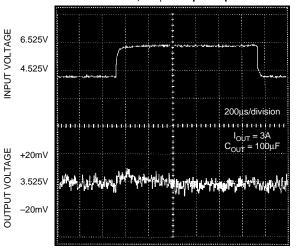


MIC29312 Load Transient Response Test Circuit

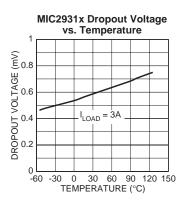




MIC29312 Line Transient Response with 3A Load, 100μF Output Capacitance



MIC2931x Dropout Voltage vs. Output Current



HIC29310-3.3Dropout Characteristics

vs. Input Voltage

 $\mathsf{R}_{\mathsf{LOAD}}$ 

0 INPUT VOLTAGE (V)

vs. Temperature

 $I_{OUT} = 3A$ 

0 30 60 90 120 150

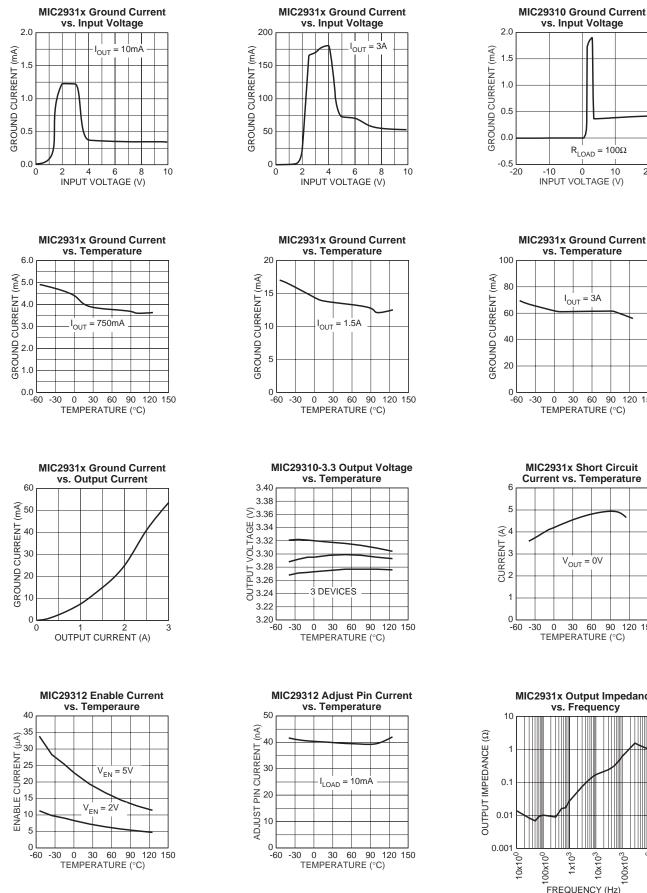
TEMPERATURE (°C)

-10

 $= 100\Omega$ 

10

20



 $V_{OUT} = \overline{0V}$ 

-60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

MIC2931x Output Impedance vs. Frequency 100×10<sup>3</sup> 1x10<sup>6</sup> 1x10<sup>3</sup> 100x10<sup>0</sup> 10x10<sup>3</sup> FREQUENCY (Hz)

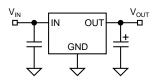
#### **Applications Information**

The MIC29310 and MIC29312 are high performance lowdropout voltage regulators suitable for all moderate to highcurrent voltage regulator applications. Their 600mV of dropout voltage at full load make them especially valuable in battery powered systems and as high efficiency noise filters in "post-regulator" applications. Unlike older NPN-pass transistor designs, where the minimum dropout voltage is limited by the base-emitter voltage drop and collector-emitter saturation voltage, dropout performance of the PNP output of these devices is limited merely by the low V<sub>CE</sub> saturation voltage.

A trade-off for the low dropout voltage is a varying base drive requirement. But Micrel's Super ßeta PNP<sup>™</sup> process reduces this drive requirement to merely 2% to 5% of the load current.

MIC29310/312 regulators are fully protected from damage due to fault conditions. Current limiting is provided. This limiting is linear; output current under overload conditions is constant. Thermal shutdown disables the device when the die temperature exceeds the maximum safe operating temperature. Transient protection allows device (and load) survival even when the input voltage spike above and below nominal. The output structure of these regulators allows voltages in excess of the desired output voltage to be applied without reverse current flow. The MIC29312 version offers a logic level ON/OFF control: when disabled, the devices draw nearly zero current.

An additional feature of this regulator family is a common pinout: a design's current requirement may change up or down yet use the same board layout, as all of Micrel's highcurrent Super ßeta PNP<sup>™</sup> regulators have identical pinouts.



# Figure 3. The MIC29310 regulator requires only two capacitors for operation.

#### **Thermal Design**

Linear regulators are simple to use. The most complicated design parameters to consider are thermal characteristics. Thermal design requires the following application-specific parameters:

- Maximum ambient temperature, T<sub>A</sub>
- Output Current, I<sub>OUT</sub>
- Output Voltage, V<sub>OUT</sub>
- Input Voltage, V<sub>IN</sub>

First, we calculate the power dissipation of the regulator from these numbers and the device parameters from this datasheet.

$$\mathsf{P}_{\mathsf{D}} = \mathsf{I}_{\mathsf{OUT}} \times (1.02\mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}})$$

Where the ground current is approximated by 2% of  $\rm I_{OUT}.$  Then the heat sink thermal resistance is determined with this formula:

$$\theta_{SA} = \frac{T_{JMAX} - T_A}{P_D} - (\theta_{JC} + \theta_{CS})$$

Where  $T_{J\,MAX} \leq 125^\circ C$  and  $\theta_{CS}$  is between 0 and 2°C/W.

The heat sink may be significantly reduced in applications where the minimum input voltage is known and is large compared with the dropout voltage. Use a series input resistor to drop excessive voltage and distribute the heat between this resistor and the regulator. The low dropout properties of Micrel Super ßeta PNP regulators allow very significant reductions in regulator power dissipation and the associated heat sink without compromising performance. When this technique is employed, a capacitor of at least 0.1 $\mu$ F is needed directly between the input and regulator ground.

Please refer to Application Note 9 for further details and examples on thermal design and heat sink specification.

#### **Capacitor Requirements**

For stability and minimum output noise, a capacitor on the regulator output is necessary. The value of this capacitor is dependent upon the output current; lower currents allow smaller capacitors. MIC29310/2 regulators are stable with a minimum capacitor value of  $10\mu$ F at full load.

This capacitor need not be an expensive low ESR type: aluminum electrolytics are adequate. In fact, extremely low ESR capacitors may contribute to instability. Tantalum capacitors are recommended for systems where fast load transient response is important.

Where the regulator is powered from a source with a high AC impedance, a  $0.1\mu$ F capacitor connected between Input and GND is recommended. This capacitor should have good characteristics to above 250kHz.

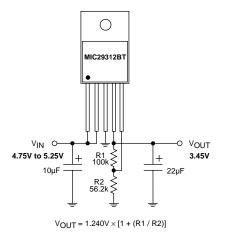
#### Transient Response and 5V to 3.3V Conversion

The MIC29310/2 have excellent response to variations in input voltage and load current. By virtue of their low dropout voltage, these devices do not saturate into dropout as readily as similar NPN-based designs. A 3.3V output Micrel LDO will maintain full speed and performance with an input supply as low as 4.2V, and will still provide some regulation with supplies down to 3.8V, unlike NPN devices that require 5.1V or more for good performance and become nothing more than a resistor under 4.6V of input. Micrel's PNP regulators provide superior performance in "5V to 3.3V" conversion applications than NPN regulators, especially when all tolerances are considered.

#### **Minimum Load Current**

The MIC29310/2 regulators are specified between finite loads. If the output current is too small, leakage currents dominate and the output voltage rises. A 10mA minimum load current is necessary for proper regulation.

#### Adjustable Regulator Design



#### Figure 4. Adjustable Regulator with Resistors

The adjustable regulator version, MIC29312, allows programming the output voltage anywhere between 1.25V and the 15V maximum operating rating of the family. Two resistors are used. Resistors can be quite large, up to  $1M\Omega$ , because of the very high input impedance and low bias current of the sense comparator. The resistor values are calculated by:

$$R1 = R2 \times (\frac{V_{OUT}}{1.240} - 1)$$

Where  $V_0$  is the desired output voltage. Figure 4 shows component definition. Applications with widely varying load currents may scale the resistors to draw the minimum load current required for proper operation (see the table below).

#### **Enable Input**

The MIC29312 version features an enable (EN) input that allows ON/OFF control of the device. Special design allows "zero" current drain when the device is disabled—only micro-amperes of leakage current flows. The EN input has TTL/CMOS compatible thresholds for simple interfacing with logic, or may be directly tied to  $V_{\rm IN}$ . Enabling the regulator requires approximately 20µA of current into the EN pin.

Voltage	Standard ( $\Omega$ )		Min. L	.oad (Ω)
_	R1	R2	R1	R2
2.85	100k	76.8k	162	124
2.9	100k	75.0k	165	124
3.0	100k	69.8k	174	124
3.1	100k	66.5k	187	124
3.15	100k	64.9k	191	124
3.3	100k	60.4k	205	124
3.45	100k	56.2k	221	124
3.6	100k	52.3k	237	124
3.8	100k	48.7k	255	124
4.0	100k	45.3k	274	124
4.1	100k	43.2k	287	124

#### **Resistor Value Table for the MIC29312 Adjustable Regulator**

Note: This regulator has a minimum load requirement. "Standard" values assume the load meets this requirement. "Minimum Load" values are calculated to draw 10mA and allow regulation with an open load (the minimum current drawn from the load may be zero).



# MIC29510/29512

#### 5A Fast-Response LDO Regulator

#### **Preliminary Information**

### **General Description**

The MIC29510 and MIC29512 are high-current, high-accuracy, low-dropout voltage regulators featuring fast transient recovery from input voltage surges and output load current changes. These regulators use a PNP pass element that features Micrel's proprietary Super ßeta PNP<sup>™</sup> process.

The MIC29510/2 is available in two versions: the three pin fixed output MIC29510 and the five pin adjustable output voltage MIC29512. All versions are fully protected against overcurrent faults, reversed input polarity, reversed lead insertion, overtemperature operation, and positive and negative transient voltage spikes.

A TTL compatible enable (EN) control pin supports external on/off control. If on/off control is not required, the device may be continuously enabled by connecting EN to IN.

The MIC29510/2 is available in the standard three and five pin TO-220 package with an operating junction temperature range of  $0^{\circ}$ C to +125°C.

For applications requiring even lower dropout voltage, input voltage greater than 16V, or an error flag, see the MIC29500/29501/29502/29503.

### Features

- Fast transient response
- 5A current capability
- 700mV dropout voltage at full load
- Low ground current
- Accurate 1% guaranteed tolerance
- "Zero" current shutdown mode (MIC29512)
- · Fixed voltage and adjustable versions

### Applications

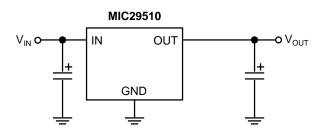
- Pentium<sup>™</sup> and Power PC<sup>™</sup> processor supplies
- High-efficiency "green" computer systems
- High-efficiency linear power supplies
- High-efficiency switching supply post regulator
- Battery-powered equipment

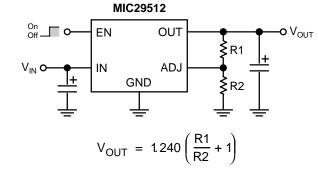
### **Ordering Information**

Part Number	Temp. Range*	Voltage	Current	Package
MIC29510-3.3BT	0°C to +125°C	3.3V	5.0A	TO-220-3
MIC29510-5.0BT	0°C to +125°C	5.0V	5.0A	TO-220-3
MIC29512BT	0°C to +125°C	Adj.	5.0A	TO-220-5

Junction Temperature

## **Typical Application**





**Fixed Regulator Configuration** 

#### Adjustable Regulator Configuration

### **Pin Configuration**



On all devices, the Tab is grounded.

### Pin Description 3-Pin TO-220 (MIC29510)

Pin Number	Pin Name	Pin Function	
1	IN	Unregulated Input: +16V maximum supply.	
2	GND	Ground: Internally connected to tab (ground).	
3	OUT	Regulated Output	

#### 5-Pin TO-220 (MIC29512)

Pin Number	Pin Name	Pin Function
1	EN	Enable (Input): Logic-level ON/OFF control.
2	IN	Unregulated Input: +16V maximum supply.
3	GND	Ground: Internally connected to tab (ground).
4	OUT	Regulated Output
5	ADJ	Output Voltage Adjust: 1.240V feedback from external resistive divider.

### **Absolute Maximum Ratings**

Input Supply Voltage (Note 1)	–20V to +20V
Power Dissipation	Internally Limited
Storage Temperature Range	–65°C to +150°C
Lead Temperature (Soldering, 5 sec.)	260°C

### **Operating Ratings**

Operating Junction Temperature	0°C to +125°C
θ <sub>JC</sub> (TO-220)	2°C/W
θ <sub>JA</sub> (TO-220)	55°C/W

### **Electrical Characteristics**

All measurements at  $T_J = 25^{\circ}C$  unless otherwise noted. **Bold** values are guaranteed across the operating temperature range.

Parameter	Condition	Min	Тур	Max	Units
Output Voltage	$10\text{mA} \le \text{I}_{\text{O}} \le \text{I}_{\text{FL}}, (\text{V}_{\text{OUT}} + 1\text{V}) \le \text{V}_{\text{IN}} \le 8\text{V} \text{ (Note 2)}$			2	%
Line Regulation	$I_0 = 10mA$ , $(V_{OUT} + 1V) \le V_{IN} \le 8V$		0.06	0.5	%
Load Regulation	$V_{IN} = V_{OUT} + 1V$ , $10mA \le I_{OUT} \le I_{FULL \ LOAD}$ (Notes 2, 6)		0.2	1	%
$\Delta V_O / \Delta T$	Output Voltage Temperature Coefficient (Note 6)		20	100	ppm/°C
Dropout Voltage	$ \Delta V_{OUT} = -1\%, \text{ (Note 3)} $ MIC29510/29512 I <sub>O</sub> = 100mA I <sub>O</sub> = 750mA I <sub>O</sub> = 1.5A I <sub>O</sub> = 3A I <sub>O</sub> = 5A		80 200 320 500 700	200 1000	mV mV mV mV mV
Ground Current	MIC29510/29512 $I_O = 750$ mA, $V_{IN} = V_{OUT} + 1V$ $I_O = 1.5A$ $I_O = 3A$ $I_O = 5A$		3 10 36 100	20 150	mA mA mA mA
I <sub>GNDDO</sub> Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than specified $V_{OUT}$ . $I_{OUT} = 10$ mA		2	3	mA
Current Limit	MIC29510/29512 V <sub>OUT</sub> = 0V (Note 4)	5.0	6.5		А
e <sub>n</sub> , Output Noise Voltage (10Hz to 100kHz) I <sub>L</sub> = 100mA	$C_{L} = 47 \mu F$		260		$\mu V_{RMS}$

#### Reference (MIC29512 only)

Reference Voltage	$10\text{mA} \le \text{I}_{O} \le \text{I}_{FL}, \text{ V}_{OUT} + 1\text{V} \le \text{V}_{IN} \le 8\text{V} \text{ (Note 2)}$	1.215		1.265	V <sub>MAX</sub>
Adjust Pin Bias Current			40	80 <b>120</b>	nA nA
Reference Voltage Temperature Coefficient	(Note 7)		20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C

MIC29510/29512

Parameter	Conditions	Min	Typical	Max	Units
Enable Input (MIC29512 only)	·				
Input Logic Voltage	Low (Off) High (On)	2.4		0.8	V V
Enable (EN) Pin Input Current	V <sub>EN</sub> = V <sub>IN</sub>		15	30 <b>75</b>	μΑ μΑ
	V <sub>EN</sub> = 0.8V		-	2 <b>4</b>	μΑ μΑ
Regulator Output Current in Shutdown	(Note 8)		10	20	μΑ μΑ

General Note: Devices are ESD sensitive. Handling precautions recommended.

Note 1: The maximum continuous supply voltage is 16V.

Note 2: Full Load current is defined as 5A for the MIC29510/29512. For testing,  $V_{OUT}$  is programmed to 5V.

Note 3: Dropout voltage is defined as the input-to-output differential when the output voltage drops to 99% of its nominal value with V<sub>OUT</sub> + 1V applied to V<sub>IN</sub>.

**Note 4:** For this test,  $V_{IN}$  is the larger of 8V or  $V_{OUT}$  + 3V.

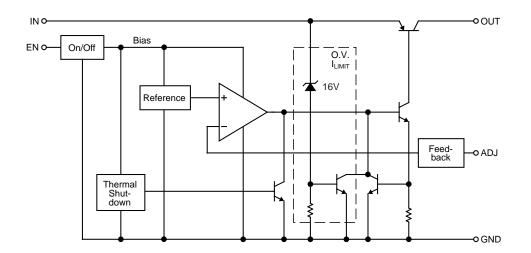
Note 5: Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus the ground pin current.

Note 6: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

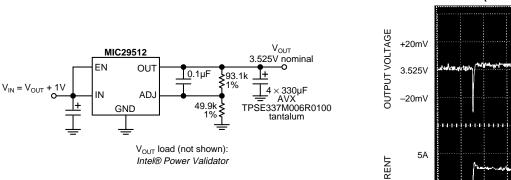
 $\label{eq:Note 7: V_{REF} le V_{OUT} le (V_{IN}-1~V), \ 2.4V le V_{IN} le 16V, \ 10mA < I_L le I_{FL}, \ T_J le T_{J~MAX.}$ 

Note 8:  $V_{EN} \leq 0.8V$  and  $V_{IN} \leq 8V$ ,  $V_{OUT} = 0$ .

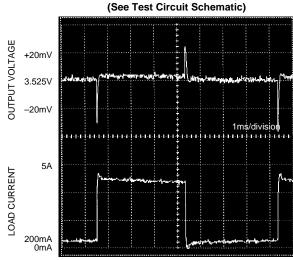
#### **Block Diagram**



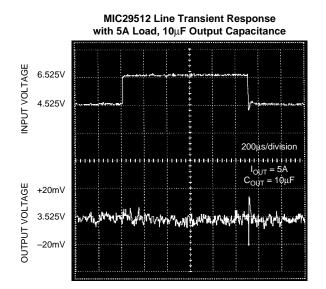
## **Typical Characteristics**



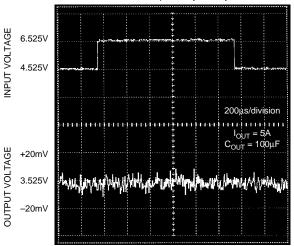
MIC29512 Load Transient Response Test Circuit



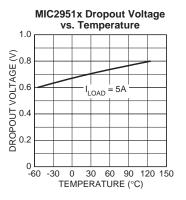
**MIC29512 Load Transient Response** 

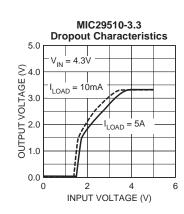


MIC29512 Line Transient Response with 5A Load, 100μF Output Capacitance

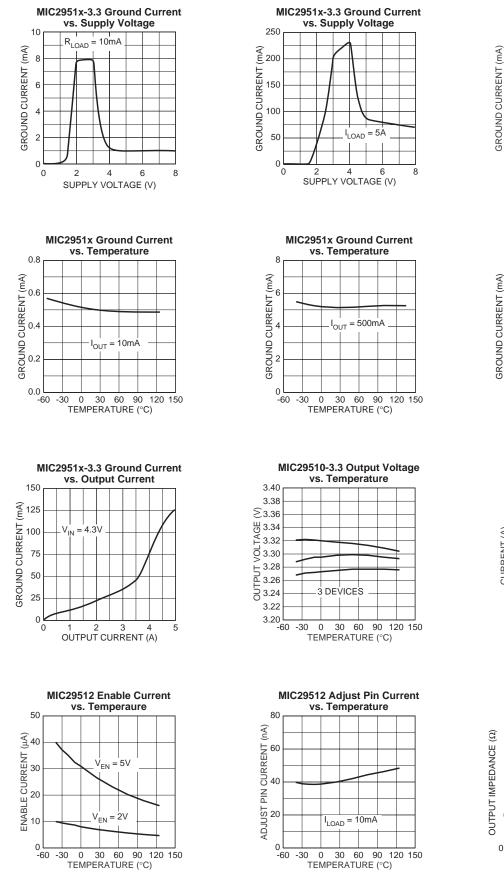


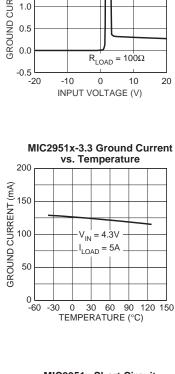
MIC2951x Dropout Voltage vs. Output Current











MIC2951x Ground

Current vs. Input Voltage

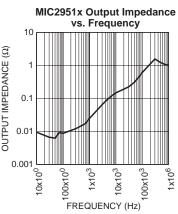
V<sub>OUT</sub> = 3.3V

2.5

2.0

1.5

MIC2951x Short Circuit Current vs. Temperature 10 g 8 7 CURRENT (A)  $V_{OUT} = 0V$ 6 5 4 3 2 0∟ -60 30 60 90 120 150 -30 0 TEMPERATURE (°C)



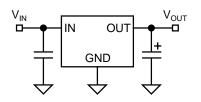
#### **Applications Information**

The MIC29510 and MIC29512 are high performance lowdropout voltage regulators suitable for all moderate to highcurrent voltage regulator applications. Their 600mV of dropout voltage at full load make them especially valuable in battery powered systems and as high efficiency noise filters in "post-regulator" applications. Unlike older NPN-pass transistor designs, where the minimum dropout voltage is limited by the base-emitter voltage drop and collector-emitter saturation voltage, dropout performance of the PNP output of these devices is limited merely by the low V<sub>CE</sub> saturation voltage.

A trade-off for the low dropout voltage is a varying base drive requirement. But Micrel's Super ßeta PNP<sup>™</sup> process reduces this drive requirement to merely 2 to 5% of the load current.

MIC29510/512 regulators are fully protected from damage due to fault conditions. Current limiting is provided. This limiting is linear; output current under overload conditions is constant. Thermal shutdown disables the device when the die temperature exceeds the maximum safe operating temperature. Transient protection allows device (and load) survival even when the input voltage spike above and below nominal. The output structure of these regulators allows voltages in excess of the desired output voltage to be applied without reverse current flow. The MIC29512 version offers a logic level ON/OFF control: when disabled, the devices draw nearly zero current.

An additional feature of this regulator family is a common pinout: a design's current requirement may change up or down yet use the same board layout, as all of Micrel's highcurrent Super ßeta PNP<sup>™</sup> regulators have identical pinouts.



# Figure 3. The MIC29510 LDO regulator requires only two capacitors for operation.

#### Thermal Design

Linear regulators are simple to use. The most complicated design parameters to consider are thermal characteristics. Thermal design requires the following application-specific parameters:

- Maximum ambient temperature, T<sub>A</sub>
- Output Current, IOUT
- Output Voltage, V<sub>OUT</sub>
- Input Voltage, V<sub>IN</sub>

First, we calculate the power dissipation of the regulator from these numbers and the device parameters from this datasheet.

$$\mathsf{P}_{\mathsf{D}} = \mathsf{I}_{\mathsf{OUT}} \times (1.02\mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}})$$

Where the ground current is approximated by 2% of  $\rm I_{OUT}.$  Then the heat sink thermal resistance is determined with this formula:

$$\theta_{SA} = \frac{T_{JMAX} - T_A}{P_D} - (\theta_{JC} + \theta_{CS})$$

Where  $T_{J\,MAX} \leq 125^{\circ}C$  and  $\theta_{CS}$  is between 0 and 2°C/W.

The heat sink may be significantly reduced in applications where the minimum input voltage is known and is large compared with the dropout voltage. Use a series input resistor to drop excessive voltage and distribute the heat between this resistor and the regulator. The low dropout properties of Micrel Super ßeta PNP regulators allow very significant reductions in regulator power dissipation and the associated heat sink without compromising performance. When this technique is employed, a capacitor of at least 0.1 $\mu$ F is needed directly between the input and regulator ground.

Please refer to Application Note 9 for further details and examples on thermal design and heat sink specification.

#### **Capacitor Requirements**

For stability and minimum output noise, a capacitor on the regulator output is necessary. The value of this capacitor is dependent upon the output current; lower currents allow smaller capacitors. MIC29510/2 regulators are stable with a minimum capacitor value of  $47\mu$ F at full load.

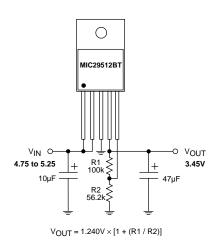
This capacitor need not be an expensive low ESR type: aluminum electrolytics are adequate. In fact, extremely low ESR capacitors may contribute to instability. Tantalum capacitors are recommended for systems where fast load transient response is important.

Where the regulator is powered from a source with a high AC impedance, a  $0.1\mu$ F capacitor connected between Input and GND is recommended. This capacitor should have good characteristics to above 250kHz.

#### Transient Response and 5V to 3.3V Conversion

The MIC29510/2 have excellent response to variations in input voltage and load current. By virtue of their low dropout voltage, these devices do not saturate into dropout as readily as similar NPN-based designs. A 3.3V output Micrel LDO will maintain full speed and performance with an input supply as low as 4.2V, and will still provide some regulation with supplies down to 3.8V, unlike NPN devices that require 5.1V or more for good performance and become nothing more than a resistor under 4.6V of input. Micrel's PNP regulators provide superior performance in "5V to 3.3V" conversion applications than NPN regulators, especially when all tolerances are considered.

#### Adjustable Regulator Design



#### Figure 4. Adjustable Regulator with Resistors

The adjustable regulator version, MIC29512, allows programming the output voltage anywhere between 1.25V and the 16V maximum operating rating of the family. Two resistors are used. Resistors can be quite large, up to  $100k\Omega$ , because of the very high input impedance and low bias current of the sense comparator. The resistor values are calculated by:

R1 = R2 × (
$$\frac{V_{OUT}}{1.240}$$
 - 1)

Where  $\mathrm{V}_{\mathrm{O}}$  is the desired output voltage. Figure 4 shows component definition.

#### Enable Input

The MIC29512 versions features an enable (EN) input that allows ON/OFF control of the device. Special design allows "zero" current drain when the device is disabled—only micro-amperes of leakage current flows. The EN input has TTL/ CMOS compatible thresholds for simple interfacing with logic, or may be directly tied to  $V_{\rm IN}$ . Enabling the regulator requires approximately 20µA of current into the EN pin.

### Resistor Value Table for the MIC29512 Adjustable Regulator

Voltage	Standard ( $\Omega$ )		
	R1	R2	
2.85	100k	76.8k	
2.9	100k	75.0k	
3.0	100k	69.8k	
3.1	100k	66.5k	
3.15	100k	64.9k	
3.3	100k	60.4k	
3.45	100k	56.2k	
3.6	100k	52.3k	
3.8	100k	48.7k	
4.0	100k	45.3k	
4.1	100k	43.2k	



# MIC29710/29712

#### 7.5A Fast-Response LDO Regulator

### **General Description**

The MIC29710 and MIC29712 are high-current, high-accuracy, low-dropout voltage regulators featuring fast transient recovery from input voltage surges and output load current changes. These regulators use a PNP pass element that features Micrel's proprietary Super ßeta PNP<sup>™</sup> process.

The MIC29710/2 is available in two versions: the three pin fixed output MIC29710 and the five pin adjustable output voltage MIC29712. All versions are fully protected against overcurrent faults, reversed lead insertion, overtemperature operation, and positive and negative transient voltage spikes.

A TTL compatible enable (EN) control pin supports external on/off control. If on/off control is not required, the device may be continuously enabled by connecting EN to IN.

The MIC29710/2 is available in the standard three and five pin TO-220 package with an operating junction temperature range of  $0^{\circ}$ C to +125°C.

For applications requiring even lower dropout voltage or input voltage greater than 16V, see the MIC29750/29752.

#### **Features**

- · Fast transient response
- 7.5A current capability
- 700mV dropout voltage at full load
- Low ground current
- Accurate 2% guaranteed tolerance
- "Zero" current shutdown mode (MIC29712)
- No minimum load current
- Fixed voltage and adjustable versions

### Applications

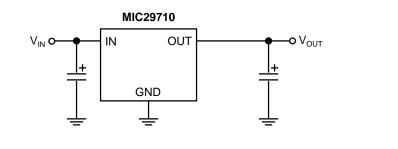
- Pentium<sup>™</sup>, Pentium Plus<sup>™</sup>, and Power PC<sup>™</sup> processor supplies
- High-efficiency "green" computer systems
- High-efficiency linear power supplies
- · High-efficiency switching supply post regulator
- Battery-powered equipment

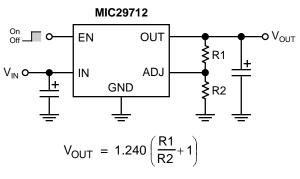
#### Ordering Information

		Voltage	Current	Package
MIC29710-3.3BT	0°C to +125°C	3.3V	7.5A	TO-220-3
MIC29710-5.0BT	0°C to +125°C	5.0V	7.5A	TO-220-3
MIC29712BT	0°C to +125°C	Adj.	7.5A	TO-220-5

\* Junction Temperature

### **Typical Application**

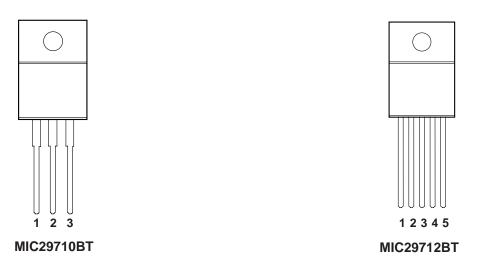




Fixed Regulator Configuration

#### Adjustable Regulator Configuration

### **Pin Configuration**



#### On all devices, the Tab is grounded.

### Pin Description 3-Pin TO-220 (MIC29710)

Pin Number	Pin Name	Pin Function
1	IN	Unregulated Input: +16V maximum supply.
2	GND	Ground: Internally connected to tab (ground).
3	OUT	Regulated Output

#### 5-Pin TO-220 (MIC29712)

Pin Number	Pin Name	Pin Function
1	EN	Enable (Input): Logic-level ON/OFF control.
2	IN	Unregulated Input: +16V maximum supply.
3	GND	Ground: Internally connected to tab (ground).
4	OUT	Regulated Output
5	ADJ	Output Voltage Adjust: 1.240V feedback from external resistive divider.

### **Absolute Maximum Ratings**

Input Supply Voltage, Note 1	-0.7 V to +20V
Power Dissipation	Internally Limited
Storage Temperature Range	–65°C to +150°C
Lead Temperature (Soldering, 5 sec.)	260°C

### **Operating Ratings**

Operating Junction Temperature	0°C to +125°C
θ <sub>JC</sub> (TO-220)	2°C/W
θ <sub>JA</sub> (TO-220)	55°C/W

### **Electrical Characteristics**

All measurements at  $T_J = 25^{\circ}$ C unless otherwise noted. **Bold** values are guaranteed across the operating temperature range.

Parameter	Condition	Min	Тур	Max	Units
Output Voltage	$10\text{mA} \le \text{I}_{\text{O}} \le 7.5\text{A}, (\text{V}_{\text{OUT}} + 1\text{V}) \le \text{V}_{\text{IN}} \le 8\text{V}, \text{Note 2}$	-2		2	%
Line Regulation	$I_0 = 10 \text{mA}, (V_{OUT} + 1 \text{V}) \le V_{IN} \le 8 \text{V}$		0.06	0.5	%
Load Regulation	$V_{IN} = V_{OUT} + 1V$ , 10mA $\le I_{OUT} \le$ 7.5A, <b>Notes 2, 6</b>		0.2	1	%
Output Voltage Temperature Coefficient	$\Delta V_{O} / \Delta T$ , Note 6		20	100	ppm/°C
Dropout Voltage	$ \Delta V_{OUT} = -1\%, \text{ (Note 3)} \\ \text{MIC29710/29712} \qquad I_{O} = 100\text{mA} \\ I_{O} = 750\text{mA} \\ I_{O} = 1.5\text{A} \\ I_{O} = 3\text{A} \\ I_{O} = 5\text{A} \\ I_{O} = 7.5\text{A} \\ MORE IN EVALUATE IN EVALUATION IN THE INFORMATION INTERVALUE INTERVALUE INFORMATION IN THE INFORMATION IN THE INFORMATION INTERVALUE I$		80 180 220 300 450 700	200 1000	mV mV mV mV mV mV
Ground Current	MIC29710/29712 $I_{O} = 750$ mA, $V_{IN} = V_{OUT} + 1V$ $I_{O} = 1.5A$ $I_{O} = 3A$ $I_{O} = 5A$ $I_{O} = 7.5A$		6 20 36 100 250	20 375	mA mA mA mA mA
I <sub>GNDDO</sub> Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than specified $V_{OUT}$ . $I_{OUT} = 10$ mA		1	2	mA
Current Limit	MIC29710/29712 V <sub>OUT</sub> = 0V, <b>Note 4</b>		11	15	A
e <sub>n</sub> , Output Noise Voltage (10Hz to 100kHz) V <sub>OUT</sub> = 5.0V	$C_L = 47\mu F$ $I_o = 100 \text{mA}$		260		μV <sub>RMS</sub>
Reference (MIC29712 only)					
Reference Voltage	$10\text{mA} \le \text{I}_{\text{O}} \le 7.5\text{A}, \text{ V}_{\text{OUT}} + 1\text{V} \le \text{V}_{\text{IN}} \le 8\text{V}, \text{ Note 2}$	1.215	1.240	1.265	V <sub>MAX</sub>
Adjust Pin Bias Current			40	80 <b>120</b>	nA nA
Reference Voltage Temperature Coefficient	Note 7		20		ppm/°C
Adjust Pin Bias Current Temperature Coefficient			0.1		nA/°C

MIC29710/29712

Parameter	Conditions	Min	Typical	Max	Units	
Enable Input (MIC29712 only)						
Input Logic Voltage	Low (Off) High (On)	2.4		0.8	V V	
Enable (EN) Pin Input Current	$V_{EN} = V_{IN}$		15	30 <b>75</b>	μΑ μΑ	
	V <sub>EN</sub> = 0.8V		-	2 <b>4</b>	μΑ μΑ	
Regulator Output Current in Shutdown	(Note 8)		10	20	μΑ μΑ	

General Note: Devices are ESD sensitive. Handling precautions are recommended.

Note 1: The maximum continuous supply voltage is 16V.

Note 2: For testing, MIC29712  $V_{\mbox{OUT}}$  is programmed to 5V.

Note 3: Dropout voltage is defined as the input-to-output differential when the output voltage drops to 99% of its nominal value with V<sub>OUT</sub> + 1V applied to V<sub>IN</sub>.

**Note 4:** For this test,  $V_{IN}$  is the larger of 8V or  $V_{OUT}$  + 3V.

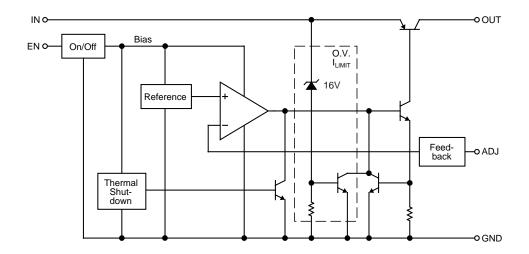
Note 5: Ground pin current is the regulator quiescent current. The total current drawn from the source is the sum of the load current plus the ground pin current.

Note 6: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

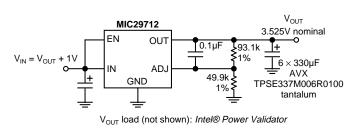
 $\label{eq:Note 7: V_REF} \textbf{Note 7:} \quad V_{REF} \leq V_{OUT} \leq (V_{IN}-1~V), \ 2.4V \leq V_{IN} \leq 8V, \ 10mA < I_L \leq 7.5A, \ T_J \leq T_{J~MAX.}$ 

Note 8:  $V_{EN} \le 0.8V$  and  $V_{IN} \le 16V$ ,  $V_{OUT} = 0$ .

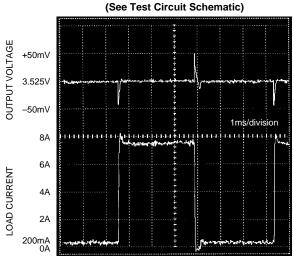
#### **Block Diagram**



## **Typical Characteristics**

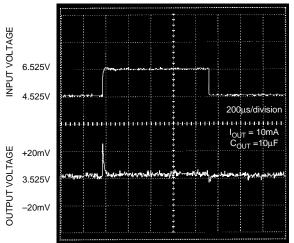


MIC29712 Load Transient Response Test Circuit

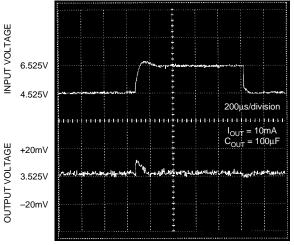


**MIC29712 Load Transient Response** 

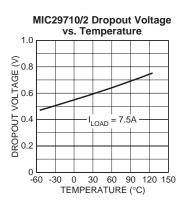
MIC29712 Line Transient Response with 10mA Load, 10μF Output Capacitance

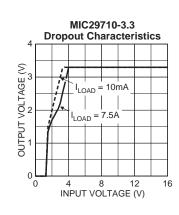


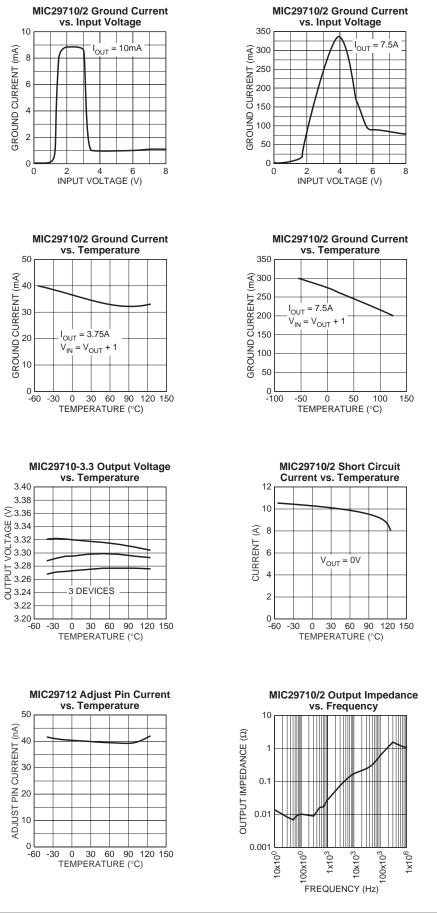
MIC29712 Line Transient Response with 10mA Load, 100 $\mu$ F Output Capacitance



MIC29710/2 Dropout Voltage vs. Output Current







0 0 6 8 OUTPUT CURRENT (A) MIC29712 Enable Current vs. Temperaure 40 35 (AT) 30  $V_{EN} = 5V$ 

MIC29710/2 Ground Current

vs. Temperature

I<sub>OUT</sub> = 750mA

 $V_{IN} = V_{OUT} + 1$ 

TEMPERATURE (°C)

MIC29710/2 Ground Current

vs. Output Current

VOUT IN

90 120 150

12

10

8

6

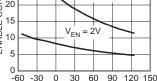
4

2

0 -60 -30 0 30 60

250

**GROUND CURRENT (mA)** 



-60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

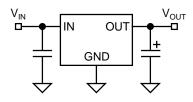
#### **Applications Information**

The MIC29710 and MIC29712 are high performance lowdropout voltage regulators suitable for all moderate to highcurrent voltage regulator applications. Their 700mV of dropout voltage at full load make them especially valuable in battery powered systems and as high efficiency noise filters in "post-regulator" applications. Unlike older NPN-pass transistor designs, where the minimum dropout voltage is limited by the base-emitter voltage drop and collector-emitter saturation voltage, dropout performance of the PNP output of these devices is limited merely by the low V<sub>CE</sub> saturation voltage. Output regulation is excellent across the input voltage, output current, and temperature ranges. The MIC29710/ 712 does not have a minimum load current limitation.

A trade-off for the low dropout voltage is a varying base drive requirement. But Micrel's Super ßeta PNP<sup>™</sup> process reduces this drive requirement to merely 2 to 5% of the load current.

MIC29710/712 regulators are fully protected from damage due to fault conditions. Current limiting is provided. The output current under overload conditions is limited to a constant value. Thermal shutdown disables the device when the die temperature exceeds the maximum safe operating temperature. Transient protection allows device (and load) survival even when the input voltage spike above and below nominal. The MIC29712 version offers a logic level ON/OFF control: when disabled, the devices draw nearly zero current.

An additional feature of this regulator family is a common pinout: a design's current requirement may change up or down yet use the same board layout, as all of Micrel's highcurrent Super ßeta PNP<sup>™</sup> regulators have identical pinouts.



# Figure 3. The MIC29710 requires only two capacitors for operation.

#### **Thermal Design**

Linear regulators are simple to use. The most complicated design parameters to consider are thermal characteristics. Thermal design requires the following application-specific parameters:

- Maximum ambient temperature, T<sub>A</sub>
- Output Current, I<sub>OUT</sub>
- Output Voltage, V<sub>OUT</sub>
- Input Voltage, VIN

First, we calculate the power dissipation of the regulator from these numbers and the device parameters from this datasheet.

$$\mathsf{P}_{\mathsf{D}} = \mathsf{I}_{\mathsf{OUT}} \times (1.03 \mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}})$$

Where the ground current is approximated by 3% of  $\rm I_{OUT}.$  Then the heat sink thermal resistance is determined with this formula:

$$\theta_{SA} = \frac{T_{JMAX} - T_A}{P_D} - (\theta_{JC} + \theta_{CS})$$

Where T  $_{J\mbox{ MAX}} \leq 125^\circ C$  and  $\theta_{CS}$  is between 0 and 2°C/W.

The heat sink may be significantly reduced in applications where the minimum input voltage is known and is large compared with the dropout voltage. Use a series input resistor to drop excessive voltage and distribute the heat between this resistor and the regulator. The low dropout properties of Micrel Super ßeta PNP regulators allow very significant reductions in regulator power dissipation and the associated heat sink without compromising performance. When this technique is employed, a capacitor of at least 0.1 $\mu$ F is needed directly between the input and regulator ground.

Please refer to Application Note 9 for further details and examples on thermal design and heat sink specification.

#### **Capacitor Requirements**

For stability and minimum output noise, a capacitor on the regulator output is necessary. The value of this capacitor is dependent upon the output current; lower currents allow smaller capacitors. MIC29710/2 regulators are stable with a minimum capacitor value of  $47\mu$ F at full load.

This capacitor need not be an expensive low ESR type: aluminum electrolytics are adequate. In fact, extremely low ESR capacitors may contribute to instability. Tantalum capacitors are recommended for systems where fast load transient response is important.

Where the regulator is powered from a source with a high AC impedance, a  $0.1\mu$ F capacitor connected between Input and GND is recommended. This capacitor should have good characteristics to above 250kHz.

#### Transient Response and 5V to 3.3V Conversion

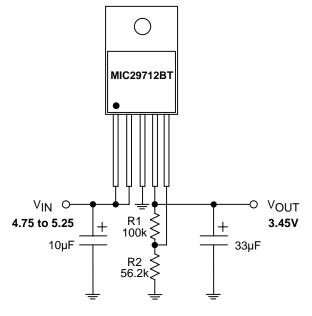
The MIC29710/2 have excellent response to variations in input voltage and load current. By virtue of their low dropout voltage, these devices do not saturate into dropout as readily as similar NPN-based designs. A 3.3V output Micrel LDO will maintain full speed and performance with an input supply as low as 4.2V, and will still provide some regulation with supplies down to 3.8V, unlike NPN devices that require 5.1V or more for good performance and become nothing more than a resistor under 4.6V of input. Micrel's PNP regulators provide superior performance in "5V to 3.3V" conversion applications, especially when all tolerances are considered.

#### Adjustable Regulator Design

The adjustable regulator version, MIC29712, allows programming the output voltage anywhere between 1.25V and the 16V maximum operating rating of the family. Two resistors are used. Resistors can be quite large, up to  $100k\Omega$ , because of the very high input impedance and low bias current of the sense comparator. The resistor values are calculated by:

$$R1 = R2 \times (\frac{V_{OUT}}{1.240} - 1)$$

Where  $\mathrm{V}_\mathrm{O}$  is the desired output voltage. Figure 4 shows component definition.



 $V_{OUT} = 1.240V \times [1 + (R1 / R2)]$ 

Figure 4. Adjustable Regulator with Resistors

#### Enable Input

The MIC29712 versions features an enable (EN) input that allows ON/OFF control of the device. Special design allows "zero" current drain when the device is disabled—only micro-amperes of leakage current flows. The EN input has TTL/CMOS compatible thresholds for simple interfacing with logic, or may be directly tied to  $V_{\rm IN}$ . Enabling the regulator requires approximately 20µA of current into the EN pin.

Voltage	Standard (Ω)	
	R1	R2
2.85	100k	76.8k
2.9	100k	75.0k
3.0	100k	69.8k
3.1	100k	66.5k
3.15	100k	64.9k
3.3	100k	60.4k
3.45	100k	56.2k
3.525	93.1k	51.1k
3.6	100k	52.3k
3.8	100k	48.7k
4.0	100k	45.3k
4.1	100k	43.2k

Figure 5. MIC29712 Resistor Table



# MIC39150/39151

1.5A Low-Voltage Low-Dropout Regulator

#### **Preliminary Information**

### **General Description**

The MIC39150 and MIC39151 are high-current, high-accuracy low-dropout voltage regulators designed for 2.5V applications. Dropout voltage is guaranteed at 500mV maximum over the operating temperature range, allowing a 2.5V regulated output with as little as 3.0V input. Featuring Micrel's Super ßeta PNP pass element for low ground current, the MIC39150/1 also exhibits fast transient recovery from input voltage surges and output load changes.

The MIC39150/1 is fully protected against overcurrent faults, reversed input polarity, reversed lead insertion, overtemperature operation, and positive and negative voltage spikes.

The MIC39150/1 is available in standard TO-220 and surface-mount TO-263 packages with a junction operating temperature range of  $0^{\circ}$ C to +125°C.

For applications requiring input voltage greater than 16V or automotive load dump protection, see the MIC29150/1/2/3 family.

#### Features

- 2.5V Output
- 1.5A minimum output current
- 500mV dropout voltage
- 1% guaranteed tolerance
- Low ground current
- · Overcurrent and overtemperature protection
- Reversed-battery protection
- Fast transient response

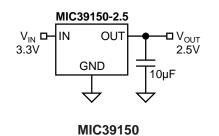
#### **Applications**

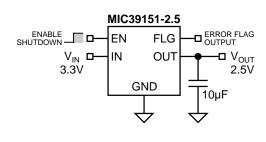
- Multimedia and PC processor supplies
- High-efficiency "green" computer systems
- High-efficiency linear power supplies
- · High-efficiency switching supply post regulator

#### **Ordering Information**

Part Number	Voltage	Junction Temp. Range	Package
MIC39150-2.5BT	2.5V	0°C to +125°C	3-lead TO-220
MIC39150-2.5BU	2.5V	0°C to +125°C	3-lead TO-263
MIC39151-2.5BT	2.5V	0°C to +125°C	5-lead TO-220
MIC39151-2.5BU	2.5V	0°C to +125°C	5-lead TO-263

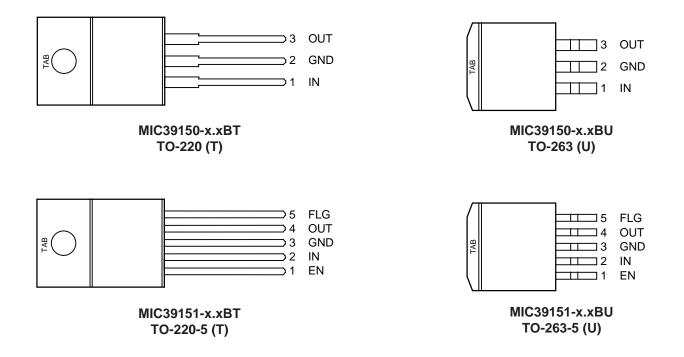
### **Typical Application**





MIC39151

### **Pin Configuration**



### **Pin Description**

Pin Number MIC39150	Pin Number MIC39151	Pin Name	Pin Function
	1	EN	Enable (Input): Active-high, logic-level enable/shutdown control.
1	2	IN	Unregulated Input: +16V maximum supply.
2, тав	3, тав	GND	Ground: Ground pin and TAB are internally connected.
3	4	OUT	Regulator Output
	5	FLG	Fault Flag (Ouput): Open-collector (active-low) output.

Supply Voltage (V <sub>IN</sub> )2	0V to +20V
Enable Voltage (V <sub>EN</sub> )	+20V
Storage Temperature (T <sub>S</sub> )65°C	to +150°C
Lead Temperature (soldering, 5 sec.)	260°C
ESD, Note 3	

# **Operating Ratings (Note 2)**

Supply Voltage (V <sub>IN</sub> )	+16V
Enable Voltage (V <sub>EN</sub> )	+16V
Maximum Power Dissipation (P <sub>D(max)</sub> )	Note 4
Junction Temperature (T <sub>J</sub> )	
Package Thermal Resistance	
TO-263 (θ <sub>JC</sub> )	2°C/W
TO-220 (θ <sub>JC</sub> )	2°C/W

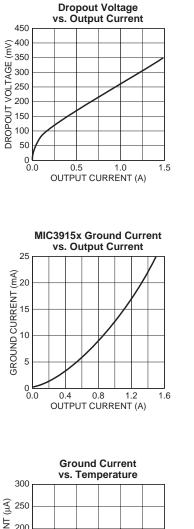
## **Electrical Characteristics**

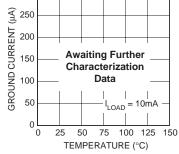
 $T_J = 25^{\circ}C$ , **bold** values indicate  $0^{\circ}C \le T_J \le +125^{\circ}C$ ; unless noted

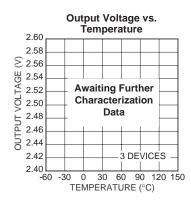
Symbol	Parameter	Condition	Min	Тур	Max	Units
V <sub>OUT</sub>	Output Voltage	$10\text{mA} \le \text{I}_{\text{OUT}} \le 1.5\text{A}, \text{V}_{\text{OUT}} + 1\text{V} \le \text{V}_{\text{IN}} \le 8\text{V}$	-1 <b>-2</b>		1 2	% %
	Line Regulation	$I_{OUT} = 10mA, V_{OUT} + 1V \le V_{IN} \le 16V$		0.06	0.5	%
	Load Regulation	$V_{IN} = V_{OUT} + 1V$ , $10mA \le I_{OUT} \le 1.5A$ ,		0.2	1	%
$\Delta V_{OUT} / \Delta T$	Output Voltage Temp. Coefficient, Note 5			20	100	ppm/°C
V <sub>DO</sub>	Dropout Voltage, Note 6	$I_{OUT} = 100 \text{mA}, \Delta V_{OUT} = -1\%$		80	200	mV
		$I_{OUT} = 750 \text{mA}, \Delta V_{OUT} = -1\%$		220		mV
		$I_{OUT} = 1.5A, \Delta V_{OUT} = -1\%$		350	500	mV
I <sub>GND</sub>	Ground Current, Note 7	$I_{OUT} = 750 \text{mA}, V_{IN} = V_{OUT} + 1 \text{V}$		5	20	mA
		$I_{OUT} = 1.5A, V_{IN} = V_{OUT} + 1V$		15		mA
I <sub>GND(do)</sub>	Dropout Ground Pin Current	$V_{IN} \le V_{OUT(nominal)} - 0.5V, I_{OUT} = 10mA$		2	3	mA
I <sub>OUT(lim)</sub>	Current Limit	$V_{OUT} = 0V, V_{IN} = V_{OUT} + 1V$		2.5		A
I <sub>OUT(min)</sub>	Minimum Load Current			7	10	mA
Enable Inpu	it (MIC39151)	•				
e <sub>n</sub>	Output Noise Voltage	$C_{OUT} = 10\mu$ F, $I_{OUT} = 100$ mA, 10Hz to 100kHz		400		μV(rms)
		$C_{OUT} = 33\mu$ F, $I_{OUT} = 100$ mA, 10Hz to 100kHz		260		μV(rms)
V <sub>EN</sub>	Enable Input Voltage	logic low (off)			0.8	V
		logic high (on)	2.4			V
I <sub>IN</sub>	Enable Input Current	$V_{EN} = V_{IN}$		15	30 <b>75</b>	μΑ μΑ
		V <sub>EN</sub> = 0.8V			2 4	μΑ μΑ
I <sub>OUT(shdn)</sub>	Shutdown Output Current	Note 8		10	20	μA
,	(MIC39151)			1	1	
I <sub>FLG(leak)</sub>	Output Leakage Current	V <sub>OH</sub> = 16V		0.01	1 2	μΑ μΑ
V <sub>FLG(do)</sub>	Output Low Voltage	V <sub>IN</sub> = 2.250V, I <sub>OL</sub> , = 250µA, <b>Note 9</b>		125	150 <b>200</b>	mV mV

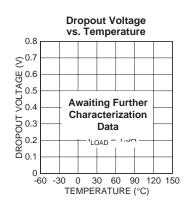
- Note 1. Exceeding the absolute maximum ratings may damage the device.
- Note 2. The device is not guaranteed to function outside its operating rating.
- Note 3. Devices are ESD sensitive. Handling precautions recommended.
- Note 4.  $P_{D(max)} = (T_{J(max)} T_A) \div \theta_{JA}$ , where  $\theta_{JA}$  depends upon the printed circuit layout. See "Applications Information."
- Note 5. Output voltage temperature coefficient is  $\Delta V_{OUT(worst case)} \div (T_{J(max)} T_{J(min)})$  where  $T_{J(max)}$  is +125°C and  $T_{J(min)}$  is 0°C.
- Note 6.  $V_{DO} = V_{IN} V_{OUT}$  when  $V_{OUT}$  decreases to 99% of its nominal output voltage with  $V_{IN} = V_{OUT} + 1V$ .
- **Note 7.**  $I_{GND}$  is the quiescent current.  $I_{IN} = I_{GND} + I_{OUT}$ .
- $\label{eq:VEN} \textbf{Note 8.} \quad V_{EN} \leq 0.8 \text{V}, \, V_{IN} \leq 8 \text{V}, \, \text{and} \, \, V_{OUT} = 0 \text{V}.$
- Note 9. For a 2.5V device,  $V_{IN} = 2.250V$  (device is in dropout).

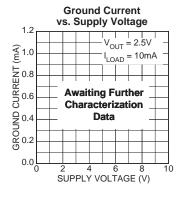
# **Typical Characteristics**

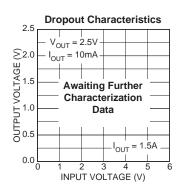


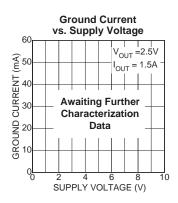




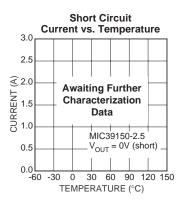


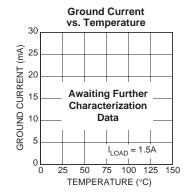


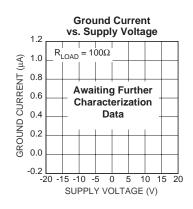


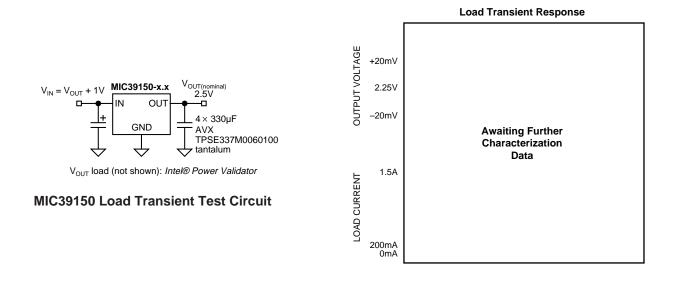


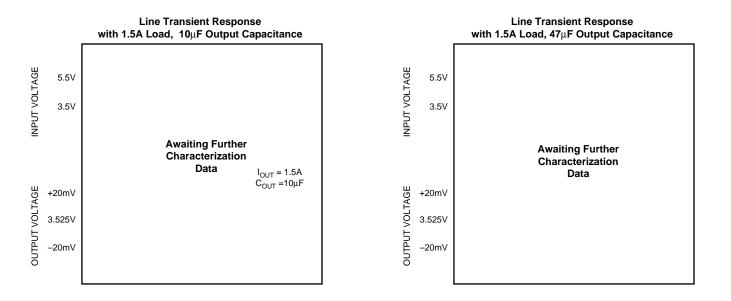
**Ground Current** vs. Temperature 2.5 **GROUND CURRENT (mA)** 2.0 1.5 **Awaiting Further** Characterization 1.0 Data I<sub>LOAD</sub> = 250mA 0.5 0.0 0 25 50 75 100 125 150 TEMPERATURE (°C)

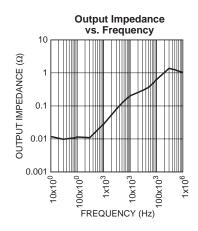






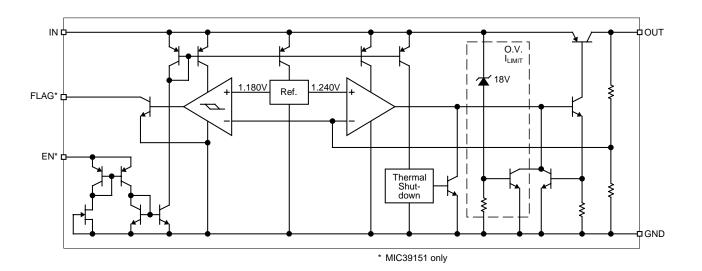






**Section 5: Data Sheets** 

## **Functional Diagram**



### **Applications Information**

The MIC39150/1 is a high-performance low-dropout voltage regulator suitable for moderate to high-current voltage regulator applications. Its 500mV dropout voltage at full load make it especially valuable in battery-powered systems and as high-efficiency noise filters in post-regulator applications. Unlike older NPN-pass transistor designs, where the minimum dropout voltage is limited by the base-to-emitter voltage drop and collector-to-emitter saturation voltage, dropout performance of the PNP output of these devices is limited only by the low  $V_{CE}$  saturation voltage.

A trade-off for the low dropout voltage is a varying base drive requirement. Micrel's Super ßeta PNP<sup>™</sup> process reduces this drive requirement to only 2% to 5% of the load current.

The MIC39150/1 regulator is fully protected from damage due to fault conditions. Current limiting is provided. This limiting is linear; output current under overload conditions is constant. Thermal shutdown disables the device when the die temperature exceeds the maximum safe operating temperature. Transient protection allows device (and load) survival even when the input voltage spike above and below nominal. The output structure of these regulators allows voltages in excess of the desired output voltage to be applied without reverse current flow.

An additional feature of this regulator family is a common pinout: a design's current requirement may change up or down yet use the same board layout, as all of Micrel's highcurrent Super ßeta PNP<sup>™</sup> regulators have identical pinouts.

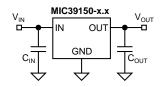


Figure 1. Capacitor Requirements

### **Thermal Design**

Linear regulators are simple to use. The most complicated design parameters to consider are thermal characteristics. Thermal design requires the following application-specific parameters:

- Maximum ambient temperature (T<sub>A</sub>)
- Output Current (I<sub>OUT</sub>)
- Output Voltage (V<sub>OUT</sub>)
- Input Voltage (V<sub>IN</sub>)

First, calculate the power dissipation of the regulator from these numbers and the device parameters from this datasheet.

$$P_{D} = I_{OUT} (1.02V_{IN} - V_{OUT})$$

Where the ground current is approximated by 2% of  $\rm I_{OUT}.$  Then the heat sink thermal resistance is determined with this formula:

$$\theta_{SA} = \frac{T_{J(max)} - T_{A}}{P_{D}} - \left(\theta_{JC} + \theta_{CS}\right)$$

Where  $T_{J \text{ (max)}} \leq 125^{\circ}\text{C}$  and  $\theta_{CS}$  is between 0° and 2°C/W.

The heat sink may be significantly reduced in applications where the minimum input voltage is known and is large compared with the dropout voltage. Use a series input resistor to drop excessive voltage and distribute the heat between this resistor and the regulator. The low dropout properties of Micrel Super ßeta PNP regulators allow significant reductions in regulator power dissipation and the associated heat sink without compromising performance. When this technique is employed, a capacitor of at least  $0.1\mu$ F is needed directly between the input and regulator ground.

Refer to *Application Note 9* for further details and examples on thermal design and heat sink specification.

#### **Capacitor Requirements**

For stability and minimum output noise, a capacitor on the regulator output is necessary. The value of this capacitor is dependent upon the output current; lower currents allow smaller capacitors. MIC39150/1 regulator is stable with a minimum capacitor value of  $10\mu$ F at full load.

This capacitor need not be an expensive low-ESR type: aluminum electrolytics are adequate. Extremely low ESR capacitors may contribute to instability. Tantalum capacitors are recommended for systems where fast load transient response is important.

#### Transient Response and 3.3V to 2.5V Conversion

The MIC39150/1 has excellent response to variations in input voltage and load current. By virtue of its low dropout voltage, this device does not saturate into dropout as readily as similar NPN-based designs. A 2.5V output Micrel LDO regulator will maintain full speed and performance with an input supply as low as 3.4V and will still provide some regulation with supplies down to 3.0V, unlike NPN devices that require 4.3V or more for good performance and become nothing more than a resistor below 3.8V input. Micrel's PNP regulators provide superior performance in 3.3V-to-2.5V conversion applications compared to NPN regulators, especially when all tolerances are considered.

### **Minimum Load Current**

The MIC39150 regulator is specified between finite loads. If the output current is too small, leakage currents dominate and the output voltage rises. A 10mA minimum load current is necessary for proper regulation.

### Error Flag

The MIC39151 version features an error flag circuit which monitors the output voltage and signals an error condition when the voltage 5% below the nominal output voltage. The error flag is an open-collector output that can sink 10mA during a fault condition.

Low output voltage can be caused by a number of problems, including an overcurrent fault (device in current limit) or low input voltage. The flag is inoperative during overtemperature shutdown.

### **Enable Input**

The MIC39151 version features an enable input for on/off control of the device. Its shutdown state draws "zero" current (only microamperes of leakage). The enable input is TTL/

CMOS compatible for simple logic interface, but can be connected to up to 20V. When enabled, it draws approximately  $15 \mu A.$ 



# MIC39300/39301

3A Low-Voltage Low-Dropout Regulator

### **Preliminary Information**

## **General Description**

The MIC39300 and MIC39301 are high-current, high-accuracy low-dropout voltage regulators designed for 2.5V applications. Dropout voltage is guaranteed at 500mV maximum over the operating temperature range, allowing a 2.5V regulated output with as little as 3.0V input. Featuring Micrel's Super ßeta PNP pass element for low ground current, the MIC39300/1 also exhibits fast transient recovery from input voltage surges and output load changes.

The MIC39300/1 is fully protected against overcurrent faults, reversed input polarity, reversed lead insertion, overtemperature operation, and positive and negative voltage spikes.

The MIC39300/1 is available in standard TO-220 and surface-mount TO-263 packages with a junction operating temperature range of 0°C to +125°C.

For applications requiring input voltage greater than 16V, see the MIC29300/1/2/3 family.

## Features

- 2.5V Output
- 3A minimum output current
- Guarenteed 500mV dropout voltage
- 1% guaranteed tolerance
- Low ground current
- Overcurrent and overtemperature protection
- Reversed-battery protection
- Fast transient response

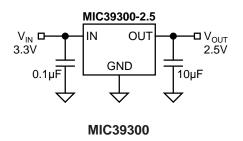
### **Applications**

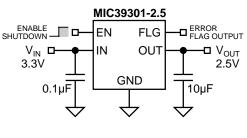
- Multimedia and PC processor supplies
- High-efficiency "green" computer systems
- High-efficiency linear power supplies
- High-efficiency switching supply post regulator
- StrongARM<sup>™</sup> processor supply

## **Ordering Information**

Part Number	Voltage	Junction Temp. Range	Package
MIC39300-2.5BT	2.5V	0°C to +125°C	3-lead TO-220
MIC39300-2.5BU	2.5V	0°C to +125°C	3-lead TO-263
MIC39301-2.5BT	2.5V	0°C to +125°C	5-lead TO-220
MIC39301-2.5BU	2.5V	0°C to +125°C	5-lead TO-263

## **Typical Application**

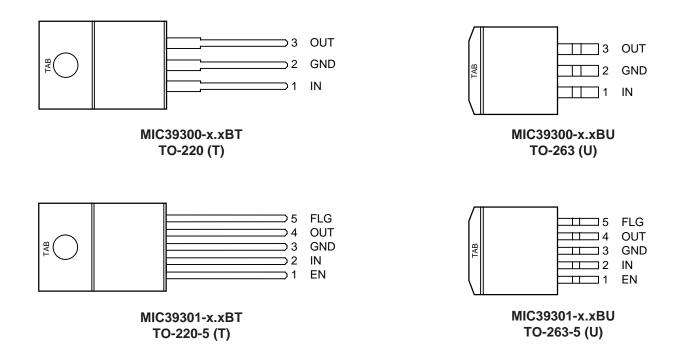




MIC39301

StrongARM is a trademark of Advanced RISC Machines, Ltd.

## **Pin Configuration**



## **Pin Description**

Pin Number MIC39300	Pin Number MIC39301	Pin Name	Pin Function
	1	EN	Enable (Input): Active-high, logic-level enable/shutdown control.
1	2	IN	Unregulated Input: +16V maximum supply.
2, тав	3, tab	GND	Ground: Ground pin and TAB are internally connected.
3	4	OUT	Regulator Output
	5	FLG	Fault Flag (Ouput): Open-collector (active-low) output.

Supply Voltage (V <sub>IN</sub> )	–20V to +20V
Enable Voltage (V <sub>EN</sub> )	+20V
Storage Temperature (T <sub>S</sub> )	. −65°C to +150°C
Lead Temperature (soldering, 5 sec.)	260°C
ESD, Note 3	

# **Operating Ratings (Note 2)**

Supply Voltage (V <sub>IN</sub> )	+16V
Enable Voltage (V <sub>EN</sub> )	+16V
Maximum Power Dissipation (P <sub>D(max)</sub> )	Note 4
Junction Temperature (T <sub>J</sub> )	. 0°C to +125°C
Package Thermal Resistance	
TO-263 (θ <sub>JC</sub> )	2°C/W
TO-220 (θ <sub>JC</sub> )	2°C/W

# **Electrical Characteristics**

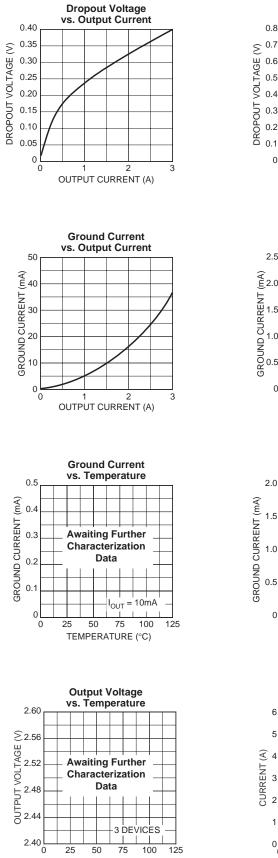
T <sub>J</sub> = 25°C	, <b>bold</b> values	indicate $0^{\circ}C \leq 1$	T <sub>J</sub> ≤ +125°C; ui	nless noted
-----------------------	----------------------	------------------------------	-----------------------------	-------------

Symbol	Parameter	Condition	Min	Тур	Max	Units
V <sub>OUT</sub>	Output Voltage	$10\text{mA} \le \text{I}_{\text{OUT}} \le 3\text{A}, \text{ V}_{\text{OUT}} + 1\text{V} \le \text{V}_{\text{IN}} \le 8\text{V}$	1 <b>-2</b>		1 2	% %
	Line Regulation	$I_{OUT} = 10mA, V_{OUT} + 1V \le V_{IN} \le 8V$		0.06	0.5	%
	Load Regulation	$V_{IN} = V_{OUT} + 1V$ , $10mA \le I_{OUT} \le 3A$		0.2	1	%
$\Delta V_{OUT} / \Delta T$	Output Voltage Temp. Coefficient, Note 5			20	100	ppm/°C
V <sub>DO</sub>	Dropout Voltage, Note 6	$I_{OUT} = 100 \text{mA}, \Delta V_{OUT} = -1\%$		80	200	mV
		$I_{OUT} = 750 \text{mA}, \Delta V_{OUT} = -1\%$		200		mV
		$I_{OUT} = 1.5A, \Delta V_{OUT} = -1\%$		320		mV
		$I_{OUT} = 3A, \Delta V_{OUT} = -1\%$		400	500	mV
I <sub>GND</sub>	Ground Current, Note 7	I <sub>OUT</sub> = 750mA, V <sub>IN</sub> = V <sub>OUT</sub> + 1V		3	20	mA
		$I_{OUT} = 1.5A, V_{IN} = V_{OUT} + 1V$		10		mA
		$I_{OUT} = 3A, V_{IN} = V_{OUT} + 1V$		36		mA
I <sub>GND(do)</sub>	Dropout Ground Pin Current	$V_{IN} \le V_{OUT(nominal)} - 0.5V, I_{OUT} = 10mA$		2	3	mA
I <sub>OUT(lim)</sub>	Current Limit	$V_{OUT} = 0V, V_{IN} = V_{OUT} + 1V$		4.5		A
e <sub>n</sub>	Output Noise Voltage	$C_{OUT} = 47\mu$ F, $I_{OUT} = 100$ mA, 10Hz to 100kHz		260		μV(rms
Enable Inpu	it (MIC39301)				•	
V <sub>EN</sub>	Enable Input Voltage	logic low (off)			0.8	V
		logic high (on)	2.4			V
I <sub>IN</sub>	Enable Input Current	$V_{EN} = V_{IN}$		15	30 <b>75</b>	μA μA
		V <sub>EN</sub> = 0.8V			2 4	μA μA
I <sub>OUT(shdn)</sub>	Shutdown Output Current	Note 8		10	20	μΑ
	(MIC39301)	•				
I <sub>FLG(leak)</sub>	Output Leakage Current	V <sub>OH</sub> = 16V		0.01	1 2	μΑ μΑ
V <sub>FLG(do)</sub>	Output Low Voltage	V <sub>IN</sub> = 2.250V, I <sub>OL</sub> , = 250µA, <b>Note 9</b>		125	150 <b>200</b>	mV mV

Micrel

- Note 1. Exceeding the absolute maximum ratings may damage the device.
- Note 2. The device is not guaranteed to function outside its operating rating.
- **Note 3.** Devices are ESD sensitive. Handling precautions recommended.
- Note 4.  $P_{D(max)} = (T_{J(max)} T_A) \div \theta_{JA}$ , where  $\theta_{JA}$  depends upon the printed circuit layout. See "Applications Information."
- **Note 5.** Output voltage temperature coefficient is  $\Delta V_{OUT(worst case)} \div (T_{J(max)} T_{J(min)})$  where  $T_{J(max)}$  is +125°C and  $T_{J(min)}$  is 0°C.
- Note 6.  $V_{DO} = V_{IN} V_{OUT}$  when  $V_{OUT}$  decreases to 99% of its nominal output voltage with  $V_{IN} = V_{OUT} + 1V$ .
- **Note 7.**  $I_{GND}$  is the quiescent current.  $I_{IN} = I_{GND} + I_{OUT}$ .
- Note 8.  $~V_{EN} \leq 0.8 \text{V}, \, V_{IN} \leq 8 \text{V}, \, \text{and} \, \, V_{OUT} = 0 \text{V}$
- **Note 9.** For a 2.5V device,  $V_{IN} = 2.250V$  (device is in dropout).

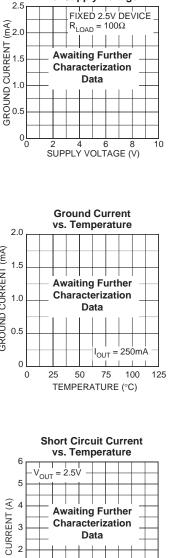
## **Typical Characteristics**



100 125

75

TEMPERATURE (°C)



**Dropout Voltage** 

vs. Temperature

Awaiting Further

Characterization

Data

50 75 100 125

TEMPERATURE (°C)

**Ground Current** 

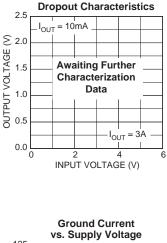
vs. Supply Voltage

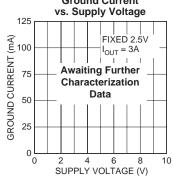
0 L

25

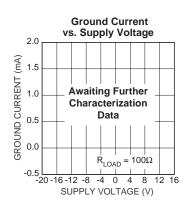
3A

LOAD





**Ground Current** vs. Temperature 60 **GROUND CURRENT** (mA) 50 40 Awaiting Further Characterization 30 Data 20 10 = 3A ουτ 0 0 25 50 75 100 125 TEMPERATURE (°C)



25 50 50

25

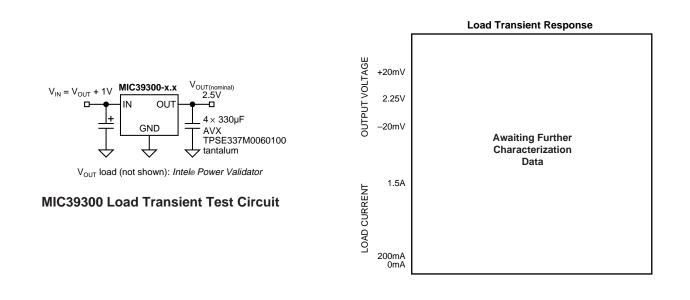
0 L 0

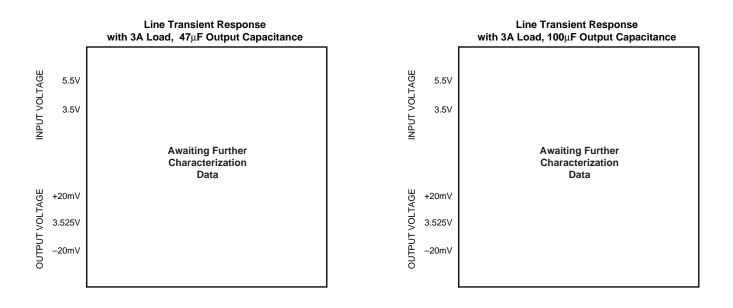
 $V_{OUT} = 0V$ 

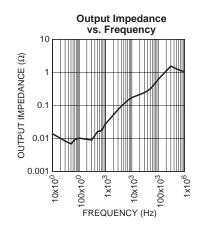
100 125

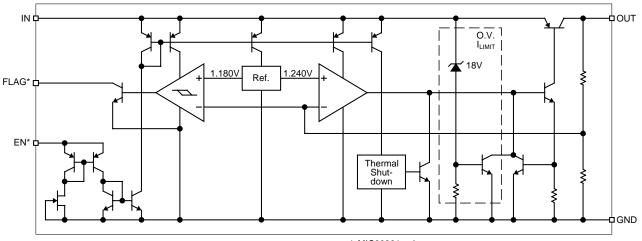
75

TEMPERATURE (°C)









\* MIC39301 only

## **Applications Information**

The MIC39300/1 is a high-performance low-dropout voltage regulator suitable for moderate to high-current voltage regulator applications. Its 500mV dropout voltage at full load makes it especially valuable in battery-powered systems and as a high-efficiency noise filter in post-regulator applications. Unlike older NPN-pass transistor designs, where the minimum dropout voltage is limited by the base-to-emitter voltage drop and collector-to-emitter saturation voltage, dropout performance of the PNP output of these devices is limited only by the low  $V_{CE}$  saturation voltage.

A trade-off for the low dropout voltage is a varying base drive requirement. Micrel's Super ßeta PNP<sup>™</sup> process reduces this drive requirement to only 2% to 5% of the load current.

The MIC29300/1 regulator is fully protected from damage due to fault conditions. Current limiting is provided. This limiting is linear; output current under overload conditions is constant. Thermal shutdown disables the device when the die temperature exceeds the maximum safe operating temperature. Transient protection allows device (and load) survival even when the input voltage spike above and below nominal. The output structure of these regulators allows voltages in excess of the desired output voltage to be applied without reverse current flow.

An additional feature of this regulator family is their common pinout. A design's current requirement may increase or decrease while using the same board layout, since all of Micrel's high-current Super ßeta PNP<sup>™</sup> regulators have identical pinouts.

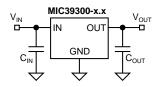


Figure 1. Capacitor Requirements

### **Thermal Design**

Linear regulators are simple to use. The most complicated design parameters to consider are thermal characteristics. Thermal design requires four application-specific parameters:

- Maximum ambient temperature (T<sub>A</sub>)
- Output Current (I<sub>OUT</sub>)
- Output Voltage (V<sub>OUT</sub>)
- Input Voltage (V<sub>IN</sub>)

Calculate the power dissipation of the regulator from these numbers and the device parameters from this datasheet, where the ground current is approximated by 2% of I<sub>OUT</sub>:

$$\mathsf{P}_{\mathsf{D}} = \mathsf{I}_{\mathsf{OUT}} (1.02\mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}})$$

The heat sink thermal resistance is determined by:

$$\theta_{SA} = \frac{T_{J(max)} - T_{A}}{P_{D}} - \left(\theta_{JC} + \theta_{CS}\right)$$

where  $T_{J \text{ (max)}} \leq 125^{\circ}\text{C}$  and  $\theta_{CS}$  is between 0° and 2°C/W.

The heat sink may be significantly reduced in applications where the minimum input voltage is known and is large compared with the dropout voltage. Use a series input resistor to drop excessive voltage and distribute the heat between this resistor and the regulator. The low dropout properties of Micrel Super ßeta PNP regulators allow significant reductions in regulator power dissipation and the associated heat sink without compromising performance. When this technique is employed, a capacitor of at least  $0.1\mu$ F is needed directly between the input and regulator ground.

Refer to *Application Note 9* for further details and examples on thermal design and heat sink specification.

#### **Capacitor Requirements**

For stability and minimum output noise, a capacitor on the regulator output is necessary. The value of this capacitor is dependent upon the output current; lower currents allow smaller capacitors. The MIC39300/1 regulator is stable with a minimum capacitor value of  $47\mu$ F at full load.

This need not be an expensive low-ESR type capacitor aluminum electrolytics are adequate. Extremely low ESR capacitors may contribute to instability. Tantalum capacitors are recommended for systems where fast load transient response is important.

### Transient Response and 3.3V to 2.5V Conversion

The MIC39300/1 has excellent response to variations in input voltage and load current. By virtue of its low dropout voltage, this device does not saturate into dropout as readily as similar NPN-based designs. A 2.5V output Micrel LDO regulator will maintain full speed and performance with an input supply as low as 3.4V and will still provide some regulation with supplies down to 3.0V, unlike NPN devices that require 4.3V or more for good performance and become nothing more than a resistor below 4.6V input. Micrel's PNP regulators provide superior performance in 3.3V-to-2.5V conversion applications when compared to NPN regulators, especially when all tolerances are considered.

### **Minimum Load Current**

The MIC39300/1 regulator is specified between finite loads. If the output current is too small, leakage currents dominate and the output voltage rises. A 10mA minimum load current is necessary for proper regulation.

### Error Flag

The MIC39301 version features an error flag circuit which monitors the output voltage and signals an error condition when the voltage 5% below the nominal output voltage. The error flag is an open-collector output that can sink 10mA during a fault condition.

Low output voltage can be caused by a number of problems, including an overcurrent fault (device in current limit) or low input voltage. The flag is inoperative during overtemperature shutdown.

### **Enable Input**

The MIC39301 version features an enable input for on/off control of the device. Its shutdown state draws "zero" current (only microamperes of leakage). The enable input is TTL/

CMOS compatible for simple logic interface, but can be connected to up to 20V. When enabled, it draws approximately  $15\mu A.$ 



# **MIC5200**

## **100mA Low-Dropout Voltage Regulator**

### **Preliminary Information**

## **General Description**

The MIC5200 is an efficient linear voltage regulator with very low dropout voltage (typically 17mV at light loads and 200mV at 100mA), and very low ground current (1mA at 100mA output), offering better than 1% initial accuracy with a logic compatible ON/OFF switching input. Designed especially for hand-held battery powered devices, the MIC5200 is switched by a CMOS or TTL compatible logic signal. The ENABLE control may be tied directly to V<sub>IN</sub> if unneeded. When disabled, power consumption drops nearly to zero. The ground current of the MIC5200 increases only slightly in dropout, further prolonging battery life. Key MIC5200 features include protection against reversed battery, current limiting, and overtemperature shutdown.

The MIC5200 is available in several fixed voltages and accuracy configurations. Other options are available; contact Micrel for details.

### Features

- High output voltage accuracy
- Variety of output voltages
- Guaranteed 100mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Zero OFF mode current
- Logic-controlled electronic shutdown
- Available in 8-lead SOIC, MM8<sup>™</sup> 8-lead MSOP, and SOT-223 packages

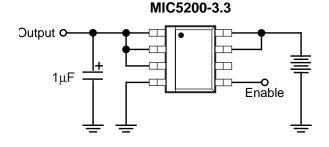
### Applications

- Cellular Telephones
- Laptop, Notebook, and Palmtop Computers
- Battery Powered Equipment
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> Regulation/Switching
- Bar Code Scanners
- SMPS Post-Regulator/ DC to DC Modules
- High Efficiency Linear Power Supplies

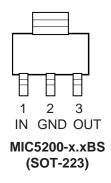
Part Number	Voltage	Accuracy	Junction Temp. Range*	Package
MIC5200-3.0BM	3.0	1%	–40°C to +125°C	SO-8
MIC5200-3.3BM	3.3	1%	–40°C to +125°C	SO-8
MIC5200-4.8BM	4.85	1%	–40°C to +125°C	SO-8
MIC5200-5.0BM	5.0	1%	–40°C to +125°C	SO-8
MIC5200-3.3BMM	3.3V	1%	–40°C to +125°C	MSOP-8
MIC5200-5.0BMM	5.0V	1%	–40°C to +125°C	MSOP-8
MIC5200-3.0BS	3.0	1%	–40°C to +125°C	SOT-223
MIC5200-3.3BS	3.3	1%	–40°C to +125°C	SOT-223
MIC5200-4.8BS	4.85	1%	–40°C to +125°C	SOT-223
MIC5200-5.0BS	5.0	1%	-40°C to +125°C	SOT-223

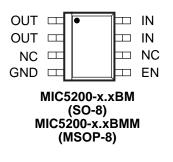
Other voltages available. Contact Micrel for details.

## **Typical Application**



Ordering Information





EN may be tied directly to V<sub>IN</sub>

## **Pin Description**

Pin Number SOT-223	Pin Number SO-8, MSOP-8	Pin Name	Pin Function
3	1, 2	OUT	Output: Pins 1 and 2 must be externally connected together.
	3, 6	NC	(not internally connected): Connect to ground plane for lowest thermal resistance.
2, тав	4	GND	Ground: Ground pin and TAB are internally connected.
	5	EN	Enable/Shutdown (Input): TTL compatible input. High = enabled; low = shutdown.
1	7, 8	IN	Supply Input: Pins 7 and 8 must be extenally connected together.

## **Absolute Maximum Ratings**

Power Dissipation	Internally Limited
Lead Temperature (soldering, 5 sec.)	260°C
Operating Junction Temperature Range	–40°C to +125°C
Input Supply Voltage	–20V to +60V
Enable Input Voltage	–20V to +60V
Thermal Characteristics	
SOT-223 (θ <sub>ιc</sub> )	15°C/W
SO-8 (θ <sub>JA</sub> )	

Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Electrical specifications do not apply when operating the device beyond its specified **Operating Ratings**.

# **Recommended Operating Conditions**

Input Voltage	2.5V to 26V
Operating Junction Temperature Range	–40°C to +125°C
Enable Input Voltage	–20V to V <sub>IN</sub>

## **Electrical Characteristics**

Limits in standard typeface are for $T_{1} = 25^{\circ}$ C and limits in <b>boldface</b> apply over the junction temperature range of $-40^{\circ}$ C to $+125^{\circ}$ C.
Unless otherwise specified, $V_{IN} = V_{OUT} + 1V$ , $I_L = 1$ mA, $C_L = 3.3\mu$ F, and $V_{ENABLE} \ge 2.0$ V

Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>o</sub>	Output Voltage Accuracy	Variation from specified V <sub>OUT</sub>	-1 -2		1 <b>2</b>	%
$\frac{\Delta V_{O}}{\Delta T}$	Output Voltage Temperature Coef.	(Note 2)		40	150	ppm/°C
$\frac{\Delta V_{O}}{V_{IN}}$	Line Regulation	$V_{IN} = V_{OUT} + 1 V \text{ to } 26V$		0.004	0.10 <b>0.40</b>	%
$\frac{\Delta V_{O}}{V_{OUT}}$	Load Regulation	I <sub>L</sub> = 0.1mA to 100mA (Note 3)		0.04	0.16 <b>0.30</b>	%
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage (Note 4)	$I_{L} = 100\mu A$ $I_{L} = 20m A$ $I_{L} = 30m A$ $I_{L} = 50m A$ $I_{L} = 100m A$		17 130 150 190 230	350	mV
I <sub>GND</sub>	Quiescent Current	V <sub>ENABLE</sub> ≤ 0.7V (Shutdown)		0.01	10	μA
I <sub>GND</sub>	Ground Pin Current	$V_{\text{ENABLE}} \ge 2.0\text{V}, I_{\text{L}} = 100\mu\text{A}$ $I_{\text{L}} = 20\text{mA}$ $I_{\text{L}} = 30\text{mA}$ $I_{\text{L}} = 50\text{mA}$ $I_{\text{L}} = 100\text{mA}$		130 270 330 500 1000	350 <b>1500</b>	μΑ
PSRR	Ripple Rejection			70		dB
I <sub>GNDDO</sub>	Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than specified $V_{OUT}$ I <sub>L</sub> = 100 $\mu$ A (Note 5)		270	330	μA
I <sub>LIMIT</sub>	Current Limit	V <sub>OUT</sub> = 0V	100	250		mA
$\frac{\Delta V_{O}}{\Delta P_{D}}$	Thermal Regulation	(Note 6)		0.05		%/W
e <sub>n</sub>	Output Noise			100		μV

### **ENABLE** Input

V <sub>IL</sub>	Input Voltage Level Logic Low Logic High	OFF ON	2.0		0.7	V
I <sub>IL</sub> I <sub>IH</sub>	ENABLE Input Current	$V_{IL} \le 0.7V$ $V_{IH} \ge 2.0V$		0.01 15	1 <b>50</b>	μA

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J (MAX)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_{A}$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{(MAX)} = (T_{J(MAX)} - T_{A}) + \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The  $\theta_{JC}$  of the MIC5200-xxBS is 15°C/W and  $\theta_{JA}$  for the MIC5200BM is 160°C/W mounted on a PC board (see "Thermal Considerations" section for further details).

**Note 2:** Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 0.1mA to 100mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

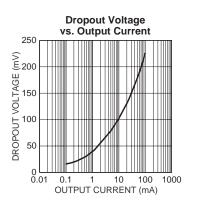
**Note 4:** Dropout Voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

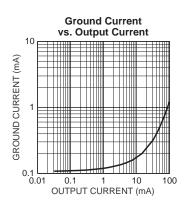
**Note 5:** Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

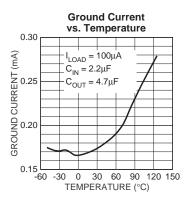
**Note 6:** Thermal regulation is defined as the change in output voltage at a time t after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 100mA load pulse at  $V_{IN} = 26V$  for t = 10ms.

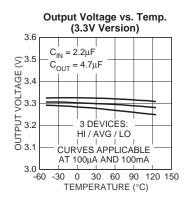
Micrel

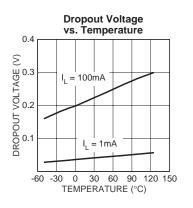
# **Typical Characteristics**

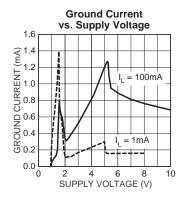


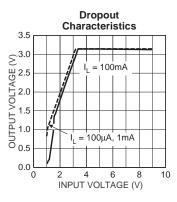


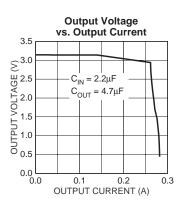




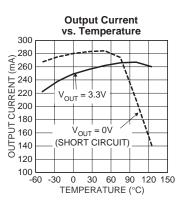


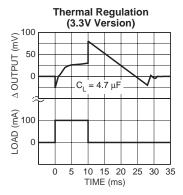


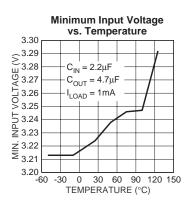




**Ground Current** vs. Temperature 1.5  $I_{LOAD} = 100 \text{mA}$ **GROUND CURRENT (mA)** 1.4  $C_{IN} = 2.2 \mu F$  $C_{OUT} = 4.7 \mu F$ 1.3 1.2 1.1 1.0 └ -50 50 100 150 0 TEMPERATURE (°C)

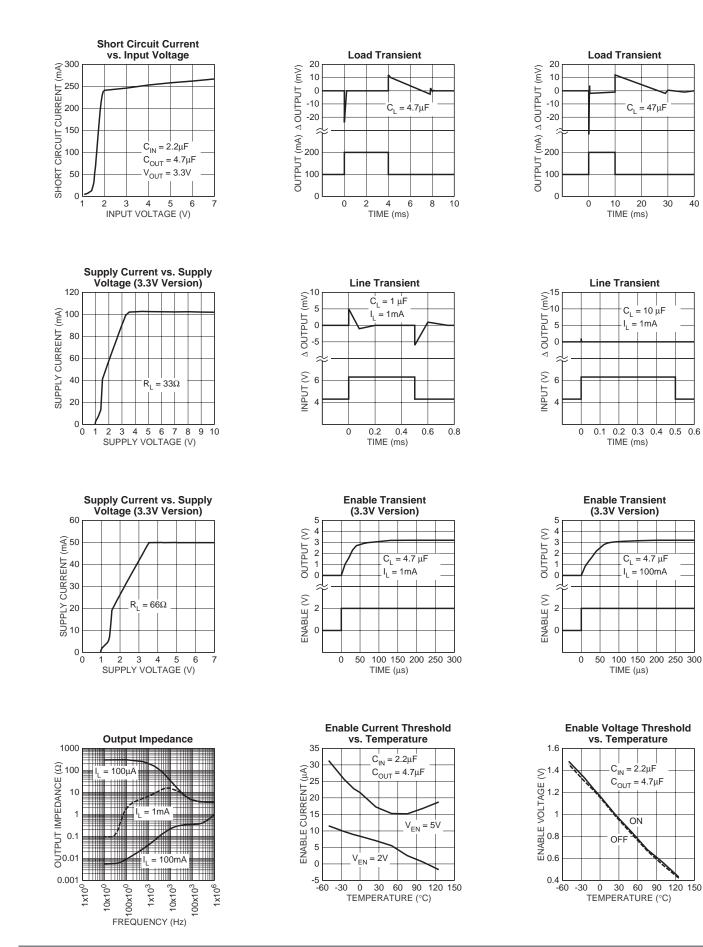


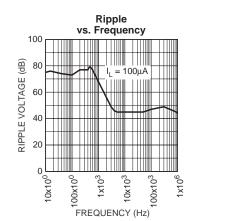


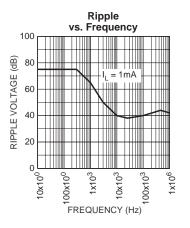


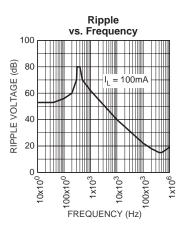
20

30 40









## **Applications Information**

### **External Capacitors**

A 1µF capacitor is recommended between the MIC5200 output and ground to prevent oscillations due to instability. Larger values serve to improve the regulator's transient response. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about –30°C, so solid tantalum capacitors are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1 mA. A 1 $\mu$ F capacitor should be placed from the MIC5200 input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the input.

The MIC5200 will remain stable and in regulation with no load in addition to the internal voltage divider, unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

### **ENABLE** Input

The MIC5200 features nearly zero OFF mode current. When the ENABLE input is held below 0.7V, all internal circuitry is powered off. Pulling this pin high (over 2.0V) re-enables the device and allows operation. The ENABLE pin requires a small amount of current, typically 15 $\mu$ A. While the logic threshold is TTL/CMOS compatible, ENABLE may be pulled as high as 30V, independent of the voltage on V<sub>IN</sub>.

## Thermal Considerations Part I. Layout

The MIC5200-xxBM (8-pin surface mount package) has the following thermal characteristics when mounted on a single layer copper-clad printed circuit board.

PC Board Dielectric	$\boldsymbol{\theta}_{JA}$
FR4	160°C/W
Ceramic	120°C/W

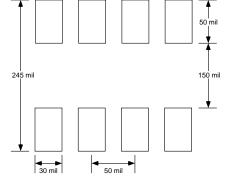
Multi-layer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

The "worst case" value of 160°C/W assumes no ground plane, minimum trace widths, and a FR4 material board.

### Part II. Nominal Power Dissipation and Die Temperature

The MIC5200-xxBM at a 25°C ambient temperature will operate reliably at up to 625mW power dissipation when mounted in the "worst case" manner described above. At an ambient temperature of 55°C, the device may safely dissipate 440mW. These power levels are equivalent to a die temperature of 125°C, the recommended maximum temperature for non-military grade silicon integrated circuits.

For MIC5200-xxBS (SOT-223 package) heat sink characteristics, please refer to Micrel Application Hint 17, "Calculating P.C. Board Heat Sink Area for Surface Mount Packages".



Minimum recommended board pad size, SO-8.



# **MIC5201**

### 200mA Low-Dropout Voltage Regulator

### **General Description**

The MIC5201 is an efficient linear voltage regulator with very low dropout voltage (typically 17mV at light loads and 200mV at 100mA), and very low ground current (1mA at 100mA output), offering better than 1% initial accuracy with a logic compatible on-off switching input.

Designed especially for hand-held battery powered devices, the MIC5201 can be switched by a CMOS or TTL compatible enable signal. This enable control may be connected directly to  $V_{\rm IN}$  if unneeded. When disabled, power consumption drops nearly to zero. The ground current of the MIC5201 increases only slightly in dropout, further prolonging battery life. Key MIC5201 features include current limiting, overtemperature shutdown, and protection against reversed battery.

The MIC5201 is available in several fixed voltages and accuracy configurations. It features the same pinout as the LT1121 with better performance. Other options are available; contact Micrel for details.

### **Features**

- High output voltage accuracy
- Variety of output voltages
- Guaranteed 200mA output
- · Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- · Current and thermal limiting
- Reversed-battery protection
- Load-dump protection (fixed voltage versions)
- Zero off-mode current
- · Logic-controlled electronic enable
- Available in SO-8 and SOT-223 packages

### Applications

- Cellular telephones
- Laptop, notebook, and palmtop computers
- Battery powered equipment
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> regulation/switching
- Bar code scanners
- SMPS post-regulator/ dc-to-dc modules
- High-efficiency linear power supplies

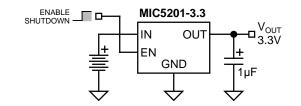
### **Ordering Information**

Part Number	Voltage	Junction Temp. Range*	Package
MIC5201BM	Adj	–40°C to +125°C	SO-8
MIC5201-3.0BM	3.0	–40°C to +125°C	SO-8
MIC5201-3.3BM	3.3	–40°C to +125°C	SO-8
MIC5201-5.0BM	5.0	–40°C to +125°C	SO-8
MIC5201-3.0BS	3.0	–40°C to +125°C	SOT-223
MIC5201-3.3BS	3.3	–40°C to +125°C	SOT-223
MIC5201-4.8BS	4.85	–40°C to +125°C	SOT-223
MIC5201-5.0BS	5.0	–40°C to +125°C	SOT-223

Other voltages available. Contact Micrel for details.

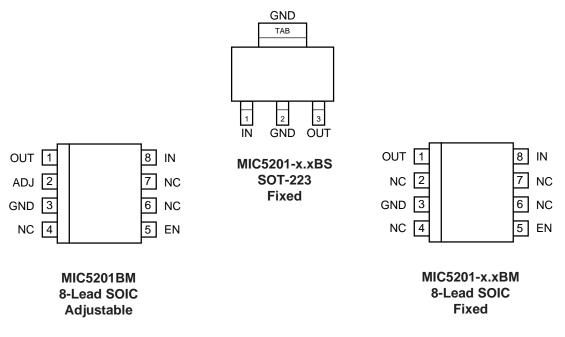
\* Junction Temperature.

## **Typical Application**



MM8 is a trademark of Micrel, Inc.

## **Pin Configuration**



## **Pin Description**

Pin No. SOT-223	Pin No. SO-8 Adj.	Pin No. SO-8 Fixed	Pin Name	Pin Function
3	1	1	OUT	Regulated Output
	2		ADJ	Feedback Input: (Adjustable version only)
	4, 6, 7	2, 4, 6, 7	NC	not internally connected: Connect to ground plane for lowest thermal resistance.
2	3	3	GND	Ground
	5	5	EN	Enable (Input): TTL compatible input. High = enable. Low or open = off/disable.
1	8	8	V <sub>IN</sub>	Unregulated Supply Input

## **Absolute Maximum Ratings**

Supply Input Voltage (VIN) Fixed	–20V to +60V
Supply Input Voltage (VIN) Adjustable	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> ) Fixed	–20V to +60V
Enable Input Voltage (V <sub>EN</sub> ) Adjustable	–20V to +20V
Power Dissipation (P <sub>D</sub> )	. Internally Limited
Junction Temperature (T <sub>J</sub> )	. –40°C to +125°C
Lead Temperature (soldering, 5 sec.)	260°C

# **Operating Ratings**

Supply Input Voltage (VIN) Fixed	2.5V to +26V
Supply Input Voltage (VIN) Adjustable	2.5V to +16V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature (T <sub>1</sub> )	–40°C to +125°C

## Electrical Characteristics

Symbol	Parameter	Condition	Min	Тур	Max	Units
V <sub>O</sub>	Output Voltage Accuracy	Variation from specified V <sub>OUT</sub>	-1 -2		1 2	% %
$\Delta V_O / \Delta T$	Output Voltage Temperature Coef.	Note 2		40	150	ppm/°
$\Delta V_0 / V_0$	Line Regulation, Fixed	$V_{IN} = V_{OUT} + 1V$ to 26V		0.004	0.20 <b>0.40</b>	% %
$\Delta V_0 / V_0$	Line Regulation, Adjustable	$V_{IN} = V_{OUT} + 1V$ to 16V		0.004	0.20 <b>0.40</b>	% %
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 200mA, <b>Note 3</b>		0.04	0.16 <b>0.30</b>	% %
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage, Note 4	$I_{L} = 100\mu A$ $I_{L} = 20m A$ $I_{L} = 50m A$ $I_{L} = 100m A$ $I_{L} = 200m A$		17 130 180 225 270	400	mV mV mV mV mV
I <sub>GND</sub>	Quiescent Current	$V_{\text{ENABLE}} \leq 0.7 V \text{ (shutdown)}$		0.01		μΑ
I <sub>GND</sub>	$ \begin{array}{ c c c c c } \hline Ground \mbox{Pin Current} & I_L = 100 \mu A \\ I_L = 20 m A \\ I_L = 50 m A \\ I_L = 100 m A \\ I_L = 200 m A \end{array} $		130 270 500 1000 3000	400 <b>2000</b>	μΑ μΑ μΑ μΑ μΑ	
PSRR	Ripple Rejection			75		dB
I <sub>GNDDO</sub>	Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than specified $V_{OUT}$ , $I_L = 100\mu A$ , <b>Note 5</b>		270	330	μΑ
ILIMIT	Current Limit	V <sub>OUT</sub> = 0V		280	500	mA
$\Delta V_O / \Delta P_D$	Thermal Regulation	Note 6		0.05		%/W
e <sub>n</sub>	Output Noise			100		μV
Enable Inp	ıt	•	•	•		
V <sub>IL</sub>	Input Voltage Level	logic low (off)			0.7	V
V <sub>IH</sub>	Input Voltage Level	logic high (on)	2.0			V
I <sub>IL</sub>	Enable Input Current	$V_{IL} \leq 0.7V$		0.01	1	μA
I <sub>IH</sub>	Enable Input Current	$V_{IH} \le 2.0V$		15	50	μA
	MIC5201 Adjustable Version Only)	•	•	•		-
V <sub>REF</sub>	Reference Voltage		1.223 <b>1.217</b>	1.242	1.255 <b>1.267</b>	V V
IIL	Reference Voltage Temp. Coef.			20		ppm/°0

General Note: Devices are ESD sensitive. Handling precautions recommended.

Note 1: Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{(max)} = (T_{J(max)} - T_A) + \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The  $\theta_{JC}$  of the MIC5201-x.xBS is 15°C/W and  $\theta_{JA}$  for the MIC5201BM is 160°C/W mounted on a PC board (see "Thermal Considerations" section for further details).

Note 2: Output voltage temperature coefficient is defined as the worst-case voltage change divided by the total temperature range.

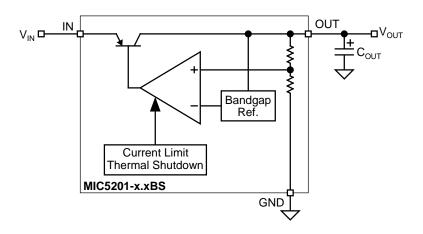
Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load Note 3: range from 0.1mA to 200mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

Dropout Voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V Note 4: differential.

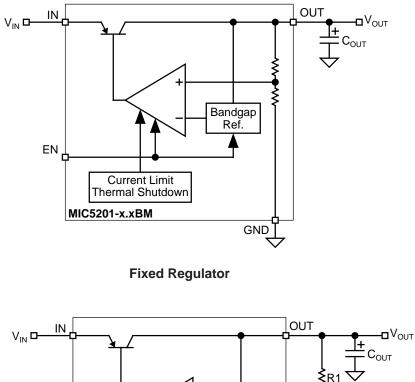
Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of Note 5: the load current plus the ground pin current.

Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line Note 6: regulation effects. Specifications are for a 200mA load pulse at  $V_{IN}$  = 26V for fixed and  $V_{IN}$  = 16V for adjustable at t = 10ms. Section 5: Data Sheets 205 **Designing With LDO Regulators** 

## **Block Diagrams**







EN Current Limit Thermal Shutdown MIC5201BM [adj.] GND

Adjustable Regulator

250

150 100

50

10

GROUND CURRENT (mA)

0.1 – 0.01

0.30

GROUND CURRENT (mA) 0.50 0.50

0.15 L -60

0.1

0.01 0.1

€ 200

DROPOUT VOLTAGE

**Dropout Voltage** 

vs. Output Current

10 100 1000

OUTPUT CURRENT (mA)

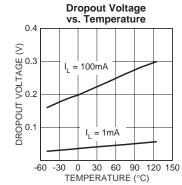
**Ground Current** 

vs. Output Current

OUTPUT CURRENT (mA)

**Ground Current** 

1



1.6

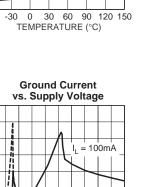
(mA) 1.4 1.2 0.0 0.6 0.4 0.6 0.4 0.2

0.0

0

2

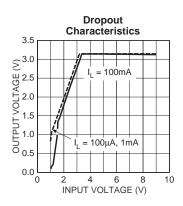
4

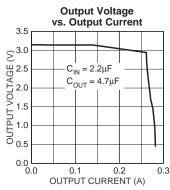


= 1mA

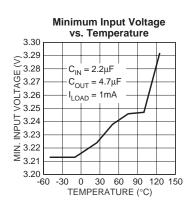
6 8

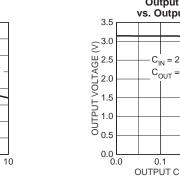
SUPPLY VOLTAGE (V)

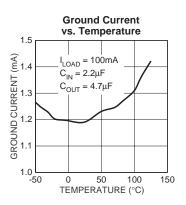




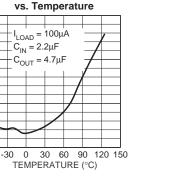
Thermal Regulation (3.3V Version) (100 50 0 € C<sub>L</sub> = 4.7 μF LOAD (mA) 100 0 0 5 10 15 20 25 30 35 TIME (ms)





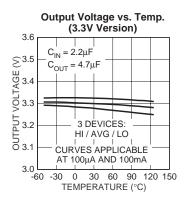


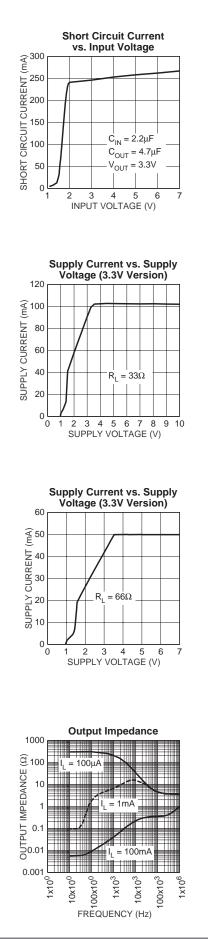
**Output Current** vs. Temperature 300 280 € 280 € 260 240 220 200 180 160 140 200  $V_{OUT} = 3.3V$  $V_{OUT} = 0V$ (SHORT CIRCUIT) 120 100 30 60 90 120 150 -60 -30 0 TEMPERATURE (°C)

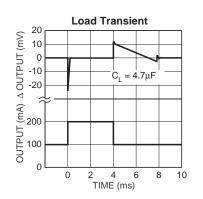


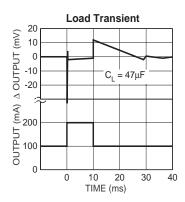
10

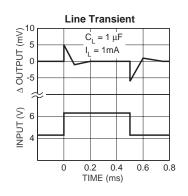
100

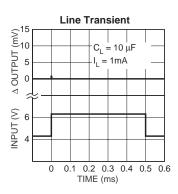










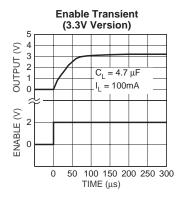


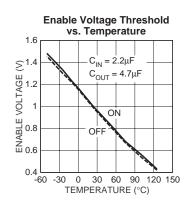
OUTPUT (V)

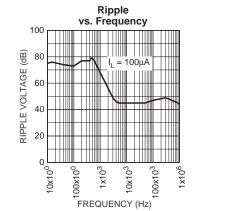
ENABLE (V)

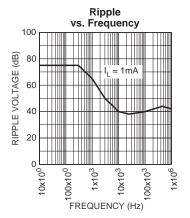
0 50 100 150 200 250 300 TIME (μs)

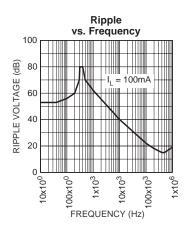
Enable Current Threshold vs. Temperature  $C_{IN} = 2.2\mu F$  $C_{OUT} = 4.7\mu F$  $C_{OUT} = 4.7\mu F$  $V_{EN} = 5V$  $V_{EN} = 5V$  $C_{OUT} = 4.7\mu F$  $C_{OUT} = 4.7\mu F$ 











## **Applications Information**

Figure 1 shows a basic fixed-voltage application with the unused enable input connected to  $V_{\mbox{\scriptsize IN}}.$ 

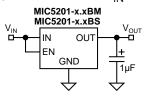
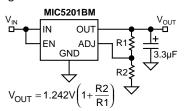


Figure 1. Fixed Application

Adjustable regulators require two resistors to set the output voltage. See Figure 2.



#### Figure 2. Adjustable Application

Resistors values are not critical because ADJ (adjust) has a high impedance, but for best results use resistors of  $470k\Omega$  or less.

### **Output Capacitors**

A 1µF capacitor is recommended between the MIC5201 output and ground to prevent oscillations due to instability. Larger values serve to improve the regulator's transient response. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about –30°C, so solid tantalums are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

#### **Input Capacitors**

A 1 $\mu$ F capacitor should be placed from the MIC5201 input to ground if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

#### **Noise Reduction Capacitors**

On adjustable devices, a capacitor from ADJ to GND will decrease high-frequency noise on the output. See Figure 3.

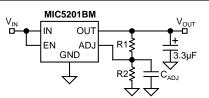


Figure 3. Decreasing Ouput Noise

#### **Minimum Load**

The MIC5201 will remain stable and in regulation with no load unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

#### **Dual-Supply Systems**

When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.Thermal Considerations

#### Layout

The MIC5201-x.xBM (8-pin surface mount package) has the following thermal characteristics when mounted on a single layer copper-clad printed circuit board.

PC Board Dielectric	θ <sub>JA</sub>
FR4	160° C/W
Ceramic	120° C/W

Multilayer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

The "worst case" value of 160°C/W assumes no ground plane, minimum trace widths, and a FR4 material board.

#### Nominal Power Dissipation and Die Temperature

The MIC5201-x.xBM at a 25°C ambient temperature will operate reliably at up to 625mW power dissipation when mounted in the "worst case" manner described above. At an ambient temperature of 55°C, the device may safely dissipate 440mW. These power levels are equivalent to a die temperature of 125°C, the recommended maximum temperature for non-military grade silicon integrated circuits.

For MIC5201-x.xBS (SOT-223 package) heat sink characteristics, please refer to Micrel Application Hint 17, *P.C. Board Heat Sinking*.

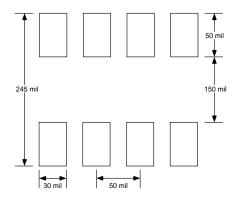


Figure 4. Min. Recommended SO-8 PCB Pads Size



# **MIC5202**

Dual 100mA Low-Dropout Voltage Regulator

### **Preliminary Information**

## **General Description**

The MIC5202 is a family of dual linear voltage regulators with very low dropout voltage (typically 17mV at light loads and 210mV at 100mA), and very low ground current (1mA at 100mA output–each section), offering better than 1% initial accuracy with a logic compatible ON/OFF switching input. Designed especially for hand-held battery powered devices, the MIC5202 is switched by a CMOS or TTL compatible logic signal. This ENABLE control my be tied directly to  $V_{IN}$  if unneeded. When disabled, power consumption drops nearly to zero. The ground current of the MIC5202 increases only slightly in dropout, further prolonging battery life. Key MIC5202 features include protection against reversed battery, current limiting, and over-temperature shutdown.

The MIC5202 is available in several fixed voltages. Other options are available; contact Micrel for details.

## Features

- High output voltage accuracy
- Variety of output voltages
- Guaranteed 100mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Reverse-battery protection
- Zero OFF mode current
- Logic-controlled electronic shutdown
- Available in SO-8 package

### Applications

- Cellular Telephones
- Laptop, Notebook, and Palmtop Computers
- Battery Powered Equipment
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> Regulation/Switching
- Bar Code Scanners
- SMPS Post-Regulator/ DC to DC Modules
  - High Efficiency Linear Power Supplies

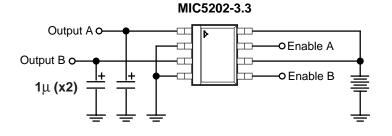
## **Ordering Information**

Part Number	Volts	Accuracy	Temperature Range*	Package
MIC5202-3.0BM	3.0	1%	–40°C to +125°C	SO-8
MIC5202-3.3BM	3.3	1%	–40°C to +125°C	SO-8
MIC5202-4.8BM	4.85	1%	–40°C to +125°C	SO-8
MIC5202-5.0BM	5.0	1%	–40°C to +125°C	SO-8

\* Junction Temperature

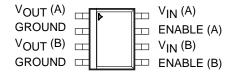
Other voltages are available; contact Micrel for details.

## **Typical Application**



ENABLE pins may be tied directly to  $V_{IN}$ 

## **Pin Configuration**



#### MIC5202-xxBM

Both GROUND pins must be tied to the same potential.  $V_{IN}$  (A) and  $V_{IN}$  (B) may run from separate supplies.

## **Absolute Maximum Ratings**

Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Electrical specifications do not apply when operating the device beyond its specified **Operating Ratings.** 

Power Dissipation	Internally Limited
Lead Temperature (Soldering, 5 seconds)	260°C
Operating Junction Temperature Range	–40°C to +125°C
Input Supply Voltage	–20V to +60V
ENABLE Input Voltage	–20V to +60V
SO-8 θ <sub>JA</sub>	See Note 1

# **Recommended Operating Conditions**

Input Voltage 2.5V to 26V	
Operating Junction Temperature Range –40°C to +125°C	
ENABLE Input Voltage 0V to V	

## **Electrical Characteristics**

Limits in standard typeface are for  $T_J = 25^{\circ}$ C and limits in **boldface** apply over the junction temperature range of -40°C to +125°C. Specifications are for each half of the (dual) MIC5202. Unless otherwise specified,  $V_{IN} = V_{OUT} + 1V$ ,  $I_L = 1$ mA,  $C_L = 10\mu$ F, and  $V_{CONTROL} \ge 2.0$ V.

Symbol	Parameter	Condition	Min	Тур	Max	Units
V <sub>O</sub>	Output Voltage	Variation from specified V <sub>OUT</sub> Accuracy	-1 -2		1 2	%
$\frac{\Delta V_{O}}{\Delta T}$	Output Voltage Temperature Coef.	(Note 2)		40	150	ppm/°C
$\frac{\Delta V_{O}}{V_{O}}$	Line Regulation	$V_{IN} = V_{OUT} + 1 V \text{ to } 26V$		0.004	0.10 <b>0.40</b>	%
$\frac{\Delta V_{O}}{V_{O}}$	Load Regulation	I <sub>L</sub> = 0.1mA to 100mA (Note 3)		0.04	0.16 <b>0.30</b>	%
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage (Note 4)	$I_{L} = 100\mu A$ $I_{L} = 20m A$ $I_{L} = 30m A$ $I_{L} = 50m A$ $I_{L} = 100m A$		17 130 150 180 225	350	mV
l <sub>Q</sub>	Quiescent Current	$V_{CONTROL} \le 0.7V$ (Shutdown)		0.01		μΑ
I <sub>GND</sub>	Ground Pin Current	$V_{CONTROL} \ge 2.0V, I_{L} = 100\mu A$ $I_{L} = 20m A$ $I_{L} = 30m A$ $I_{L} = 50m A$ $I_{L} = 100m A$		170 270 330 500 1200	1500	μΑ
PSRR	Ripple Rejection			75		dB
I <sub>GNDDO</sub>	Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less specified $V_{OUT}$ , $I_{L} = 100\mu$ A (Note 5)		270	330	μΑ
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		280		mA
$\frac{\Delta V_{O}}{\Delta P_{D}}$	Thermal Regulation	(Note 6)		0.05		%/W
e <sub>n</sub>	Output Noise			100		μV

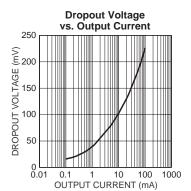
## **Control Input**

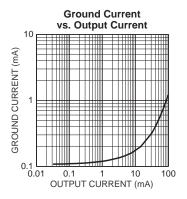
V <sub>IL</sub>	Input Voltage Level Logic Low Logic High	OFF ON	2.0		0.7	V
I <sub>IL</sub> IH	Control Input Current	$V_{IL} \le 0.7V$ $V_{IH} \ge 2.0V$		0.01 8	50	μA

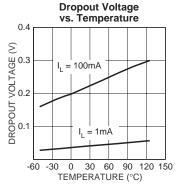
212

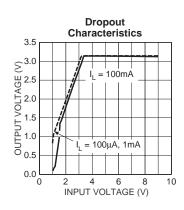
Note 1:	Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature, $T_{J(MAX)}$ the junction-to-ambient thermal resistance, $\theta_{JA}$ , and the ambient temperature, $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using: $P_{(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The junction to ambient thermal resistance of the MIC5202BM is 160°C/W mounted on a PC board.
Note 2:	Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.
Note 3:	Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 0.1mA to 100mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.
Note 4:	Dropout Voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.
Note 5:	Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.
Note 6:	Thermal regulation is defined as the change in output voltage at a time t after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 100mA load pulse at $V_{IN} = 26V$ for t = 10ms, and is measured separately for each section.

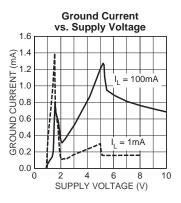
## Typical Characteristics (Each Regulator—2 Regulators/Package)

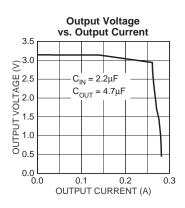


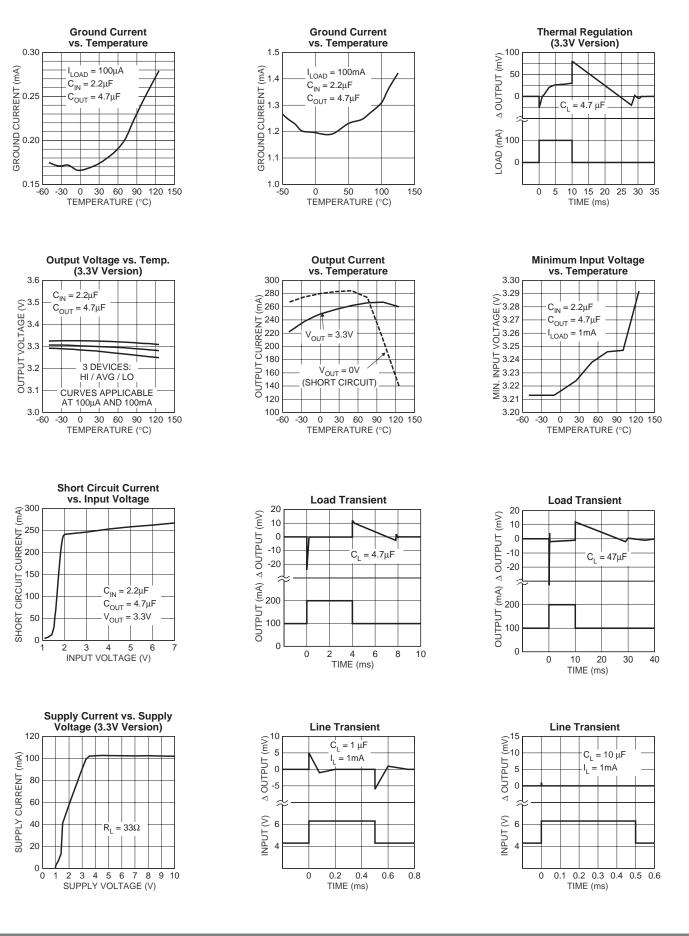


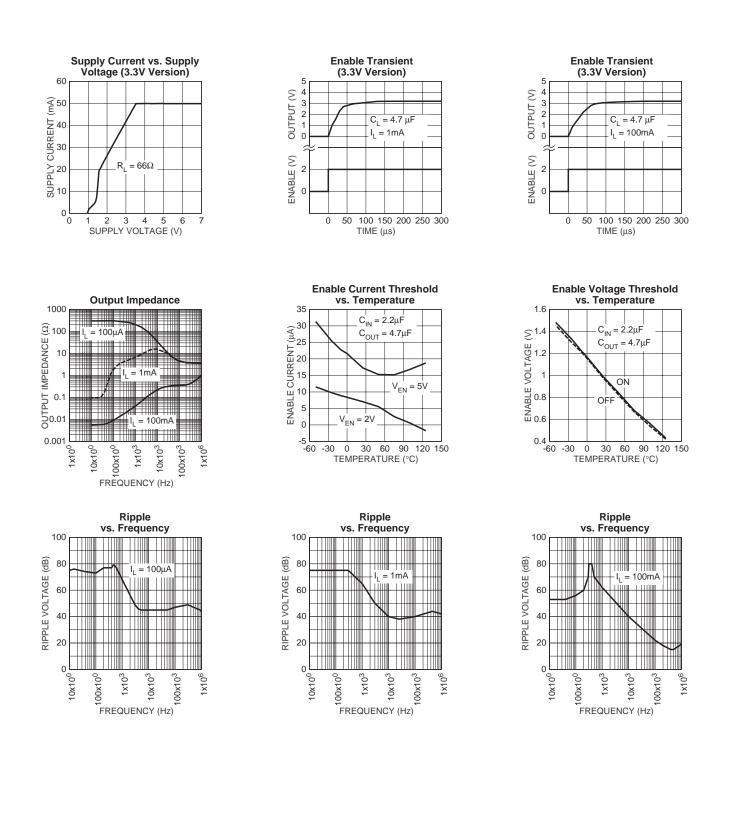












## **Applications Information**

### **External Capacitors**

A 1µF capacitor is recommended between the MIC5202 output and ground to prevent oscillations due to instability. Larger values serve to improve the regulator's transient response. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about –30°C, so solid tantalums are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1 mA. A 1 $\mu$ F capacitor should be placed from the MIC5202 input to ground if there is more than 10 inches of wire between the input and the AC filter capacitor or if a battery is used as the supply.

### **ENABLE Input**

The MIC5202 features nearly zero OFF mode current. When the ENABLE input is held below 0.7V, all internal circuitry is powered off. Pulling this pin high (over 2.0V) re-enables the device and allows operation. The ENABLE pin requires a small amount of current, typically 15µA. While the logic threshold is TTL/CMOS compatible, ENABLE may be pulled as high as 30V, independent of the voltage on V<sub>IN</sub>. The two portions of the MIC5202 may be enabled separately.

### **General Notes**

The MIC5202 will remain stable and in regulation with no load in addition to the internal voltage divider, unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications. Thermal shutdown is independant on both halfs of the dual MIC5202, however an over-temperature condition on one half might affect the other because of proximity. When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

Both MIC5202 GROUND pins must be tied to the same ground potential. Isolation between the two halfs allows connecting the two  $V_{IN}$  pins to different supplies.

### Thermal Considerations Part I. Layout

The MIC5202-xxBM (8-pin surface mount package) has the following thermal characteristics when mounted on a single layer copper-clad printed circuit board.

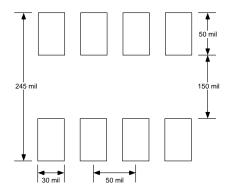
PC Board Dielectric	θ <sub>JA</sub>	
FR4	160°C/W	
Ceramic	120°C/W	

Multi-layer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

The "worst case" value of 160°C/W assumes no ground plane, minimum trace widths, and a FR4 material board.

#### Part II. Nominal Power Dissipation and Die Temperature

The MIC5202-xxBM at a 25°C ambient temperature will operate reliably at up to 625mW power dissipation when mounted in the "worst case" manner described above. At an ambient temperature of 55°C, the device may safely dissipate 440mW. These power levels are equivalent to a die temperature of 125°C, the recommended maximum temperature for non-military grade silicon integrated circuits.



Minimum recommended board pad size, SO-8.



# MIC5203

## 80mA Low-Dropout Voltage Regulator

## **General Description**

The MIC5203 is a family of efficient linear voltage regulators with very low dropout voltage (typically 20mV at light loads and 300mV at 80mA) and very low ground current ( $225\mu$ A at 10mA output), offering better than 3% initial accuracy with a logic-compatible enable input.

Designed especially for hand-held, battery-powered devices, the MIC5203 can be controlled by a CMOS or TTL compatible logic signal. When disabled, power consumption drops nearly to zero. If on-off control is not required, the enable pin may be tied to the input for 3-terminal operation. The ground current of the MIC5203 increases only slightly in dropout, further prolonging battery life. Key MIC5203 features include current limiting, overtemperature shutdown, and protection against reversed battery.

The MIC5203 is available in 3.0V, 3.3V, 3.6V, 3.8V, 4.0V, 4.5V, 4.75V, and 5.0V fixed voltages. Other voltages are available; contact Micrel for details.

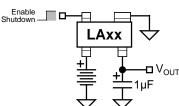
## **Features**

- · Tiny 4-lead and 5-lead surface-mount packages
- Wide Selection of output voltages
- Guaranteed 80mA output
- Low quiescent current
- Low dropout voltage
- Tight load and line regulation
- Low temperature coefficient
- Current and thermal limiting
- Reversed input polarity protection
- Zero off-mode current
- Logic-controlled electronic shutdown

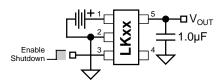
# Applications

- Cellular telephones
- Laptop, notebook, and palmtop computers
- Battery-powered equipment
- Bar code scanners
- SMPS post-regulator/dc-to-dc modules
- High-efficiency linear power supplies

# **Typical Applications**



SOT-143 Version



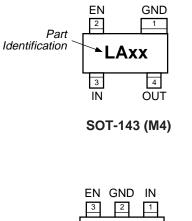
SOT-23-5 Version

# **Ordering Information**

Part Number	Marking	Voltage	Junction Temp. Range	Package
MIC5203-3.0BM4	LA30	3.0	–40°C to +125°C	SOT-143
MIC5203-3.3BM4	LA33	3.3	–40°C to +125°C	SOT-143
MIC5203-3.6BM4	LA36	3.6	–40°C to +125°C	SOT-143
MIC5203-3.8BM4	LA38	3.8	–40°C to +125°C	SOT-143
MIC5203-4.0BM4	LA40	4.0	–40°C to +125°C	SOT-143
MIC5203-4.5BM4	LA45	4.5	–40°C to +125°C	SOT-143
MIC5203-4.7BM4	LA47	4.75	–40°C to +125°C	SOT-143
MIC5203-5.0BM4	LA50	5.0	–40°C to +125°C	SOT-143
MIC5203-3.0BM5	LK30	3.0	–40°C to +125°C	SOT-23-5
MIC5203-3.3BM5	LK33	3.3	–40°C to +125°C	SOT-23-5
MIC5203-3.6BM5	LK36	3.6	–40°C to +125°C	SOT-23-5
MIC5203-3.8BM5	LK38	3.8	–40°C to +125°C	SOT-23-5
MIC5203-4.0BM5	LK40	4.0	–40°C to +125°C	SOT-23-5
MIC5203-4.5BM5	LK45	4.5	–40°C to +125°C	SOT-23-5
MIC5203-4.7BM5	LK47	4.75	–40°C to +125°C	SOT-23-5
MIC5203-5.0BM5	LK50	5.0	–40°C to +125°C	SOT-23-5

Other voltages available. Contact Micrel for details.

# **Pin Configuration**





SOT-23-5 (M5)

# **Pin Description**

Pin Number SOT-143	Pin Number SOT-23-5	Pin Name	Pin Function
1	2	GND	Ground
2	3	EN	Enable (Input): TTL/CMOS compatible control input. Logic high = enabled; logic low or open = shutdown.
3	1	IN	Supply Input
	4	NC	Not internally connected.
4	5	OUT	Regulator Output

# **Absolute Maximum Ratings**

Input Supply Voltage (VIN)	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited
Storage Temperature Range (T <sub>S</sub> )	–60°C to +150°C
Lead Temperature (Soldering, 5 sec.)	

Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Electrical specifications do not apply when operating the device beyond its specified Operating Ratings.

# **Operating Ratings**

Input Voltage (V <sub>IN</sub> )	2.5V to 16V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature Range	–40°C to +125°C
Thermal Resistance $(\theta_{JA})$	Note 1

## **Electrical Characteristics**

Symbol	Parameter	Conditions	Min	Тур	Max	Units
Vo	Output Voltage Accuracy		-3		3	%
			-4		4	%
$\Delta V_O / \Delta T$	Output Voltage Temp. Coefficient	Note 2		50	200	ppm/°C
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.008	0.3 <b>0.5</b>	% %
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 80mA, <b>Note 3</b>		0.08	0.3 <b>0.5</b>	% %
V <sub>IN</sub> –V <sub>O</sub>	Dropout Voltage, Note 4	I <sub>L</sub> = 100μA		20		mV
		I <sub>L</sub> = 20mA		200	350	mV
		I <sub>L</sub> = 50mA		250		mV
		I <sub>L</sub> = 80mA		300	600	mV
I <sub>Q</sub>	Quiescent Current	$V_{EN} \le 0.4V$ (shutdown)		0.01	10	μΑ
I <sub>GND</sub>	Ground Pin Current, Note 5	$I_L = 100\mu A, V_{EN} \ge 2.0V \text{ (active)}$		180		μΑ
		$I_L = 20$ mA, $V_{EN} \ge 2.0V$ (active)		225	750	μΑ
		$I_L = 50 \text{mA}, V_{EN} \ge 2.0 \text{V} \text{ (active)}$		850		μΑ
		$I_L = 80 \text{mA}, V_{EN} \ge 2.0 \text{V} \text{ (active)}$		1800	3000	μΑ
I <sub>GNDDO</sub>	Ground Pin Current at Dropout	$V_{IN} = V_{OUT(nominal)} - 0.5V$ , Note 5		200	300	μΑ
I <sub>LIMIT</sub>	Current Limit	V <sub>OUT</sub> = 0V		180	250	mA
$\overline{\Delta V_{O/}\Delta P_D}$	Thermal Regulation	Note 6		0.05		%/W

#### **Control Input**

	Input Voltage Level					
V <sub>IL</sub>		logic Low (off)			0.6	μΑ
V <sub>IH</sub>		logic high (on)	2.0			μA
I	Control Input Current	$V_{IL} \le 0.6V$		0.01	1	μA
I <sub>IH</sub>		$V_{IH} \ge 2.0V$		15	50	μΑ

General Note: Devices are ESD protected, however, handling precautions are recommended.

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{D(max)} = (T_{J(max)} - T_A) \div \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown.  $\theta_{JA}$  of the SOT-143 is 250°C/W, mounted on a PC board. Under similar conditions, the  $\theta_{JA}$  of the SOT-23-5 is 220°C/W.

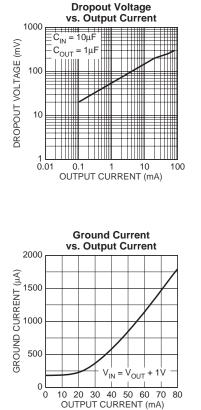
Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

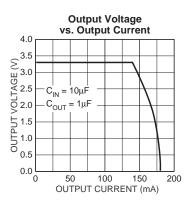
**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

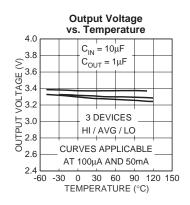
Note 4: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

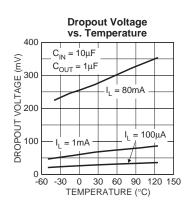
Note 5: Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

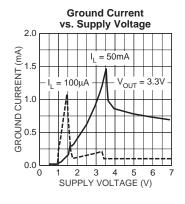
**Note 6:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for an 80mA load pulse at  $V_{IN} = 16V$  for t = 10ms.

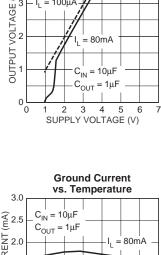












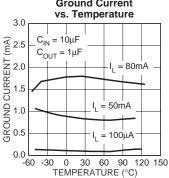
Dropout

Characteristics

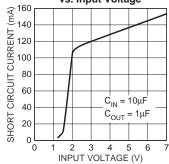
= 100µA

4

S

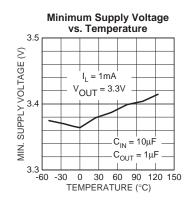


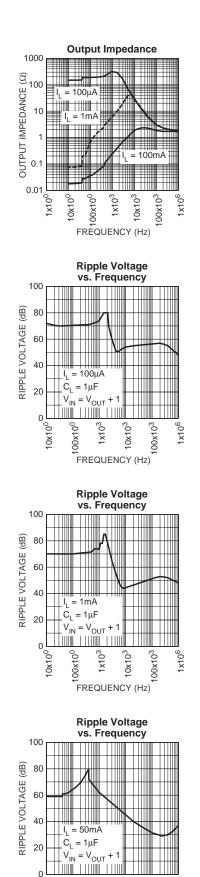
Short Circuit Current vs. Input Voltage

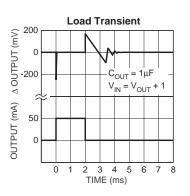


**Short Circuit Current** vs. Temperature 200 0011B01 160 140 120 140 120  $C_{IN} = 10 \mu F$  $C_{OUT} = 1 \mu F$ 100 <u>–</u> -60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

**Thermal Regulation** (3.3V Version) 60 △ OUTPUT (mV) 40 20 0 -20 -40 LOAD (mA) 50 0  $C_{L} = 1 \mu F$ 0 2 4 6 8 10 12 14 16 TIME (ms)







Line Transient

 $\dot{C}_L = 1 \mu F$ 

= 1mA

3

2

1

0

-1

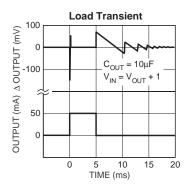
6

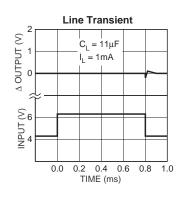
4

0.0

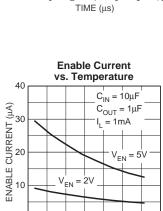
A OUTPUT (V)

INPUT (V)

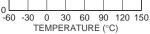




**Enable Characteristics** (3.3V Version) 4.0 OUTPUT (V) 3.0 2.0 1.0  $C_1 = 1\mu F$ 0.0  $I_L = 100 \mu A$ ENABLE (V) 2 0 0 2 4 6



8 10

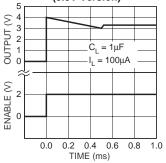


Enable Characteristics (3.3V Version)

0.2 0.4 0.6

TIME (ms)

0.8 1.0



**Section 5: Data Sheets** 

100×10<sup>0</sup>

1×10<sup>3</sup>

FREQUENCY (Hz)

10x10<sup>3</sup> 100x10<sup>3</sup> 1x10<sup>6</sup>

10×10<sup>0</sup>

## **Applications Information**

### **External Capacitors**

A 1 $\mu$ F capacitor is recommended between the MIC5203 output and ground to prevent oscillations due to instability. Larger values serve to improve the regulator's transient response. Most types of tantalum or aluminum electrolytics will be adequate; film types will work, but are costly and therefore not recommended. Many aluminum electrolytics have electrolytes that freeze at about–30°C, so solid tantalums are recommended for operation below –25°C. The important parameters of the capacitor are an effective series resistance of about 5 $\Omega$  or less and a self-resonant frequency above 500kHz. The value of this capacitor may be increased without limit.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.22\mu$ F for current below 10mA or  $0.1\mu$ F for currents below 1 mA.

Micrel

The MIC5203 will remain stable and in regulation with no load other than the internal voltage divider, unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

A  $0.1\mu$ F (or larger) capacitor should be placed from the MIC5203 input to ground if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

### **Enable Input**

The MIC5203 features nearly zero off-mode current. When EN (enable input) is held below 0.6V, all internal circuitry is powered off. Pulling EN high (over 2.0V) re-enables the device and allows operation. EN draws a small amount of current, typically 15 $\mu$ A. While the logic threshold is TTL/CMOS compatible, EN may be pulled as high as 20V, independent of V<sub>IN</sub>.



# **MIC5205**

150mA Low-Noise LDO Voltage Regulator

# **General Description**

The MIC5205 is an efficient linear voltage regulator with ultralow-noise output, very low dropout voltage (typically 17mV at light loads and 165mV at 150mA), and very low ground current ( $600\mu$ A at 100mA output). The MIC5205 offers better than 1% initial accuracy.

Designed especially for hand-held, battery-powered devices, the MIC5205 includes a CMOS or TTL compatible enable/ shutdown control input. When shutdown, power consumption drops nearly to zero. Regulator ground current increases only slightly in dropout, further prolonging battery life.

Key MIC5205 features include a reference bypass pin to improve its already excellent low-noise performance, reversed-battery protection, current limiting, and overtemperature shutdown.

The MIC5205 is available in fixed and adjustable output voltage versions in a small SOT-23-5 package.

## **Features**

- Ultra-low-noise output
- High output voltage accuracy
- Guaranteed 150mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Reverse-battery protection
- "Zero" off-mode current
- · Logic-controlled electronic enable

## Applications

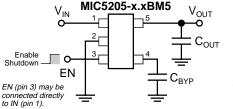
- Cellular telephones
- · Laptop, notebook, and palmtop computers
- · Battery-powered equipment
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> regulation/switching
- Consumer/personal electronics
- SMPS post-regulator/dc-to-dc modules
- High-efficiency linear power supplies

Part Number	Marking	Voltage	Accuracy	Junction Temp. Range*	Package
MIC5205BM5	LBAA	Adj	1%	-40°C to +125°C	SOT-23-5
MIC5205-2.8BM5	LB28	2.8	1%	-40°C to +125°C	SOT-23-5
MIC5205-3.0BM5	LB30	3.0	1%	-40°C to +125°C	SOT-23-5
MIC5205-3.3BM5	LB33	3.3	1%	-40°C to +125°C	SOT-23-5
MIC5205-3.6BM5	LB36	3.6	1%	-40°C to +125°C	SOT-23-5
MIC5205-3.8BM5	LB38	3.8	1%	-40°C to +125°C	SOT-23-5
MIC5205-4.0BM5	LB40	4.0	1%	-40°C to +125°C	SOT-23-5
MIC5205-5.0BM5	LB50	5.0	1%	-40°C to +125°C	SOT-23-5

Ordering Information

Other voltages available. Contact Micrel for details.

# **Typical Application**

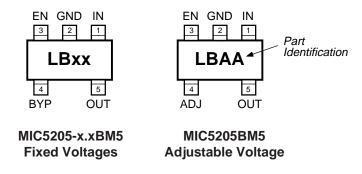


 $\begin{array}{l} \textit{Low-Noise Operation:} \\ C_{\text{BYP}} = 470 pF, \ C_{\text{OUT}} \geq 2.2 \mu F \end{array}$ 

 $\begin{array}{l} \textit{Basic Operation:} \\ C_{\text{BYP}} = not \text{ used, } C_{\text{OUT}} \geq 1 \mu F \end{array}$ 

### **Ultra-Low-Noise Regulator Application**

# **Pin Configuration**



# **Pin Description**

MIC5205-x.x (fixed)	MIC5205 (adjustable)	Pin Name	Pin Function
1	1	IN	Supply Input
2	2	GND	Ground
3	3	EN	Enable/Shutdown (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown.
4		BYP	Reference Bypass: Connect external 470pF capacitor to GND to reduce output noise. May be left open.
	4	ADJ	Adjust (Input): Adjustable regulator feedback input. Connect to resistor voltage divider.
5	5	OUT	Regulator Output

# Absolute Maximum Ratings (Note 1)

Supply Input Voltage (VIN)	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> ) Inter	nally Limited, Note 3
Lead Temperature (soldering, 5 sec.).	260°C
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Storage Temperature (T <sub>S</sub> )	–65°C to +150°C

# **Operating Ratings (Note 2)**

Input Voltage (V <sub>IN</sub> )	+2.5V to +16V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature (T)	
Thermal Resistance, SOT-23-5 ( $\theta_{IA}$ )	Note 3

## **Electrical Characteristics**

Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>O</sub>	Output Voltage Accuracy	variation from specified V <sub>OUT</sub>	-1 -2		1 <b>2</b>	% %
ΔV <sub>O</sub> /ΔT	Output Voltage Temperature Coefficient	Note 4		40		ppm/°C
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.004	0.012 <b>0.05</b>	% / V % / V
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 150mA, <b>Note 5</b>		0.02	0.2 <b>0.5</b>	% %
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage, Note 6	I <sub>L</sub> = 100μA		10	50 <b>70</b>	mV mV
		$I_L = 50 \text{mA}$		110	150 <b>230</b>	mV mV
		I <sub>L</sub> = 100mA		140	250 300	mV mV
		I <sub>L</sub> = 150mA		165	275 <b>350</b>	mV mV
I <sub>GND</sub>	Quiescent Current	$V_{EN} \le 0.4V$ (shutdown) $V_{EN} \le 0.18V$ (shutdown)		0.01	1 5	μA μA
I <sub>GND</sub>	Ground Pin Current, Note 7	$V_{EN} \ge 2.0V, I_{L} = 100 \mu A$		80	125 <b>150</b>	μΑ μΑ
		$I_L = 50 \text{mA}$		350	600 <b>800</b>	μΑ μΑ
		I <sub>L</sub> = 100mA		600	1000 <b>1500</b>	μΑ
		I <sub>L</sub> = 150mA		1300	1900 <b>2500</b>	μΑ μΑ
PSRR	Ripple Rejection	frequency = 100Hz, $I_L = 100\mu A$		75		dB
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		320	500	mA
$\Delta V_O / \Delta P_D$	Thermal Regulation	Note 8		0.05		%/W
e <sub>no</sub>	Output Noise	$I_L = 50$ mA, $C_L = 2.2\mu$ F, 470pF from BYP to GND		260		nV/√Hz

#### **ENABLE Input**

V <sub>IL</sub>	Enable Input Logic-Low Voltage	regulator shutdown			0.4 <b>0.18</b>	V V
V <sub>IH</sub>	Enable Input Logic-High Voltage	regulator enabled	2.0			V
I <sub>IL</sub> I <sub>IH</sub>	Enable Input Current	$ \begin{array}{l} V_{IL} \leq 0.4 V \\ V_{IL} \leq 0.18 V \\ V_{IH} \geq 2.0 V \\ V_{IH} \geq 2.0 V \end{array} $		0.01 5	-1 - <b>2</b> 20 <b>25</b>	μΑ μΑ μΑ μΑ

Note 1. Exceeding the absolute maximum rating may damage the device.

The device is not guaranteed to function outside its operating rating. Note 2.

The maximum allowable power dissipation at any  $T_A$  (ambient temperature) is  $P_{D(max)} = (T_{J(max)} - T_A) \div \theta_{JA}$ . Exceeding the maximum Note 3: allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The  $\theta_{JA}$  of the MIC5205xxBM5 (all versions) is 220°C/W mounted on a PC board (see "Thermal Considerations" section for further details).

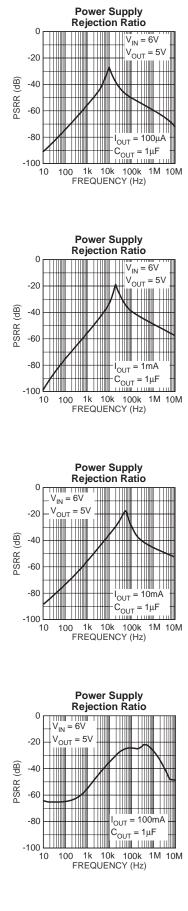
Note 4: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

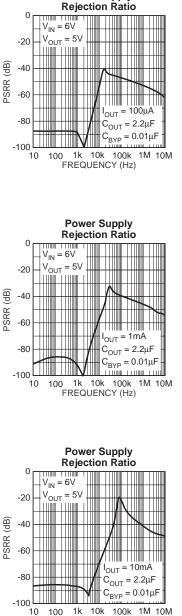
Note 5: Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 0.1mA to 150mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

Dropout Voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V Note 6: differential.

Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of Note 7: the load current plus the ground pin current.

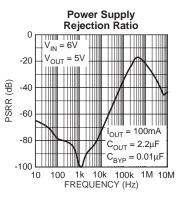
Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line Note 8: regulation effects. Specifications are for a 150mA load pulse at  $V_{IN}$  = 16V for t = 10ms.

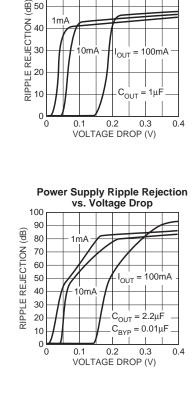




**Power Supply** 

) 100 1k 10k 100k 1M 10M FREQUENCY (Hz)

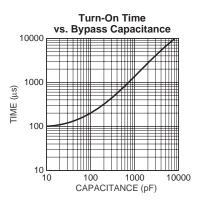


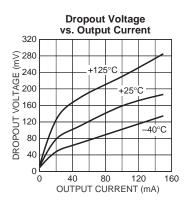


**Power Supply Ripple Rejection** 

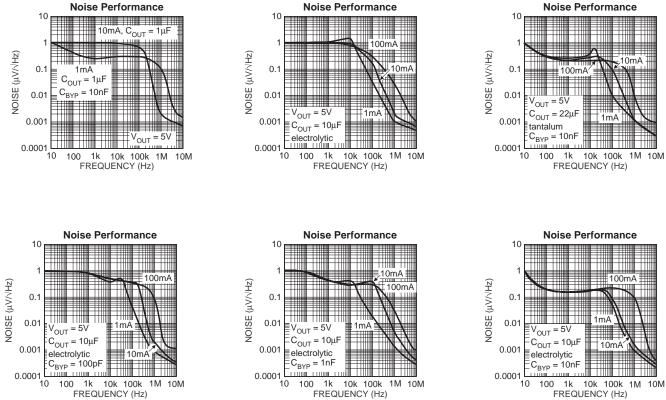
vs. Voltage Drop

60

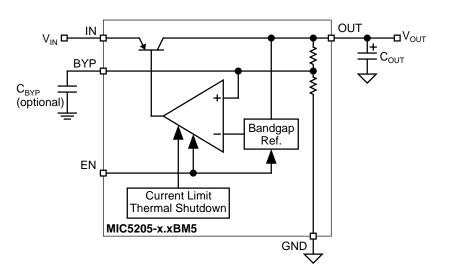




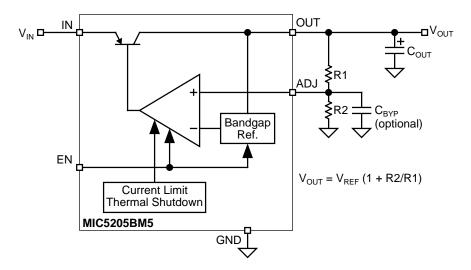
Micrel



# **Block Diagrams**







**Ultra-Low-Noise Adjustable Regulator** 

## **Applications Information**

### Enable/Shutdown

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic gates.

If the enable/shutdown feature is not required, connect EN (pin 3) to IN (supply input, pin 1). See Figure 1.

### **Input Capacitor**

A  $1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

### **Reference Bypass Capacitor**

BYP (reference bypass) is connected to the internal voltage reference. A 470pF capacitor ( $C_{BYP}$ ) connected from BYP to GND quiets this reference, providing a significant reduction in output noise.  $C_{BYP}$  reduces the regulator phase margin; when using  $C_{BYP}$ , output capacitors of 2.2µF or greater are generally required to maintain stability.

The start-up speed of the MIC5205 is inversely proportional to the size of the reference bypass capacitor. Applications requiring a slow ramp-up of output voltage should consider larger values of  $C_{\rm BYP}$ . Likewise, if rapid turn-on is necessary, consider omitting  $C_{\rm BYP}$ .

If output noise is not a major concern, omit  $\mathrm{C}_{\mathrm{BYP}}$  and leave BYP open.

### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. The minimum size of the output capacitor is dependent upon whether a reference bypass capacitor is used. 1.0 $\mu$ F minimum is recommended when C<sub>BYP</sub> is not used (see Figure 2). 2.2 $\mu$ F minimum is recommended when C<sub>BYP</sub> is 470pF (see Figure 1). Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (effective series resistance) of about  $5\Omega$  or less and a resonant frequency above 1MHz. Ultra-low-ESR capacitors can cause a low amplitude oscillation on the output and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

### No-Load Stability

The MIC5205 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

### **Thermal Considerations**

The MIC5205 is designed to provide 150mA of continuous current in a very small package. Maximum power dissipation can be calculated based on the output current and the voltage drop across the part. To determine the maximum power dissipation of the package, use the junction-to-ambient thermal resistance of the device and the following basic equation:

$$P_{D(max)} = \frac{\left(T_{J(max)} - T_{A}\right)}{\theta_{JA}}$$

 $T_{J(max)}$  is the maximum junction temperature of the die, 125°C, and  $T_A$  is the ambient operating temperature.  $\theta_{JA}$  is layout dependent; Table 1 shows examples of junction-to-ambient thermal resistance for the MIC5205.

Package	θ <sub>JA</sub> Recommended Minimum Footprint		θ <sup>JC</sup>
SOT-23-5 (M5)	220°C/W	170°C/W	130°C/W
<b>T</b> - 1, 1, -			

#### Table 1. SOT-23-5 Thermal Resistance

The actual power dissipation of the regulator circuit can be determined using the equation:

$$P_{D} = (V_{IN} - V_{OUT}) I_{OUT} + V_{IN} I_{GND}$$

Substituting  $P_{D(max)}$  for  $P_D$  and solving for the operating conditions that are critical to the application will give the maximum operating conditions for the regulator circuit. For example, when operating the MIC5205-3.3BM5 at room temperature with a minimum footprint layout, the maximum input voltage for a set output current can be determined as follows:

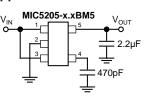
$$P_{D(max)} = \frac{(125^{\circ}C - 25^{\circ}C)}{220^{\circ}C/W}$$

 $P_{D(max)} = 455 mW$ 

The junction-to-ambient thermal resistance for the minimum footprint is  $220^{\circ}$ C/W, from Table 1. The maximum power dissipation must not be exceeded for proper operation. Using the output voltage of 3.3V and an output current of 150mA, the maximum input voltage can be determined. From the Electrical Characteristics table, the maximum ground current for 150mA output current is  $2500\mu$ A or 2.5mA.

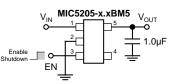
$$\begin{split} 455\text{mW} &= (\text{V}_{\text{IN}} - 3.3\text{V}) \ 150\text{mA} + \text{V}_{\text{IN}} \cdot 2.5\text{mA} \\ 455\text{mW} &= \text{V}_{\text{IN}} \cdot 150\text{mA} - 495\text{mW} + \text{V}_{\text{IN}} \cdot 2.5\text{mA} \\ 950\text{mW} &= \text{V}_{\text{IN}} \cdot 152.5\text{mA} \\ \text{V}_{\text{IN}(\text{max})} &= 6.23\text{V} \end{split}$$

Therefore, a 3.3V application at 150mA of output current can accept a maximum input voltage of 6.2V in a SOT-23-5 package. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to the Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.



## Figure 1. Ultra-Low-Noise Fixed Voltage Application

Figure 1 includes a 470pF capacitor for low-noise operation and shows EN (pin 3) connected to IN (pin 1) for an application where enable/shutdown is not required.  $C_{OUT} = 2.2 \mu F$  minimum.



## Figure 2. Low-Noise Fixed Voltage Application

Figure 2 is an example of a low-noise configuration where  $C_{BYP}$  is not required.  $C_{OUT} = 1\mu F$  minimum.

## **Adjustable Regulator Applications**

The MIC5205BM5 can be adjusted to a specific output voltage by using two external resistors (Figure 3). The resistors set the output voltage based on the following equation:

$$V_{OUT}~=~1.242V~\times \left(\frac{R2}{R1}~+~1\right)$$

This equation is correct due to the configuration of the bandgap reference. The bandgap voltage is relative to the output, as seen in the block diagram. Traditional regulators normally have the reference voltage relative to ground and have a different  $V_{OUT}$  equation.

Resistor values are not critical because ADJ (adjust) has a high input impedance, but for best results use resistors of  $470k\Omega$  or less. A capacitor from ADJ to ground provides greatly improved noise performance.

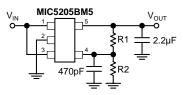


Figure 3. Ultra-Low-Noise Adjustable Voltage Application

Figure 3 includes the optional 470pF noise bypass capacitor from ADJ to GND to reduce output noise.

### **Dual-Supply Operation**

When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.



# **MIC5206**

### 150mA Low-Noise LDO Voltage Regulator

## **General Description**

The MIC5206 is an efficient linear voltage regulator with very low dropout voltage (typically 17mV at light loads and 165mV at 150mA), and very low ground current (600µA at 100mA output), with better than 1% initial accuracy. It has a logic compatible enable/shutdown control input and an internal undervoltage monitor.

Designed especially for hand-held, battery-powered devices, the MIC5206 can be switched by a CMOS or TTL compatible logic signal. When disabled, power consumption drops nearly to zero. Dropout ground current is minimized to prolong battery life.

Key features include an undervoltage monitor with an error flag output, a reference bypass pin to improve its already lownoise performance (8-lead versions only), reversed-battery protection, current limiting, and overtemperature shutdown.

The MIC5206 is available in several fixed voltages in a tiny SOT-23-5 package. It features a pinout, similar to the LP2980, but has significantly better performance. Fixed and adjustable output voltage versions, featuring the reference bypass option, are available in the 8-lead Micrel Mini 8<sup>™</sup> 8-lead MSOP (micro small-outline package).

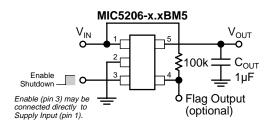
## **Features**

- · Error flag indicates undervoltage fault
- High output voltage accuracy
- Guaranteed 150mA output
- Ultra-low-noise output (8-lead versions)
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Reversed-battery protection
- "Zero" off-mode current
- Logic-controlled electronic enable

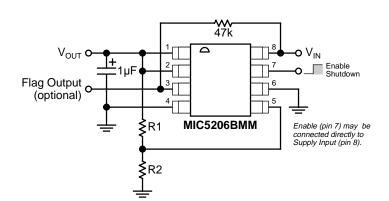
## Applications

- Cellular telephones
- · Laptop, notebook, and palmtop computers
- Battery-powered equipment
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> regulation/switching
- Consumer/personal electronics
- SMPS post-regulator/dc-to-dc modules
- · High-efficiency linear power supplies

# **Typical Applications**



**SOT-23-5 Fixed Voltage Application** 



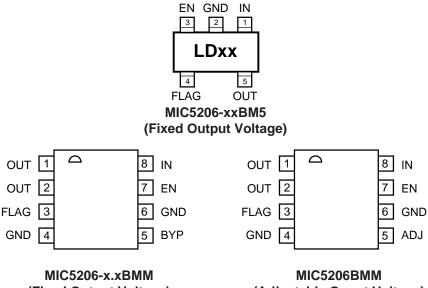
Adjustable Voltage Application

# **Ordering Information**

Part Number	Marking	Volts	Accuracy	Junction Temp. Range	Package
MIC5206-2.5BM5	LD25	2.5	1%	-40°C to +125°C	SOT-23-5
MIC5206-3.0BM5	LD30	3.0	1%	–40°C to +125°C	SOT-23-5
MIC5206-3.2BM5	LD32	3.2	1%	–40°C to +125°C	SOT-23-5
MIC5206-3.3BM5	LD33	3.3	1%	–40°C to +125°C	SOT-23-5
MIC5206-3.6BM5	LD36	3.6	1%	-40°C to +125°C	SOT-23-5
MIC5206-3.8BM5	LD38	3.8	1%	-40°C to +125°C	SOT-23-5
MIC5206-4.0BM5	LD40	4.0	1%	-40°C to +125°C	SOT-23-5
MIC5206-5.0BM5	LD50	5.0	1%	-40°C to +125°C	SOT-23-5
MIC5206BMM	—	Adj	1%	–40°C to +125°C	8-lead MSOP
MIC5206-3.0BMM	_	3.0	1%	-40°C to +125°C	8-lead MSOP
MIC5206-3.3BMM	_	3.3	1%	-40°C to +125°C	8-lead MSOP
MIC5206-3.6BMM	_	3.6	1%	-40°C to +125°C	8-lead MSOP
MIC5206-3.8BMM	_	3.8	1%	-40°C to +125°C	8-lead MSOP
MIC5206-4.0BMM	_	4.0	1%	-40°C to +125°C	8-lead MSOP
MIC5206-5.0BMM	_	5.0	1%	-40°C to +125°C	8-lead MSOP

Other voltages available. Contact Micrel for details.

# **Pin Configuration**



(Fixed Output Voltage)

(Adjustable Ouput Voltage)

# **Pin Description**

MIC5206 SOT-23-5	MIC5206 MSOP-8	Pin Name	Pin Function
1	8	IN	Supply Input
2	4, 6	GND	Ground
3	7	EN	Enable/Shutdown (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown. Do not leave floating.
4	3	FLAG	Error Flag (Output): Open-collector output. Active low indicates an ouput undervoltage condition.
	5 (fixed)	BYP	Reference Bypass: Connect external 470pF capacitor to GND to reduce output noise. May be left open.
	5 (adj.)	ADJ	Adjust (Input): Adjustable regulator feedback input. Connect to resistor voltage divider.
5	1,2	OUT	Regulator Output

## Absolute Maximum Ratings (Note 1)

## 

Lead Temperature (Soldering, 5 sec.) ...... 260°C

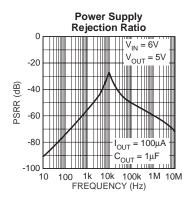
# **Operating Ratings (Note 2)**

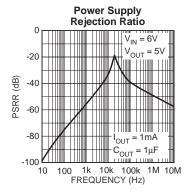
Supply Input Voltage (VIN)	+2.5V to +16V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature (T <sub>J</sub> )	-40°C to +125°C
SOT-23-5 (θ <sub>JA</sub> )	Note 3
8-lead MSOP (θ <sub>JA</sub> )	Note 3

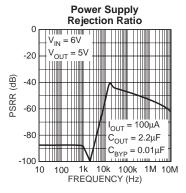
# **Electrical Characteristics**

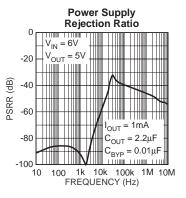
Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>O</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-1 -2		1 <b>2</b>	% %
$\Delta V_{O} / \Delta T$	Output Voltage Temperature Coefficient	Note 4		40		ppm/°C
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.004	0.012	%/V
$\Delta V_O/V_O$	Load Regulation	I <sub>L</sub> = 0.1mA to 150mA, <b>Note 5</b>		0.02	0.2	%
$\overline{V_{IN} - V_O}$	Dropout Voltage, Note 6	I <sub>L</sub> = 100μA		17	50	mV
		I <sub>L</sub> = 50mA		110	<b>70</b> 150 <b>230</b>	mV mV mV
		I <sub>L</sub> = 100mA		140	250 250 <b>300</b>	mV mV
		I <sub>L</sub> = 150mA		165	275 <b>350</b>	mV mV
I <sub>GND</sub>	Quiescent Current	$V_{EN} \le 0.4V$ (shutdown) $V_{EN} \le 0.18V$ (shutdown)		0.01	1 5	μΑ μΑ
I <sub>GND</sub>	Ground Pin Current, Note 7	$V_{EN} \ge 2.0V, I_{L} = 100\mu A$		80	125	μA
		I <sub>L</sub> = 50mA		350	<b>150</b> 600 <b>800</b>	μΑ μΑ μΑ
		I <sub>L</sub> = 100mA		600	1000 <b>1500</b>	μΑ μΑ μΑ
		I <sub>L</sub> = 150mA		1300	1900 <b>2500</b>	μΑ μΑ
PSRR	Ripple Rejection			75		dB
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		320	500	mA
$\Delta V_O / \Delta P_D$	Thermal Regulation	Note 8		0.05		%/W
e <sub>no</sub>	Output Noise	$I_L = 50$ mA, $C_L = 4.7\mu$ F, 470pF from BYP to GND (MM package only)		260		nV√Hz
Enable Inpu	it	·	•			
V <sub>IL</sub>	Enable Input Logic-Low Voltage	regulator shutdown			0.4 <b>0.18</b>	V V
V <sub>IH</sub>	Enable Input Logic-High Voltage	regulator enabled	2.0			V
IIL	Enable Input Current	$V_{IL} \le 0.4V$ $V_{II} \le 0.18V$		0.01	-1 -2	μΑ μΑ
I <sub>IH</sub>		$V_{IH}^{IL} \ge 2.0V$ $V_{IH} \ge 2.0V$		5	20 <b>25</b>	μΑ μΑ
Error Flag C	Dutput					
V <sub>ERR</sub>	Flag Threshold	undervoltage condition (below nominal)		-5	-8	%
V <sub>OL</sub>	Output Logic-Low Voltage	I <sub>L</sub> = 1mA, undervoltage condition		0.2	0.4	V
I <sub>FL</sub>	Flag Leakage Current	flag off, $V_{FLAG} = 0V$ to 16V	-1	0.1	+1	μA
	5: Data Sheets	233 D	esigning	With LD	O Regu	lators

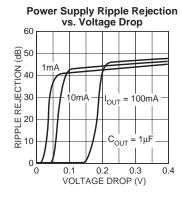
- Note 1: Exceeding the absolute maximum rating may damage the device.
- Note 2. The device is not guaranteed to function outside its operating rating.
- **Note 3:** The maximum allowable power dissipation at any  $T_A$  (ambient temperature) is  $P_{D(max)} = (T_{J(max)} T_A) \div \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The  $\theta_{JA}$  of the MIC5205-x.xBM5 (all versions) is 220°C/W, and the MIC5206-x.xBMM (all versions) is 200°C/W, mounted on a PC board (see "Thermal Considerations" for further details).
- Note 4: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.
- **Note 5:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 0.1mA to 150mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.
- Note 6: Dropout Voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.
- Note 7: Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.
- Note 8: Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 150mA load pulse at  $V_{IN} = 16V$  for t = 10ms.

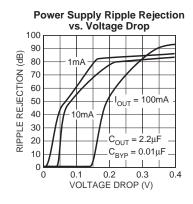


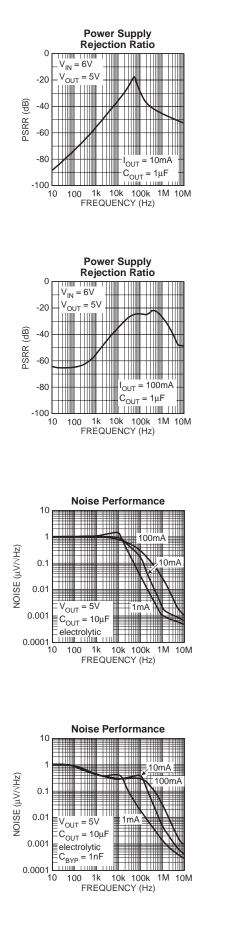


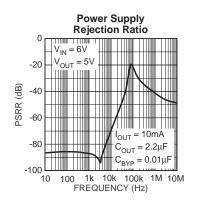


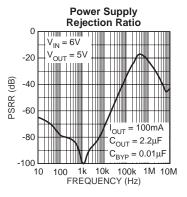


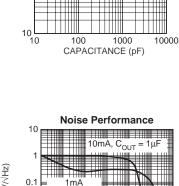












Turn-On Time

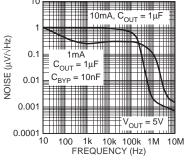
vs. Bypass Capacitance

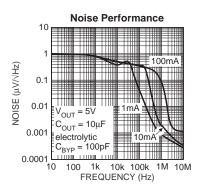
10000

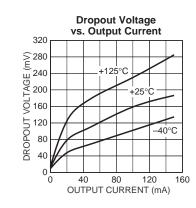
(รก) 1000

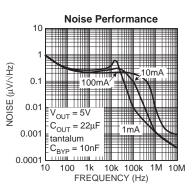
100

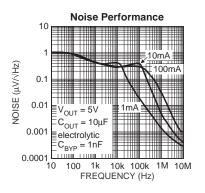
TIME (











# **Applications Information**

## Enable/Shutdown

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic gates.

If the enable/shutdown feature is not required, connect EN (enable) to IN (supply input). Refer to the text with Figures 1a and 2.

## **Input Capacitor**

A 1 $\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

## **Reference Bypass Capacitor**

BYP (reference bypass) is connected to the internal voltage reference. A 470pF capacitor ( $C_{BYP}$ ) connected from BYP to GND quiets this reference, providing a significant reduction in output noise. See Figure 2.  $C_{BYP}$  reduces the regulator phase margin; when using  $C_{BYP}$ , output capacitors of 2.2µF or greater are generally required to maintain stability.

The start-up speed of the MIC5206 is inversely proportional to the size of the reference bypass capacitor. Applications requiring a slow ramp-up of output voltage should consider larger values of C<sub>BYP</sub>. Likewise, if rapid turn-on is necessary, consider omitting C<sub>BYP</sub>.

If output noise is not a major concern, omit  $\mathrm{C}_{\mathrm{BYP}}$  and leave BYP open.

## **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. The minimum size of the output capacitor is dependent upon whether a reference bypass capacitor is used. 1.0µF minimum is recommended when C<sub>BYP</sub> is not used (see Figure 2). 2.2µF minimum is recommended when C<sub>BYP</sub> is 470pF (see Figure 2). Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (effective series resistance) of about  $5\Omega$  or less and a resonant frequency above 1MHz. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

## **No-Load Stability**

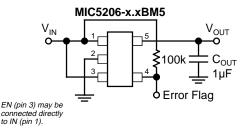
The MIC5205 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

## **Error Flag Ouput**

The error flag is an open-collector output and is active (low) when an undervoltage of approximately 5% below the nominal output voltage is detected. A pullup resistor from IN to FLAG is shown in all schematics.

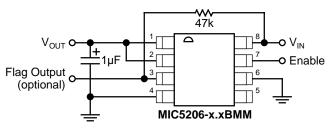
If an error indication is not required, FLAG may be left open and the pullup resistor may be omitted.

## **Fixed Regulator Applications**



## Figure 1a. Low-Noise Fixed Voltage Application

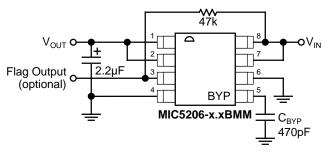
EN (pin 3) is shown connected to IN (pin 1) for an application where enable/shutdown is not required. The error flag is shown with a  $100k\Omega$  pullup resistor.



## Figure 1b. Low-Noise Fixed Voltage Application

Figure 1b is an example of a basic configuration where the lowest-noise operation is not required.  $C_{OUT} = 1\mu F$  minimum. The error flag is shown with a  $47k\Omega$  pullup resistor.

**Ultra-Low-Noise Application** 



## Figure 2. Ultra-Low-Noise Fixed Voltage Application

Figure 2 includes a  $470\mu$ F capacitor for low-noise operation and shows EN (pin 7) connected to IN (pin 8) for an application where enable/shutdown is not required. The error flag is shown with a  $47k\Omega$  pullup resistor.

## Adjustable Regulator Applications

Figure 3 shows the MIC5206BMM adjustable output voltage configuration. Two resistors set the output voltage. The formula for output voltage is:

$$V_{OUT} = 1.242V \times \left(\frac{R2}{R1} + 1\right)$$

Resistor values are not critical because ADJ (adjust) has a high input impedance, but for best results use resistors of  $470k\Omega$  or less. A capacitor from ADJ to ground provides greatly improved noise performance.

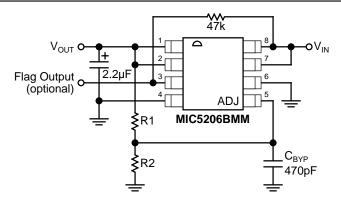


Figure 3. Ultra-Low-Noise Adjustable Voltage Application

Figure 3 also includes a 470pF capacitor for lowest-noise operation and shows EN (pin 7) connected to IN (pin 8) for an application where enable/shutdown is not required.  $C_{OUT} = 2.2\mu$ F minimum. The error flag is shown with a 47k $\Omega$  pullup resistor.

### **Thermal Considerations**

### Layout

The MIC5206-x.xBM5 (5-lead SOT-23 package) has the following thermal characteristics when mounted on a single layer copper-clad printed circuit board.

Multilayer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

PC Board Dielectric	$\theta_{JA}$
FR4	220°C/W
Ceramic	200°C/W

**SOT-23-5 Thermal Characteristics** 

The "worst case" value of 220°C/W assumes no ground plane, minimum trace widths, and a FR4 material board.

The MIC5206-xxBMM (8-lead MSOP) has a thermal resistance of 200°C/W when mounted on a FR4 board with minimum trace widths and no ground plane.

PC Board Dielectric	$\theta_{JA}$
FR4	200°C

**MSOP** Thermal Characteristics

### Nominal Power Dissipation and Die Temperature

The MIC5206-x.xBM5 at a 25°C ambient temperature will operate reliably at over 450mW power dissipation when mounted in the "worst case" manner described above. At an ambient temperature of 40°C, the device may safely dissipate over 380mW. These power levels are equivalent to a die temperature of 125°C, the maximum operating junction temperature for the MIC5206.

For additional heat sink characteristics, please refer to Micrel Application Hint 17, "Calculating P.C. Board Heat Sink Area For Surface Mount Packages".



# **MIC5207**

180mA Low-Noise LDO Voltage Regulator

# **General Description**

The MIC5207 is an efficient linear voltage regulator with ultralow-noise output, very low dropout voltage (typically 17mV at light loads and 165mV at 150mA), and very low ground current (720 $\mu$ A at 100mA output). The MIC5207 offers better than 3% initial accuracy.

Designed especially for hand-held, battery-powered devices, the MIC5207 includes a CMOS or TTL compatible enable/ shutdown control input. When shutdown, power consumption drops nearly to zero.

Key MIC5207 features include a reference bypass pin to improve its already low-noise performance, reversed-battery protection, current limiting, and overtemperature shutdown.

The MIC5207 is available in fixed and adjustable output voltage versions in a small SOT-23-5 package. TO-92 and 8-pin packages also available. Contact Micrel for details.

## Features

- Ultra-low-noise output
- High output voltage accuracy
- Guaranteed 180mA output
- Low quiescent current
- Low dropout voltage
- Extremely tight load and line regulation
- Very low temperature coefficient
- Current and thermal limiting
- Reverse-battery protection
- "Zero" off-mode current
- Logic-controlled electronic enable

## Applications

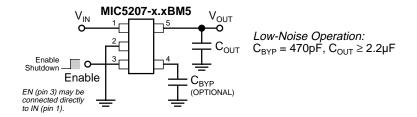
- · Cellular telephones
- Laptop, notebook, and palmtop computers
- Battery-powered equipment
- PCMCIA V<sub>CC</sub> and V<sub>PP</sub> regulation/switching
- Consumer/personal electronics
- SMPS post-regulator/dc-to-dc modules
- High-efficiency linear power supplies

## Ordering Information

Part Number*	Marking	Voltage	Junction Temp. Range	Package
MIC5207BM5	LEAA	Adj	–40°C to +125°C	SOT-23-5
MIC5207-1.8BM5	LE18	1.8	–40°C to +125°C	SOT-23-5
MIC5207-2.5BM5	LE25	2.5	–40°C to +125°C	SOT-23-5
MIC5207-3.0BM5	LE30	3.0	–40°C to +125°C	SOT-23-5
MIC5207-3.3BM5	LE33	3.3	–40°C to +125°C	SOT-23-5
MIC5207-3.6BM5	LE36	3.6	–40°C to +125°C	SOT-23-5
MIC5207-3.8BM5	LE38	3.8	–40°C to +125°C	SOT-23-5
MIC5207-4.0BM5	LE40	4.0	–40°C to +125°C	SOT-23-5
MIC5207-5.0BM5	LE50	5.0	–40°C to +125°C	SOT-23-5
MIC5207-3.3BZ	_	3.3	–40°C to +125°C	TO-92

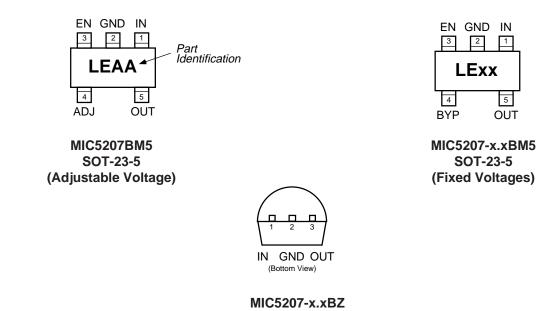
Other voltages and DIP packages available. Contact Micrel Marketing for information.

# **Typical Application**





# **Pin Configuration**



**Pin Description** 

Pin No. SOT-23-5	Pin No. TO-92	Pin Name	Pin Function
1	1	IN	Supply Input
2	2	GND	Ground
3		EN	Enable/Shutdown (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown.
4 (fix)		BYP	Reference Bypass: Connect external 470pF capacitor to GND to reduce output noise. May be left open. For 1.8V or 2.5V operation, see "Applications Information."
4 (adj)		ADJ	Adjust (Input): Adjustable regulator feedback input. Connect to resistor voltage divider.
5	3	OUT	Regulator Output

TO-92 (Fixed Voltages)

## Absolute Maximum Ratings (Note 1)

Supply Input Voltage (VIN)	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> ) Inter	nally Limited, Note 3
Lead Temperature (soldering, 5 sec.).	260°C
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Storage Temperature (T <sub>S</sub> )	–65°C to +150°C

# **Operating Ratings (Note 2)**

Input Voltage (V <sub>IN</sub> )	+2.5V to +16V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature $(\overline{T_{I}})$	–40°C to +125°C
Thermal Resistance (θ <sub>JA</sub> )	Note 3

## **Electrical Characteristics**

$V_{IN} = V_{OUT} + 1V$ : $I_{I} = 100 \mu$ A: 0	$V_{FN} = 1.0 \mu F; V_{FN} \ge 2.0 V; T_{FN}$	= 25°C, <b>bold</b> values indicate	$-40^{\circ}C \le T_{,l} \le +125^{\circ}C$ ; unless noted.
	· · · · · · · · · · · · · · · · · · ·		

Symbol	Parameter	Conditions	Min	Typical	Мах	Units
V <sub>O</sub>	Output Voltage Accuracy	variation from specified V <sub>OUT</sub>	-3 -4		3 <b>4</b>	% %
ΔV <sub>O</sub> /ΔT	Output Voltage Temperature Coefficient	Note 4		40		ppm/°C
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.005	0.05 <b>0.10</b>	%/V %/V
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 150mA, <b>Note 5</b>		0.05	0.5 <b>0.7</b>	% %
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage, Note 6	I <sub>L</sub> = 100μA		17	60 <b>80</b>	mV mV
		$I_L = 50 \text{mA}$		115	175 <b>250</b>	mV mV
		I <sub>L</sub> = 100mA		140	280 <b>325</b>	mV mV
		I <sub>L</sub> = 150mA		165	300 <b>400</b>	mV mV
I <sub>GND</sub>	Quiescent Current	$V_{EN} \le 0.4V$ (shutdown) $V_{EN} \le 0.18V$ (shutdown)		0.01	1 5	μΑ μΑ
I <sub>GND</sub>	Ground Pin Current, Note 7	$V_{EN} \ge 2.0V, I_{L} = 100\mu A$		80	130 <b>170</b>	μΑ μΑ
		$I_L = 50 \text{mA}$		350	650 <b>900</b>	μA μA
		I <sub>L</sub> = 100mA		720	1100 <b>2000</b>	μA μA
		I <sub>L</sub> = 150mA		1800	2500 <b>3000</b>	μΑ μΑ
PSRR	Ripple Rejection			75		dB
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		320	500	mA
$\Delta V_{O} / \Delta P_{D}$	Thermal Regulation	Note 8		0.05		%/W
e <sub>no</sub>	Output Noise	$I_L = 50$ mA, $C_L = 2.2\mu$ F, 470pF from BYP to GND		260		nV√Hz

#### **ENABLE** Input

V <sub>IL</sub>	Enable Input Logic-Low Voltage	regulator shutdown			0.4 <b>0.18</b>	V V
V <sub>IH</sub>	Enable Input Logic-High Voltage	regulator enabled	2.0			V
I	Enable Input Current	$V_{IL} \le 0.4V$ $V_{IL} \le 0.18V$		0.01	-1 - <b>2</b>	μΑ μΑ
IIH		$V_{IH} \ge 2.0V$ $V_{IH} \ge 2.0V$		5	20 <b>25</b>	μΑ μΑ

Note 1. Exceeding the absolute maximum rating may damage the device.

Note 2. The device is not guaranteed to function outside its operating rating.

**Note 3:** The maximum allowable power dissipation at any  $T_A$  (ambient temperature) is  $P_{D(max)} = (T_{J(max)} - T_A) \div \theta_{JA}$ . Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. The  $\theta_{JA}$  of the SOT-23-5 (M5) is 220°C/W and the TO-92 (Z) is 180°C/W (0.4" leads) or 160°C/W (0.25" leads) soldered to a PC board. See "Thermal Considerations."

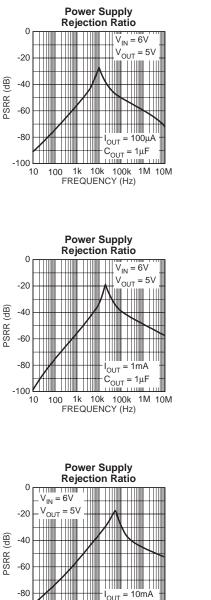
Note 4: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

**Note 5:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 0.1mA to 180mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

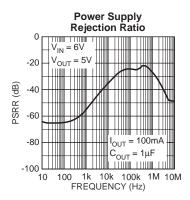
Note 6: Dropout voltage is the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

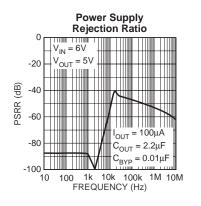
**Note 7:** Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

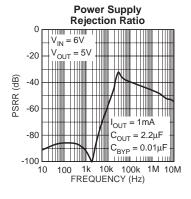
**Note 8:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 180mA load pulse at  $V_{IN} = 16V$  for t = 10ms.



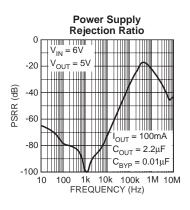
-100 10 100 1k 10k 100k 1M 10M FREQUENCY (Hz)

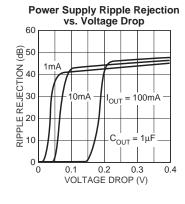


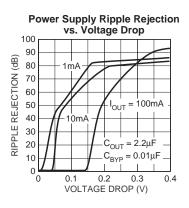


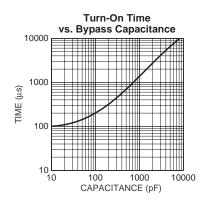


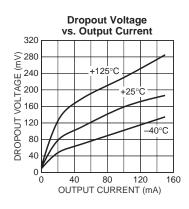
Power Supply Rejection Ratio  $V_{IN} = 6V$  $V_{OUT} = 5V$  $V_{OUT} = 5V$  $C_{OUT} = 10mA$  $C_{OUT} = 2.2\mu F$  $C_{BYP} = 0.01\mu F$ 100 100 1k 10k 100k 1M 10M FREQUENCY (Hz)



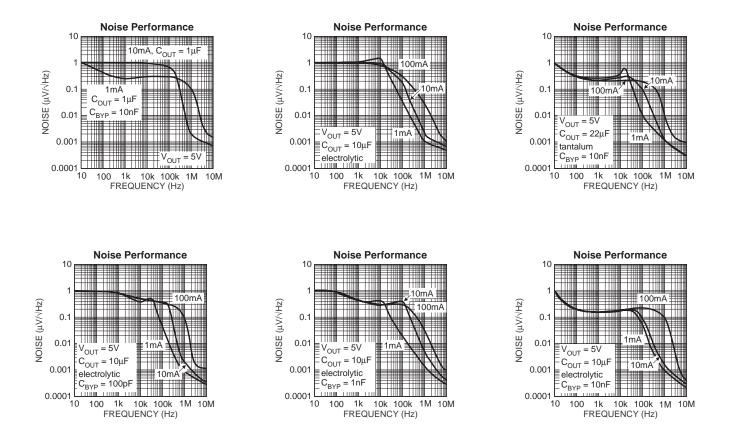




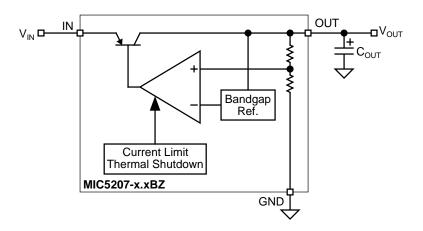




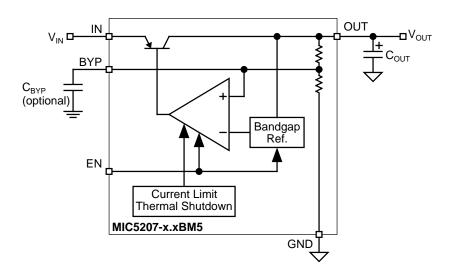




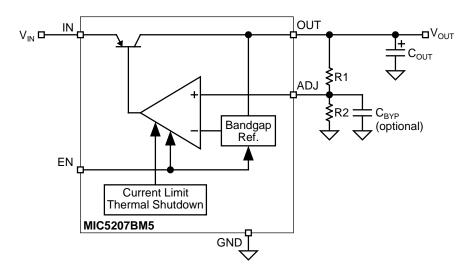
# **Block Diagrams**



Low-Noise Fixed Regulator (TO-92 version only)







**Ultra-Low-Noise Adjustable Regulator** 

## **Applications Information**

### Enable/Shutdown

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic gates.

If the enable/shutdown feature is not required, connect EN (pin 3) to IN (supply input, pin 1). See Figure 1.

### **Input Capacitor**

A  $1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

### **Reference Bypass Capacitor**

BYP (reference bypass) is connected to the internal voltage reference. A 470pF capacitor ( $C_{BYP}$ ) connected from BYP to GND quiets this reference, providing a significant reduction in output noise.  $C_{BYP}$  reduces the regulator phase margin; when using  $C_{BYP}$ , output capacitors of 2.2µF or greater are generally required to maintain stability.

The start-up speed of the MIC5207 is inversely proportional to the size of the reference bypass capacitor. Applications requiring a slow ramp-up of output voltage should consider larger values of  $C_{BYP}$ . Likewise, if rapid turn-on is necessary, consider omitting  $C_{BYP}$ .

If output noise is not a major concern, omit  $\mathrm{C}_{\mathrm{BYP}}$  and leave BYP open.

### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. The minimum size of the output capacitor is dependent upon whether a reference bypass capacitor is used. 1.0 $\mu$ F minimum is recommended when C<sub>BYP</sub> is not used (see Figure 2). 2.2 $\mu$ F minimum is recommended when C<sub>BYP</sub> is 470pF (see Figure 1). Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (effective series resistance) of about 5 $\Omega$  or less and a resonant frequency above 1MHz. Ultra-low-ESR capacitors can cause a low amplitude oscillation on the output and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

### **No-Load Stability**

The MIC5207 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

### **Thermal Considerations**

The MIC5207 is designed to provide 180mA of continuous current in a very small package. Maximum power dissipation can be calculated based on the output current and the voltage

drop across the part. To determine the maximum power dissipation of the package, use the junction-to-ambient thermal resistance of the device and the following basic equation:

$$P_{D(max)} = \frac{\left(T_{J(max)} - T_{A}\right)}{\theta_{JA}}$$

 $T_{J(max)}$  is the maximum junction temperature of the die, 125°C, and  $T_A$  is the ambient operating temperature.  $\theta_{JA}$  is layout dependent; Table 1 shows examples of junction-to-ambient thermal resistance for the MIC5207.

Package	θ <sub>JA</sub> Recommended Minimum Footprint	θ <sub>JA</sub> 1" Square Copper Clad	θ <sup>JC</sup>
SOT-23-5 (M5)	220°C/W	170°C/W	130°C/W

#### Table 1. SOT-23-5 Thermal Resistance

The actual power dissipation of the regulator circuit can be determined using the equation:

$$P_{D} = (V_{IN} - V_{OUT}) I_{OUT} + V_{IN} I_{GND}$$

Substituting  $P_{D(max)}$  for  $P_D$  and solving for the operating conditions that are critical to the application will give the maximum operating conditions for the regulator circuit. For example, when operating the MIC5207-3.3BM5 at room temperature with a minimum footprint layout, the maximum input voltage for a set output current can be determined as follows:

$$P_{D(max)} = \frac{(125^{\circ}C - 25^{\circ}C)}{220^{\circ}C/W}$$

$$P_{D(max)} = 455 mW$$

The junction-to-ambient thermal resistance for the minimum footprint is 220°C/W, from Table 1. The maximum power dissipation must not be exceeded for proper operation. Using the output voltage of 3.3V and an output current of 150mA, the maximum input voltage can be determined. From the Electrical Characteristics table, the maximum ground current for 150mA output current is 3000µA or 3mA.

$$\begin{split} 455\text{mW} &= (\text{V}_{\text{IN}} - 3.3\text{V}) \ 150\text{mA} + \text{V}_{\text{IN}} \cdot 3\text{mA} \\ 455\text{mW} &= \text{V}_{\text{IN}} \cdot 150\text{mA} - 495\text{mW} + \text{V}_{\text{IN}} \cdot 3\text{mA} \\ 950\text{mW} &= \text{V}_{\text{IN}} \cdot 153\text{mA} \\ \text{V}_{\text{IN}(\text{max})} &= 6.21\text{V} \end{split}$$

Therefore, a 3.3V application at 150mA of output current can accept a maximum input voltage of 6.2V in a SOT-23-5 package. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to the Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.

### Low-Voltage Operation

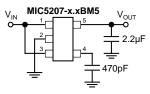
The MIC5207-1.8 and MIC5207-2.5 require special consideration when used in voltage-sensitive systems. They may momentarily overshoot their nominal output voltages unless appropriate output and bypass capacitor values are chosen.

During regulator power up, the pass transistor is fully saturated for a short time, while the error amplifier and voltage reference are being powered up more slowly from the output (see "Block Diagram"). Selecting larger output and bypass capacitors allows additional time for the error amplifier and reference to turn on and prevent overshoot.

To ensure that no overshoot is present when starting up into a light load (100 $\mu$ A), use a 4.7 $\mu$ F output capacitance and 470pF bypass capacitance. This slows the turn-on enough to allow the regulator to react and keep the output voltage from exceeding its nominal value. At heavier loads, use a 10 $\mu$ F output capacitance and 470pF bypass capacitance. Lower values of output and bypass capacitance can be used, depending on the sensitivity of the system.

Applications that can withstand some overshoot on the output of the regulator can reduce the output capacitor and/ or reduce or eliminate the bypass capacitor. Applications that are not sensitive to overshoot due to power-on reset delays can use normal output and bypass capacitor configurations.

### **Fixed Regulator Applications**



### Figure 1. Ultra-Low-Noise Fixed Voltage Regulator

Figure 1 includes a 470pF capacitor for ultra-low-noise operation and shows EN (pin 3) connected to IN (pin 1) for an application where enable/shutdown is not required.  $C_{OUT} = 2.2\mu$ F minimum.

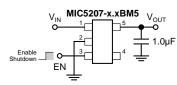


Figure 2. Low-Noise Fixed Voltage Regulator

Figure 2 is an example of a basic low-noise configuration.  $C_{OUT} = 1\mu F$  minimum.

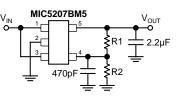
### Adjustable Regulator Applications

The MIC5207BM5 can be adjusted to a specific output voltage by using two external resistors (figure 3). The resistors set the output voltage based on the following equation:

$$V_{OUT} = V_{REF} \left( 1 + \frac{R2}{R1} \right)$$

This equation is correct due to the configuration of the bandgap reference. The bandgap voltage is relative to the output, as seen in the block diagram. Traditional regulators normally have the reference voltage relative to ground; therefore, their equations are different from the equation for the MIC5207BM5.

Resistor values are not critical because ADJ (adjust) has a high input impedance, but for best results use resistors of  $470k\Omega$  or less. A capacitor from ADJ to ground provides greatly improved noise performance.



### Figure 3. Ultra-Low-Noise Adjustable Voltage Regulator

Figure 3 includes the optional 470pF noise bypass capacitor from ADJ to GND to reduce output noise.

### **Dual-Supply Operation**

When used in dual-supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

### **USB** Application

Figure 4 shows the MIC5207-3.3BZ (3-terminal, TO-92) in a USB application. Since the V<sub>BUS</sub> supply may be greater than 10 inches from the regulator, a  $1\mu$ F input capacitor is included.

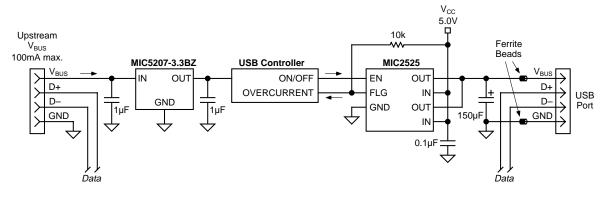


Figure 4. Single-Port Self-Powered Hub



# **MIC5208**

# **Dual 50mA LDO Voltage Regulator**

## **Preliminary Information**

# **General Description**

The MIC5208 is a dual linear voltage regulator with very low dropout voltage (typically 20mV at light loads and 250mV at 50mA), very low ground current ( $225\mu$ A at 10mA output), and better than 3% initial accuracy. It also features individual logic-compatible enable/shutdown control inputs.

Designed especially for hand-held battery powered devices, the MIC5208 can be switched by a CMOS or TTL compatible logic signal, or the enable pin can be connected to the supply input for 3-terminal operation. When disabled, power consumption drops nearly to zero. Dropout ground current is minimized to prolong battery life.

Key features include current limiting, overtemperature shutdown, and protection against reversed battery.

The MIC5208 is available in 3.0V, 3.3V, 3.6V, 4.0V and 5.0V fixed voltage configurations. Other voltages are available; contact Micrel for details.

## **Features**

- Micrel Mini 8™ MSOP package
- Guaranteed 50mA output
- Low quiescent current
- Low dropout voltage
- Wide selection of output voltages
- Tight load and line regulation
- Low temperature coefficient
- Current and thermal limiting
- Reversed input polarity protection
- Zero off-mode current
- Logic-controlled electronic enable

# Applications

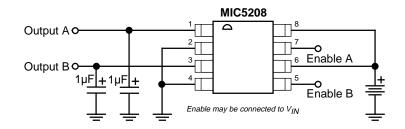
- Cellular telephones
- Laptop, notebook, and palmtop computers
- Battery powered equipment
- Bar code scanners
- SMPS post regulator/dc-to-dc modules
- High-efficiency linear power supplies

## Ordering Information

Part Number	Voltage	Accuracy	Junction Temp. Range*	Package
MIC5208-3.0BMM	3.0	3%	–40°C to +125°C	8-lead MSOP
MIC5208-3.3BMM	3.3	3%	–40°C to +125°C	8-lead MSOP
MIC5208-3.6BMM	3.6	3%	–40°C to +125°C	8-lead MSOP
MIC5208-4.0BMM	4.0	3%	–40°C to +125°C	8-lead MSOP
MIC5208-5.0BMM	5.0	3%	–40°C to +125°C	8-lead MSOP

Other voltages available. Contact Micrel for details.

# **Typical Application**



# **Pin Configuration**

### MIC5208BMM

# **Pin Description**

Pin Number	Pin Name	Pin Function
1	OUTA	Regulator Output A
2, 4	GND	Ground: Both pins must be connected together.
3	OUTB	Regulator Output B
5	ENB	Enable/Shutdown B (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown. Do not leave floating.
6	INB	Supply Input B
7	ENA	Enable/Shutdown A (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown. Do not leave floating.
8	INA	Supply Input A

## **Absolute Maximum Ratings**

Supply Input Voltage (VIN)	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited
Storage Temperature Range	–60°C to +150°C
Lead Temperature (soldering, 5 sec.)	260°C

## **Recommended Operating Conditions**

Supply Input Voltage (VIN)	2.5V to 16V
Enable Input Voltage (V <sub>EN</sub> )	0V to 16V
Junction Temperature (T <sub>J</sub> )	40°C to +125°C
8-lead MSOP (θ <sub>JA</sub> )	Note 1

# **Electrical Characteristics**

 $V_{IN} = V_{OUT} + 1V$ ;  $I_L = 1mA$ ;  $C_L = 1\mu F$ , and  $V_{EN} \ge 2.0V$ ;  $T_J = 25^{\circ}C$ , **bold** values indicate  $-40^{\circ}C$  to  $+125^{\circ}C$ ; for one-half of dual MIC5208; unless noted.

Symbol	Parameter	Conditions	Min	Typical	Мах	Units
V <sub>O</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-3 -4		3 <b>4</b>	% %
$\Delta V_{O} / \Delta T$	Output Voltage Temperature Coeffcient	Note 2		50	200	ppm/°C
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.008	0.3 <b>0.5</b>	% %
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 50mA, <b>Note 3</b>		0.08	0.3 <b>0.5</b>	% %
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage, Note 4	$I_{L} = 100\mu A$ $I_{L} = 20m A$ $I_{L} = 50m A$		20 200 250	350 500	mV mV mV
Ι <sub>Q</sub>	Quiescent Current	V <sub>EN</sub> ≤ 0.4V (shutdown)		0.01	10	μA
I <sub>GND</sub>	Ground Pin Current Note 5	$V_{EN} \ge 2.0V$ (enabled), $I_L = 100\mu A$ $I_L = 20m A$ $I_L = 50m A$		180 225 850	750 1200	μΑ μΑ μΑ
I <sub>GNDDO</sub>	Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than designed $V_{OUT}$ , Note 5		200	300	μA
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		180	250	mA
$\Delta V_{O} / \Delta P_{D}$	Thermal Regulation	Note 6		0.05		%/W

### Control Input

V <sub>IL</sub> V <sub>IH</sub>	Input Voltage Level Logic Low Logic High	shutdown enabled	2.0		0.6	V V
I <sub>IL</sub> I <sub>IH</sub>	Control Input Current	$V_{IL} \le 0.6V$ $V_{IH} \ge 2.0V$		0.01 15	1 <b>50</b>	μΑ μΑ

General Note: Devices are ESD protected, however, handling precautions are recommended.

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{MAX} = (T_{J(max)} - T_A) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown.  $\theta_{JA}$  of the 8-lead MSOP is 200°C/W, mounted on a PC board.

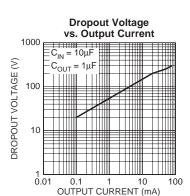
Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

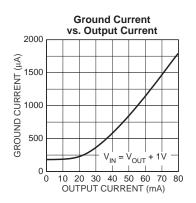
**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

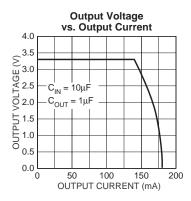
Note 4: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

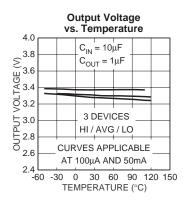
**Note 5:** Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

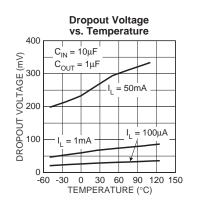
**Note 6:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 50mA load pulse at  $V_{IN} = 16V$  for t = 10ms.

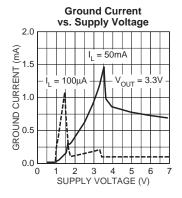












Short Circuit Current

vs. Input Voltage

 $C_{IN} = 10 \mu F$  $C_{OUT} = 1 \mu F$ 

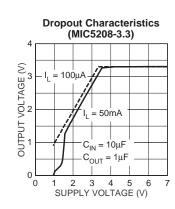
7

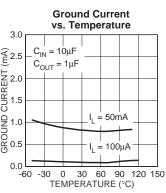
0

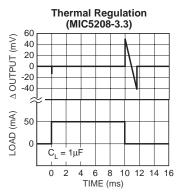
0

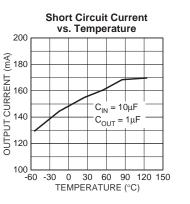
1

2 3 4 5 6

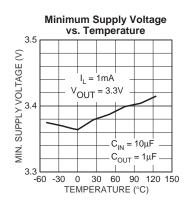


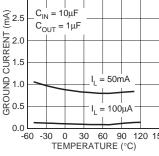






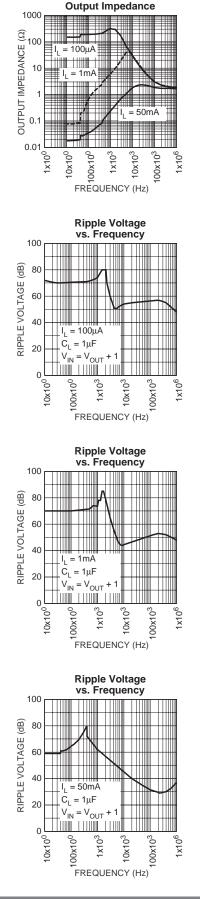
INPUT VOLTAGE (V)

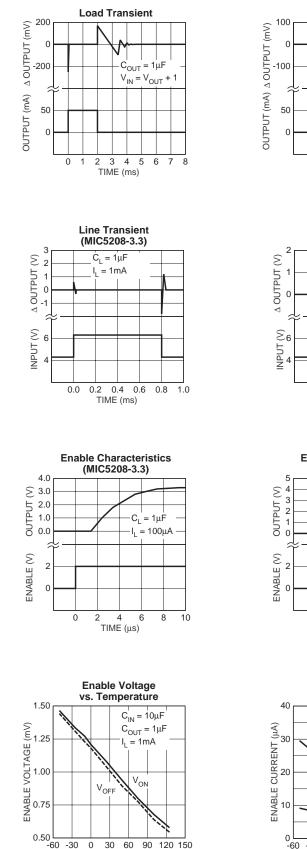


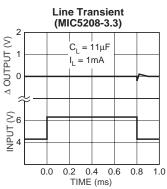


Micrel

**Section 5: Data Sheets** 







0 5

Load Transient

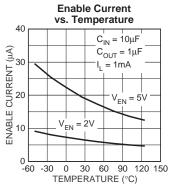
 $C_{OUT} = 10 \mu F$ 

10

TIME (ms)

15 20

 $V_{IN} = V_{OUT} + 1$ 



0 0 30 60 90 120 150 TEMPERATURE (°C)

## **Applications Information**

### Supply/Ground

Both MIC5208 GND pins must be connected to the same ground potential. INA and INB can each be connected to a different supply.

### Enable/Shutdown

ENA (enable/shutdown) and ENB may be enabled separately. Forcing ENA/B high (> 2V) enables the associated regulator. ENA/B requires a small amount of current, typically 15 $\mu$ A. While the logic threshold is TTL/CMOS compatible, ENA/B may be forced as high as 20V, independent of V<sub>IN</sub>.

### **Input Capacitor**

A  $0.1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (effective series resistance) of about 5 $\Omega$  or less and a resonant frequency above 500kHz. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytics have electrolytes that freeze at about -30°C, solid tantalums are recommended for operation below -25°C.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.22\mu$ F for current below 10mA or  $0.1\mu$ F for currents below 1mA.

### **No-Load Stability**

The MIC5208 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

### Thermal Shutdown

Thermal shutdown is independent on both halves of the dual MIC5208, however, an overtemperature condition in one half may affect the other half because of proximity.

### **Thermal Considerations**

Multilayer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

The MIC5208-xxBMM (8-lead MSOP) has a thermal resistance of 200°C/W when mounted on a FR4 board with minimum trace widths and no ground plane.

PC Board Dielectric	$\theta_{JA}$
FR4	200°C

**MSOP** Thermal Characteristics

For additional heat sink characteristics, please refer to Micrel Application Hint 17, "Calculating P.C. Board Heat Sink Area For Surface Mount Packages".



# **MIC5209**

500mA Low-Noise LDO Voltage Regulator

## **Preliminary Information**

# **General Description**

The MIC5209 is an efficient linear voltage regulator with very low dropout voltage, typically 10mV at light loads and less than 500mV at full load, with better than 1% output voltage accuracy.

Designed especially for hand-held, battery-powered devices, the MIC5209 features low ground current to help prolong battery life. An enable/shutdown pin on SO-8 and TO-263-5 versions can further improve battery life with near-zero shutdown current.

Key features include reversed-battery protection, current limiting, overtemperature shutdown, ultra-low-noise capability (SO-8 and TO-263-5 versions), and availability in thermally efficient packaging. The MIC5209 is available in adjustable or fixed output voltages.

For space-critical applications where peak currents do not exceed 500mA, see the MIC5219.

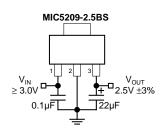
## Features

- Meets Intel® Slot 1 and Slot 2 requirements
- Guaranteed 500mA output over the full operating temperature range
- Low 500mV maximum dropout voltage at full load
- Extremely tight load and line regulation
- Thermally-efficient surface-mount package
- Low temperature coefficient
- · Current and thermal limiting
- Reversed-battery protection
- No-load stability
- 1% output accuracy
- Ultra-low-noise capability in SO-8 and TO-263-5

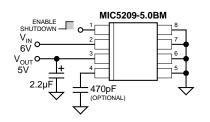
## **Applications**

- Pentium II Slot 1 and Slot 2 support circuits
- Laptop, notebook, and palmtop computers
- Cellular telephones
- Consumer and personal electronics
- SMPS post-regulator/dc-to-dc modules
- High-efficiency linear power supplies

# **Typical Applications**



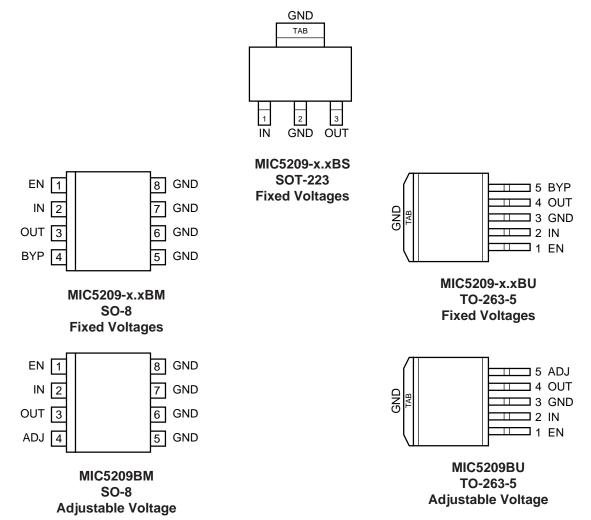
3.3V Nominal-Input Slot-1 Power Supply



**Ultra-Low-Noise 5V Regulator** 

# **Ordering Information**

Part Number	Voltage	Junct. Temp. Range	Package
MIC5209-2.5BS	2.5V	–40°C to +125°C	SOT-223
MIC5209-3.0BS	3.0V	–40°C to +125°C	SOT-223
MIC5209-3.3BS	3.3V	–40°C to +125°C	SOT-223
MIC5209-3.6BS	3.6V	–40°C to +125°C	SOT-223
MIC5209-5.0BS	5.0V	–40°C to +125°C	SOT-223
MIC5209-1.8BM	1.8V	–40°C to +125°C	SO-8
MIC5209-2.5BM	2.5V	–40°C to +125°C	SO-8
MIC5209-3.0BM	3.0V	–40°C to +125°C	SO-8
MIC5209-3.3BM	3.3V	–40°C to +125°C	SO-8
MIC5209-3.6BM	3.6V	–40°C to +125°C	SO-8
MIC5209-5.0BM	5.0V	–40°C to +125°C	SO-8
MIC5209BM	Adj.	–40°C to +125°C	SO-8
MIC5209-2.5BU	2.5V	–40°C to +125°C	TO-263-5
MIC5209-3.0BU	3.3V	–40°C to +125°C	TO-263-5
MIC5209-3.3BU	3.3V	–40°C to +125°C	TO-263-5
MIC5209-3.6BU	3.3V	–40°C to +125°C	TO-263-5
MIC5209-5.0BU	5.0V	–40°C to +125°C	TO-263-5
MIC5209BU	Adj.	–40°C to +125°C	TO-263-5



## **Pin Description**

Pin No. SOT-223	Pin No. SO-8	Pin No. TO-263-5	Pin Name	Pin Function
1	2	2	IN	Supply Input
2, тав	5–8	3	GND	Ground: SOT-223 pin 2 and TAB are internally connected. SO-8 pins 5 through 8 are internally connected.
3	3	4	OUT	Regulator Output
	1	1	EN	Enable (Input): CMOS compatible control input. Logic high = enable; logic low or open = shutdown.
	4 (fixed)	5 (fixed)	BYP	Reference Bypass: Connect external 470pF capacitor to GND to reduce output noise. May be left open. For 1.8V or 2.5V operation, see "Applications Information."
	4 (adj.)	5 (adj.)	ADJ	Adjust (Input): Feedback input. Connect to resistive voltage-divider network.

## Absolute Maximum Ratings (Note 1)

Supply Input Voltage (V <sub>IN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited, Note 3
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Lead Temperature (soldering, 5 s	sec.) 260°C
Storage Temperature (T <sub>S</sub> )	–65°C to +150°C

# **Operating Ratings (Note 2)**

Supply Input Voltage (VIN)	+2.5V to +16V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature (T <sub>J</sub> )	. –40°C to +125°C
Package Thermal Resistance	Note 3

## **Electrical Characteristics**

 $V_{IN} = V_{OUT} + 1.0V; C_{OUT} = 4.7\mu F, I_{OUT} = 100\mu A; T_J = 25^{\circ}C, \text{ bold } \text{values indicate } -40^{\circ}C \leq T_J \leq +125^{\circ}C; \text{ unless noted.}$ 

Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>OUT</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-1 -2		1 <b>2</b>	% %
ΔV <sub>OUT</sub> /ΔT	Output Voltage Temperature Coefficient	Note 4		40		ppm/°C
ΔV <sub>OUT</sub> /V <sub>OUT</sub>	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.009	0.05 <b>0.1</b>	%/V %/V
ΔV <sub>OUT</sub> /V <sub>OUT</sub>	Load Regulation	I <sub>OUT</sub> = 100μA to 500mA, <b>Note 5</b>		0.05	0.5 <b>0.7</b>	% %
V <sub>IN</sub> – V <sub>OUT</sub>	Dropout Voltage, Note 6	I <sub>OUT</sub> = 100μA		10	60 <b>80</b>	mV mV
		I <sub>OUT</sub> = 50mA		115	175 <b>250</b>	mV mV
		I <sub>OUT</sub> = 150mA		165	300 <b>400</b>	mV mV
		I <sub>OUT</sub> = 500mA		300	500 <b>600</b>	mV mV
I <sub>GND</sub>	Ground Pin Current, Notes 7, 8	$V_{EN} \ge 3.0V, I_{OUT} = 100\mu A$		80	130 <b>170</b>	μA μA
		$V_{EN} \ge 3.0V, I_{OUT} = 50mA$		350	650 <b>900</b>	μA μA
		$V_{EN} \ge 3.0V, I_{OUT} = 150mA$		1.8	2.5 <b>3.0</b>	mA mA
		$V_{EN} \ge 3.0V, I_{OUT} = 500mA$		8	20 <b>25</b>	mA mA
I <sub>GND</sub>	Ground Pin Quiescent Current,	$V_{EN} \le 0.4V$ (shutdown)		0.05	3	μA
	Note 8	$V_{EN} \le 0.18V$ (shutdown)		0.10	8	μA
PSRR	Ripple Rejection	f = 120Hz		75		dB
I <sub>LIMIT</sub>	Current Limit	V <sub>OUT</sub> = 0V		700	900 <b>1000</b>	mA mA
$\Delta V_{OUT} / \Delta P_D$	Thermal Regulation	Note 9		0.05		%/W
e <sub>no</sub>	Output Noise Note 10	$V_{OUT} = 2.5V, I_{OUT} = 50mA, C_{OUT} = 2.2\mu F, C_{BYP} = 0$		500		nV/√Hz
		$I_{OUT} = 50$ mA, $C_{OUT} = 2.2 \mu$ F, $C_{BYP} = 470$ pF		300		nV/√Hz

	Enable Input Logic-Low Voltage	V <sub>EN</sub> = logic low (regulator shutdown)			0.4	V
		V <sub>EN</sub> = logic high (regulator enabled)	2.0		0.18	V
I <sub>ENL</sub>	Enable Input Current	$V_{ENL} \le 0.4V$		0.01	-1	μA
		$V_{ENL} \le 0.18V$		0.01	-2	μA
I <sub>ENH</sub>		$V_{ENH} \ge 2.0V$		5	20 <b>25</b>	μΑ μΑ

**Note 1.** Exceeding the absolute maximum rating may damage the device.

Note 2. The device is not guaranteed to function outside its operating rating.

Note 4: Output voltage temperature coefficient is the worst case voltage change divided by the total temperature range.

Note 6: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

Note 7: Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

Note 8: V<sub>EN</sub> is the voltage externally applied to devices with the EN (enable) input pin. [SO-8 (M) and TO-263-5 (U) packages only.]

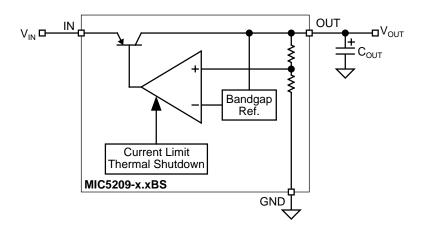
Note 9: Thermal regulation is the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 500mA load pulse at V<sub>IN</sub> = 16V for t = 10ms.

Note 10: C<sub>BYP</sub> is an optional, external bypass capacitor connected to devices with a BYP (bypass) or ADJ (adjust) pin. [SO-8 (M) and TO-263-5 (U) packages only].

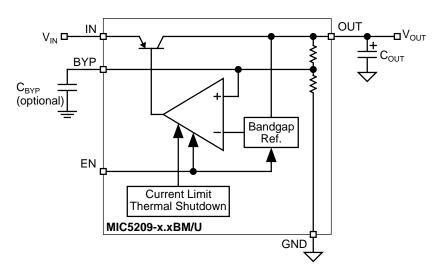
**Note 3:** The maximum allowable power dissipation at any  $T_A$  (ambient temperature) is calculated using:  $P_{D(max)} = (T_{J(max)} - T_A) \div \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. See Table 1 and the "Thermal Considerations" section for details.

**Note 5:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 100μA to 500mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

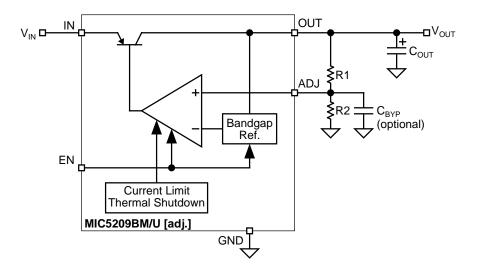
## **Block Diagrams**



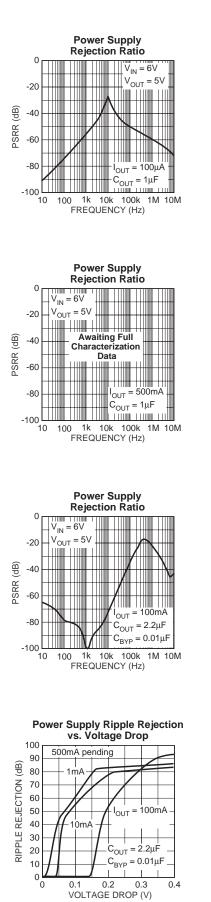
Low-Noise Fixed Regulator (SOT-223 version only)

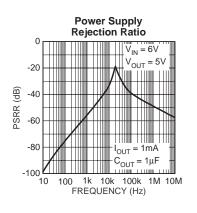


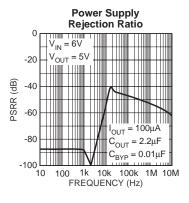
**Ultra-Low-Noise Fixed Regulator** 











**Power Supply** 

Rejection Ratio

Awaiting Full

Characterization Data

.....

I<sub>OUT</sub>  $C_{OUT} = 2.2 \mu F$ 

100 1k 10k 100k 1M 10M FREQUENCY (Hz)

= 500mA

 $C_{BYP} = 0.01$ 

/<sub>IN</sub> = 6V

 $V_{OUT} = 5V$ 

-20

-60

-80

-100

10

10

0.1

0.01

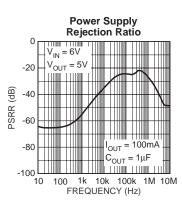
0.001

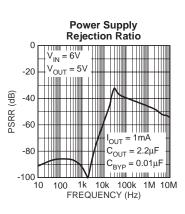
0.0001

10

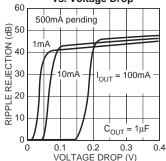
NOISE (µV/√Hz)

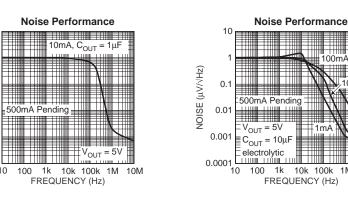
PSRR (dB) -40

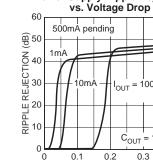




Power Supply Ripple Rejection vs. Voltage Drop







VOLTAGE DROP (V)

100mA

1M 10M

∏1mA



NOISE (µV/VHz)

10

1

0.1

0.01

0.001

0.0001

10

10

1

0.1

0.01

0.001

0.0001

25

(mA)

5 L -50

8

OUTPUT VOLTAGE (V) N P 9

0

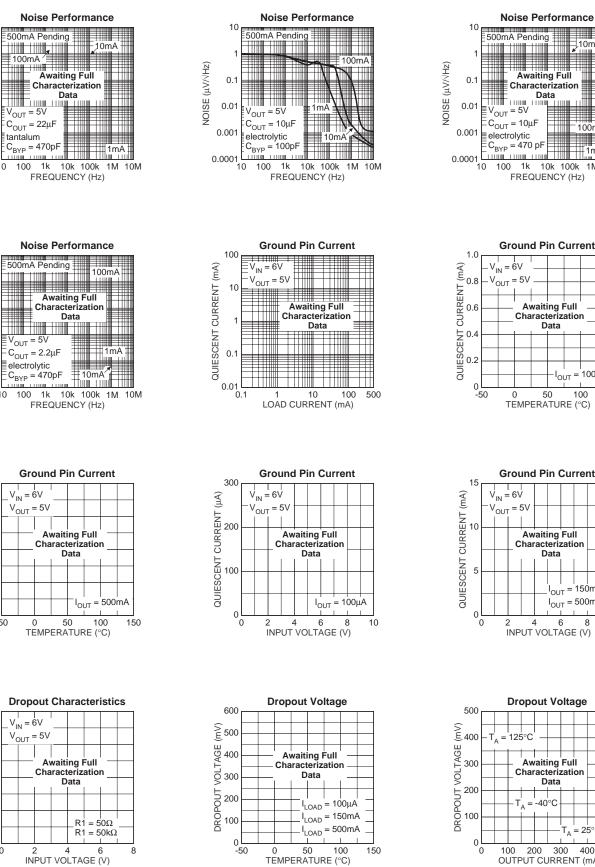
0

10

NOISE (µV/VHz)

## **Typical Characteristics**

10mA

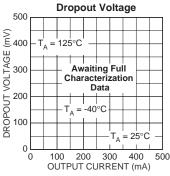


-100mA electrolytic C<sub>BYP</sub> = 470 pF 1mA 100 1k 10k 100k 1M 10M FREQUENCY (Hz) **Ground Pin Current**  $V_{IN} = 6V$  $-V_{OUT} = 5V$ Awaiting Full Characterization Data

Awaiting Full

 $= 100 \mu$ A OUT 1 0 50 100 150 TEMPERATURE (°C)

**Ground Pin Current**  $V_{IN} = 6V$  $V_{OUT} = 5V$ Awaiting Full Characterization Data I<sub>OUT</sub> = 150mÅ  $I_{OUT} = 500 \text{mA}$ 6 10 2 4 8 INPUT VOLTAGE (V)



1000

900

800

700 600

500

-50

0

OUTPUT CURRENT (mA)

Short Circuit Current

Awaiting Full Characterization

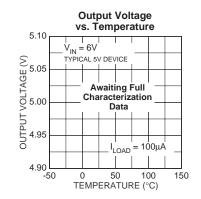
Data

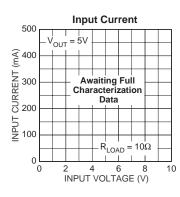
50

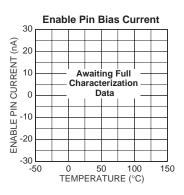
TEMPERATURE (°C)

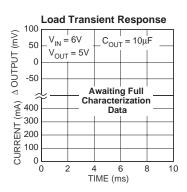
100

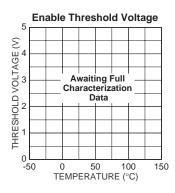
150

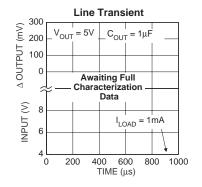


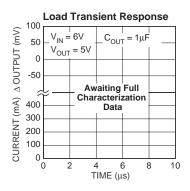


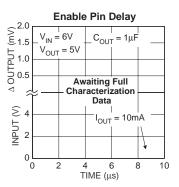


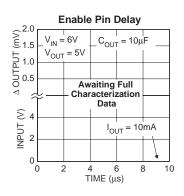


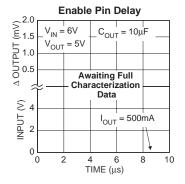














## **Applications Information**

### Enable/Shutdown

Enable is available only on devices in the SO-8 (M) and TO-263-5 (U) packages.

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic. If the enable/ shutdown feature is not required, connect EN to IN (supply input).

### **Input Capacitor**

A  $1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. The minimum size of the output capacitor is dependent upon whether a reference bypass capacitor is used. 1µF minimum is recommended when  $C_{BYP}$  is not used (see Figure 1). 2.2µF minimum is recommended when  $C_{BYP}$  is 470pF (see Figure 2). Larger values improve the regulator's transient response.

The output capacitor should have an ESR (equivalent series resistance) of about 5 $\Omega$  and a resonant frequency above 1MHz. Ultra-low-ESR capacitors can cause a low amplitude oscillation on the output and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is needed for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

### **No-Load Stability**

The MIC5209 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

### **Reference Bypass Capacitor**

BYP (reference bypass) is available only on devices in SO-8 and TO-263-5 packages.

BYP is connected to the internal voltage reference. A 470pF capacitor (C<sub>BYP</sub>) connected from BYP to GND quiets this reference, providing a significant reduction in output noise (ultra-low-noise performance). Because C<sub>BYP</sub> reduces the phase margin, the output capacitor should be increased to at least  $2.2\mu$ F to maintain stability.

The start-up speed of the MIC5209 is inversely proportional to the size of the reference bypass capacitor. Applications requiring a slow ramp-up of output voltage should consider larger values of  $C_{BYP}$ . Likewise, if rapid turn-on is necessary, consider omitting  $C_{BYP}$ .

If output noise is not critical, omit  $\mathrm{C}_{\mathrm{BYP}}$  and leave BYP open.

### Thermal Considerations

The SOT-223 has a ground tab which allows it to dissipate more power than the SO-8. Refer to "Slot-1 Power Supply" for details. At 25°C ambient, it will operate reliably at 2W dissipation with "worst-case" mounting (no ground plane, minimum trace widths, and FR4 printed circuit board).

Thermal resistance values for the SO-8 represent typical mounting on a 1"-square, copper-clad, FR4 circuit board. For greater power dissipation, SO-8 versions of the MIC5209 feature a fused internal lead frame and die bonding arrangement that reduces thermal resistance when compared to standard SO-8 packages.

Package	θ <sub>JA</sub>	θ <sub>JC</sub>	
SOT-223 (S)	50°C/W	8°C/W	
SO-8 (M)	50°C/W	25°C/W	
TO-263-5 (U)		2°C/W	

#### Table 1. MIC5209 Thermal Resistance

Multilayer boards with a ground plane, wide traces near the pads, and large supply-bus lines will have better thermal conductivity and will also allow additional power dissipation.

For additional heat sink characteristics, please refer to Micrel Application Hint 17, "Designing P.C. Board Heat Sinks", included in Micrel's *Databook*. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.

#### Low-Voltage Operation

The MIC5209-1.8 and MIC5209-2.5 require special consideration when used in voltage-sensitive systems. They may momentarily overshoot their nominal output voltages unless appropriate output and bypass capacitor values are chosen.

During regulator power up, the pass transistor is fully saturated for a short time, while the error amplifier and voltage reference are being powered up more slowly from the output (see "Block Diagram"). Selecting larger output and bypass capacitors allows additional time for the error amplifier and reference to turn on and prevent overshoot.

To ensure that no overshoot is present when starting up into a light load (100 $\mu$ A), use a 4.7 $\mu$ F output capacitance and 470pF bypass capacitance. This slows the turn-on enough to allow the regulator to react and keep the output voltage from exceeding its nominal value. At heavier loads, use a 10 $\mu$ F output capacitance and 470pF bypass capacitance. Lower values of output and bypass capacitance can be used, depending on the sensitivity of the system.

Applications that can withstand some overshoot on the output of the regulator can reduce the output capacitor and/ or reduce or eliminate the bypass capacitor. Applications that are not sensitive to overshoot due to power-on reset delays can use normal output and bypass capacitor configurations.

### **Fixed Regulator Circuits**

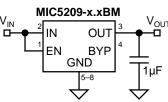
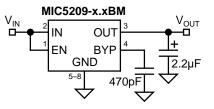


Figure 1. Low-Noise Fixed Voltage Regulator

Figure 1 shows a basic MIC5209-x.xBM (SO-8) fixed-voltage regulator circuit. See Figure 5 for a similar configuration using the more thermally-efficient MIC5209-x.xBS (SOT-223). A 1 $\mu$ F minimum output capacitor is required for basic fixed-voltage applications.



### Figure 2. Ultra-Low-Noise Fixed Voltage Regulator

Figure 2 includes the optional 470pF noise bypass capacitor between BYP and GND to reduce output noise. Note that the minimum value of  $C_{OUT}$  must be increased when the bypass capacitor is used.

Adjustable Regulator Circuits

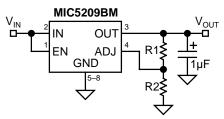
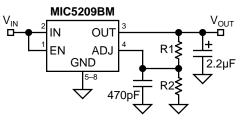


Figure 3. Low-Noise Adjustable Voltage Regulator

The MIC5209BM/U can be adjusted to a specific output voltage by using two external resistors (Figure 3). The resistors set the output voltage based on the equation:

$$V_{OUT} = V_{REF} \left( 1 + \frac{R2}{R1} \right)$$

This equation is correct due to the configuration of the bandgap reference. The bandgap voltage is relative to the output, as seen in the block diagram. Traditional regulators normally have the reference voltage relative to ground; therefore, their equations are different from the equation for the MIC5209BM/U. Although ADJ is a high-impedance input, for best performance, R2 should not exceed  $470 k \Omega.$ 



### Figure 4. Ultra-Low-Noise Adjustable Application.

Figure 4 includes the optional 470pF bypass capacitor from ADJ to GND to reduce output noise.

### Slot-1 Power Supply

Intel's Pentium II processors have a requirement for a 2.5V  $\pm$ 5% power supply for a clock synthesizer and its associated loads. The current requirement for the 2.5V supply is dependent upon the clock synthesizer used, the number of clock outputs, and the type of level shifter (from core logic levels to 2.5V levels). Intel estimates a worst-case load of 320mA.

The MIC5209 was designed to provide the 2.5V power requirement for Slot-1 applications. Its guaranteed performance of  $2.5V \pm 3\%$  at 500mA allows adequate margin for all systems, and its dropout voltage of 500mV means that it operates from a worst-case 3.3V supply where the voltage can be as low as 3.0V.

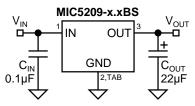


Figure 5. Slot-1 Power Supply

A Slot-1 power supply (Figure 5) is easy to implement. Only two capacitors are necessary, and their values are not critical.  $C_{\rm IN}$  bypasses the internal circuitry and should be at least  $0.1\mu F.\ C_{OUT}$  provides output filtering, improves transient response, and compensates the internal regulator control loop. Its value should be at least  $22\mu F.\ C_{\rm IN}$  and  $C_{OUT}$  may be increased as much as desired.

### Slot-1 Power Supply Power Dissipation

Powered from a 3.3V supply, the Slot-1 power supply of Figure 5 has a nominal efficiency of 75%. At the maximum anticipated Slot 1 load (320mA), the nominal power dissipation is only 256mW.

The SOT-223 package has sufficient thermal characteristics for wide design margins when mounted on a single layer copper-clad printed circuit board. The power dissipation of the MIC5209 is calculated using the voltage drop across the device  $\times$  output current plus supply voltage  $\times$  ground current. Considering worst case tolerances, the power dissipation could be as high as:

$$\begin{split} (\mathsf{V}_{\mathsf{IN}(\mathsf{max})} - \mathsf{V}_{\mathsf{OUT}(\mathsf{max})}) \times \mathsf{I}_{\mathsf{OUT}} + \mathsf{V}_{\mathsf{IN}(\mathsf{max})} \times \mathsf{I}_{\mathsf{GND}} \\ [(3.6\mathsf{V} - 2.375\mathsf{V}) \times 320\mathsf{mA}] + (3.6\mathsf{V} \times 4\mathsf{mA}) \\ \mathsf{P}_{\mathsf{D}} = 407\mathsf{mW} \end{split}$$

Using the maximum junction temperature of 125°C and a  $\theta_{JC}$  of 8°C/W for the SOT-223, 25°C/W for the SO-8, or 2°C/W for the TO-263 package, the following worst-case heat-sink thermal resistance ( $\theta_{SA}$ ) requirements are:

$$\theta_{JA} = \frac{T_{J(max)} - T_{A}}{P_{D}}$$

 $\theta_{SA} = \theta_{JA} - \theta_{JC}$ 

T <sub>A</sub>	40°C	50°C	60°C	75°C
θ <sub>JA</sub> (limit)	209°C/W	184°C/W	160°C/W	123°C/W
$\theta_{SA}$ SOT-223	201°C/W	176°C/W	152°C/W	115°C/W
θ <sub>SA</sub> SO-8	184°C/W	159°C/W	135°C/W	98°C/W
θ <sub>SA</sub> TO-263-5	207°C/W	182°C/W	158°C/W	121°C/W

Table 2. Maximum Allowable Thermal Resistance

Table 2 and Figure 6 show that the Slot-1 power supply application can be implemented with a minimum footprint layout. Figure 6 shows the necessary copper pad area to obtain specific heat sink thermal resistance ( $\theta_{SA}$ ) values. The  $\theta_{SA}$  values in Table 2 require much less than 500mm<sup>2</sup> of copper, according to Figure 6, and can easily be accomplished with the minimum footprint.

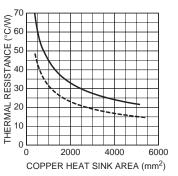


Figure 6. PCB Heat Sink Thermal Resistance



# MIC5210

## **Dual 150mA LDO Regulator**

### **Preliminary Information**

## **General Description**

The MIC5210 is a dual linear voltage regulator with very low dropout voltage (typically 10mV at light loads and 140mV at 100mA), very low ground current ( $225\mu$ A at 10mA output), and better than 1% initial accuracy. It also features individual logic-compatible enable/shutdown control inputs.

Both regulator outputs can supply up to 150mA at the same time as long as each regulator's maximum junction temperature is not exceeded.

Designed especially for hand-held battery powered devices, the MIC5210 can be switched by a CMOS or TTL compatible logic signal, or the enable pin can be connected to the supply input for 3-terminal operation. When disabled, power consumption drops nearly to zero. Dropout ground current is minimized to prolong battery life.

Key features include current limiting, overtemperature shutdown, and protection against reversed battery.

The MIC5210 is available in 3.0V, 3.3V, 3.6V, 4.0V and 5.0V fixed voltage configurations. Other voltages are available; contact Micrel for details.

## Features

- Micrel Mini 8<sup>™</sup> MSOP package
- Up to 150mA per regulator output
- Low quiescent current
- Low dropout voltage
- Wide selection of output voltages
- Tight load and line regulation
- Low temperature coefficient
- · Current and thermal limiting
- Reversed input polarity protection
- Zero off-mode current
- Logic-controlled electronic enable

### Applications

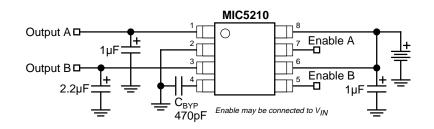
- Cellular telephones
- · Laptop, notebook, and palmtop computers
- · Battery powered equipment
- Bar code scanners
- SMPS post regulator/dc-to-dc modules
- High-efficiency linear power supplies

### **Ordering Information**

Part Number	Voltage	Accuracy	Junction Temp. Range*	Package
MIC5210-3.0BMM	3.0	1.0%	–40°C to +125°C	8-lead MSOP
MIC5210-3.3BMM	3.3	1.0%	–40°C to +125°C	8-lead MSOP
MIC5210-3.6BMM	3.6	1.0%	–40°C to +125°C	8-lead MSOP
MIC5210-4.0BMM	4.0	1.0%	–40°C to +125°C	8-lead MSOP
MIC5210-5.0BMM	5.0	1.0%	–40°C to +125°C	8-lead MSOP

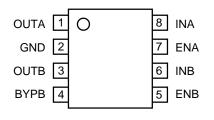
Other voltages available. Contact Micrel for details.

## **Typical Application**



Low-Noise + Ultralow-Noise (Dual) Regulator

## **Pin Configuration**





## **Pin Description**

Pin Number	Pin Name	Pin Function
1	OUTA	Regulator Output A
2	GND	Ground.
3	OUTB	Regulator Output B
4	ВҮРВ	Reference Bypass B: Connect external 470pF capacitor to GND to reduce output noise in regulator "B". May be left open.
5	ENB	Enable/Shutdown B (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown. Do not leave floating.
6	INB	Supply Input B
7	ENA	Enable/Shutdown A (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown. Do not leave floating.
8	INA	Supply Input A

## Absolute Maximum Ratings

Supply Input Voltage (VIN)	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> )	. Internally Limited
Storage Temperature Range	. –60°C to +150°C
Lead Temperature (soldering, 5 sec.)	260°C

## **Recommended Operating Conditions**

Supply Input Voltage (VIN)	2.5V to 16V
Enable Input Voltage (V <sub>EN</sub> )	0V to 16V
Junction Temperature (T <sub>J</sub> )	-40°C to +125°C
Thermal Resistance $(\theta_{JA})$	Note 1

### **Electrical Characteristics**

Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>O</sub>	Output Voltage Accuracy	variation from specified V <sub>OUT</sub>	-1 -2		1 2	% %
ΔV <sub>O</sub> /ΔT	Output Voltage Temperature Coefficient	Note 2		40		ppm/°C
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.004	0.012 <b>0.05</b>	% / V % / V
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 150mA (Note 3)		0.02	0.2 <b>0.5</b>	% %
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage, Note 4	I <sub>L</sub> = 100μA		10	50 <b>70</b>	mV mV
		I <sub>L</sub> = 50mA		110	150 <b>230</b>	mV mV
		I <sub>L</sub> = 100mA		140	250 <b>300</b>	mV mV
		I <sub>L</sub> = 150mA		165	275 <b>350</b>	mV mV
I <sub>GND</sub>	Quiescent Current	$V_{EN} \le 0.4V$ (shutdown) $V_{EN} \le 0.18V$ (shutdown)		0.01	1 5	μA μA
I <sub>GND</sub>	Ground Pin Current, Note 5 (per regulator)	$V_{EN} \ge 2.0V, I_{L} = 100\mu A$		80	125 <b>150</b>	μΑ μΑ
		$I_L = 50 \text{mA}$		350	600 <b>800</b>	μA μA
		I <sub>L</sub> = 100mA		600	1000 <b>1500</b>	μΑ μΑ
		I <sub>L</sub> = 150mA		1300	1900 <b>2500</b>	μΑ μΑ
PSRR	Ripple Rejection	frequency = 100Hz, $I_L = 100\mu A$		75		dB
ILIMIT	Current Limit	$V_{OUT} = 0V$		320	500	mA
$\Delta V_0 / \Delta P_D$	Thermal Regulation	Note 6		0.05		%/W
e <sub>no</sub>	Output Noise (Regulator B only)	$I_L = 50$ mA, $C_L = 2.2\mu$ F, 470pF from BYPB to GND		260		nV/√Hz

#### ENABLE Input

V <sub>IL</sub>	Enable Input Logic-Low Voltage	regulator shutdown			0.4 <b>0.18</b>	V V
V <sub>IH</sub>	Enable Input Logic-High Voltage	regulator enabled	2.0			V
I <sub>IL</sub>	Enable Input Current	$\begin{array}{l} V_{IL} \leq 0.4V \\ V_{IL} \leq 0.18V \end{array}$		0.01	-1 - <b>2</b>	μΑ μΑ
I <sub>IH</sub>		$V_{IH} \ge 2.0V$ $V_{IH} \ge 2.0V$		5	20 <b>25</b>	μΑ μΑ

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its operating ratings. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{D(max)} = (T_{J(max)} - T_A) \div \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. The  $\theta_{JA}$  of the 8-lead MSOP (MM) is 200°C/W mounted on a PC board (see "Thermal Considerations" section for further details).

Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 0.1mA to 150mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

Note 4: Dropout Voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

**Note 5:** Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

Note 6: Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 150mA load pulse at  $V_{IN} = 16V$  for t = 10ms.

**Section 5: Data Sheets** 

0

-20

-60

-80

-100

-20

-40

-60

-80

-100

-20

-60

-80

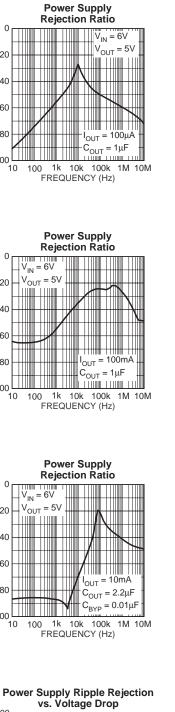
-100

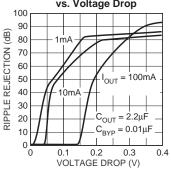
PSRR (dB) -40

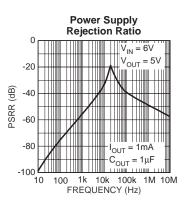
PSRR (dB)

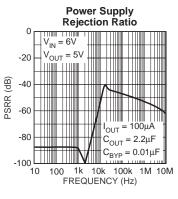
PSRR (dB) -40

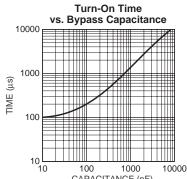
## **Typical Characteristics**



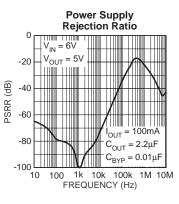


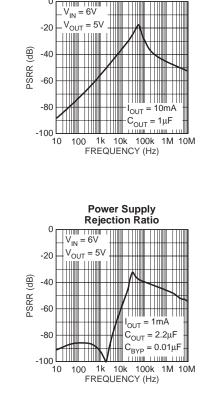






CAPACITANCE (pF)



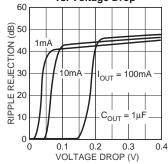


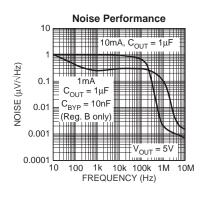
**Power Supply** 

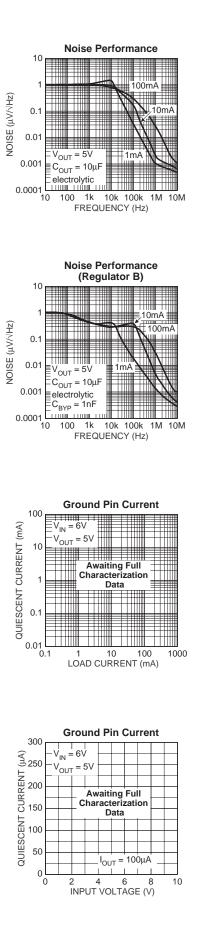
Rejection Ratio

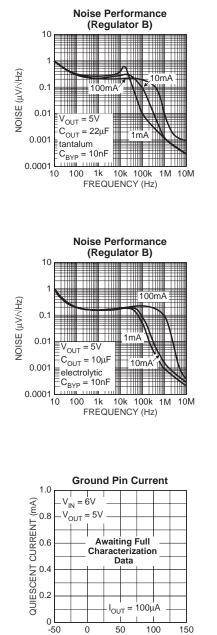
0

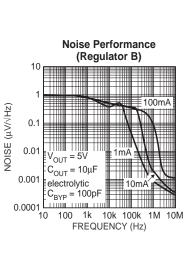
Power Supply Ripple Rejection vs. Voltage Drop

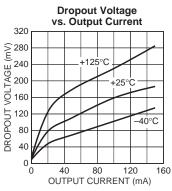




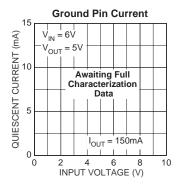




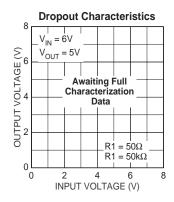


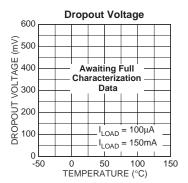


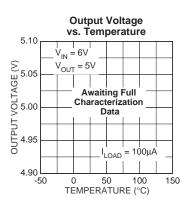
**Ground Pin Current** 25  $V_{IN}^{i} = 6V$ QUIESCENT CURRENT (mA) 01 01 02  $V_{OUT} = 5V$ Awaiting Full Characterization Data = 500µA OUT 5 -50 50 100 150 0 TEMPERATURE (°C)

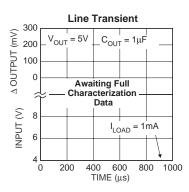


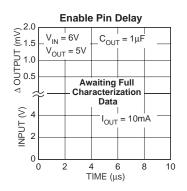
TEMPERATURE (°C)

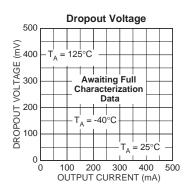


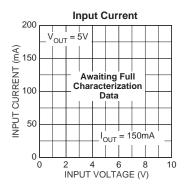












Load Transient Response

Awaiting Full

Characterization

Data

6

 $C_{OUT} = 10 \mu F$ 

 $I_{OUT} = 10 \text{mA}$ 

8 10

TIME (µs)

**Enable Pin Delay** 

Awaiting Full Characterization

Data

 $C_{OUT} = 1 \mu F$ 

8 10

100

50

0

1

-50

100

50

0 L 0

(\/m) 1.5 1.0 1.0 0.5

INPUT (V) 4

2

0

0 2

V<sub>IN</sub> = 6V

 $V_{OUT} = 5V$ 

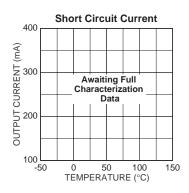
2

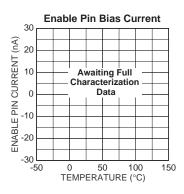
V<sub>IN</sub> = 6V

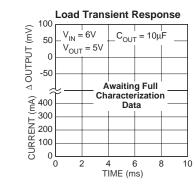
 $V_{OUT} = 5V$ 

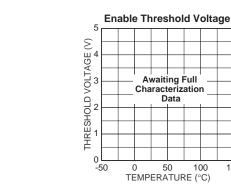
4

CURRENT (mA)  $\Delta$  OUTPUT (mV)







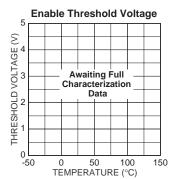


**Section 5: Data Sheets** 

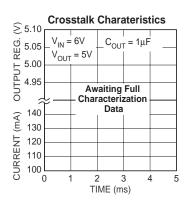
4 6

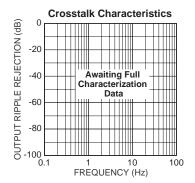
TIME (µs)

150

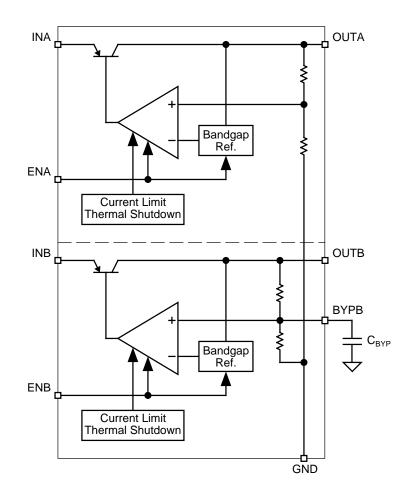


Enable Pin Delay						_
(^2.0 1.5 1.0 1.0 1.0 0.5	_V <sub>IN</sub> = V <sub>OUT</sub>	6V = 5V	_C <sub>OUT</sub>	- = 1μF		
-	<u>}                                    </u>		aiting acteriz Data			
(V) TUQNI			I <sub>OUT</sub>	= 150	mA	
0	) 2		4 θ IME (μ		3 1	0





## **Block Diagram**



## **Applications Information**

### Enable/Shutdown

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic gates.

If the enable/shutdown feature is not required, connect EN to IN (supply input).

#### Input Capacitor

A  $1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

#### **Reference Bypass Capacitor**

BYPB (reference bypass) is connected to the internal voltage reference of regulator B. A 470pF capacitor ( $C_{BYP}$ ) connected from BYPB to GND quiets this reference, providing a significant reduction in output noise.  $C_{BYP}$  reduces the regulator phase margin; when using  $C_{BYP}$ , output capacitors of 2.2µF or greater are generally required to maintain stability.

The start-up speed of the MIC5210 is inversely proportional to the size of the reference bypass capacitor. Applications requiring a slow ramp-up of output voltage should consider larger values of  $C_{BYP}$ . Likewise, if rapid turn-on is necessary, consider omitting  $C_{BYP}$ .

If output noise is not a major concern, omit  $\mathrm{C}_{\mathrm{BYP}}$  and leave BYPB open.

#### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. The minimum size of the output capacitor is dependent upon whether a reference bypass capacitor is used. 1.0 $\mu$ F minimum is recommended when C<sub>BYP</sub> is not used (see Figure 2). 2.2 $\mu$ F minimum is recommended when C<sub>BYP</sub> is 470pF (see Figure 1). Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (effective series resistance) of about  $5\Omega$  or less and a resonant frequency above 1MHz. Ultralow-ESR capacitors may cause a low-amplitude oscillation and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytic capacitors have electrolytes that freeze at about  $-30^{\circ}$ C, solid tantalum capacitors are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is required for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

### No-Load Stability

The MIC5210 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

#### **Dual-Supply Operation**

When used in dual supply systems where the regulator load is returned to a negative supply, the output voltage must be diode clamped to ground.

#### **Thermal Considerations**

Multilayer boards having a ground plane, wide traces near the pads, and large supply bus lines provide better thermal conductivity.

The MIC5210-xxBMM (8-lead MSOP) has a thermal resistance of 200°C/W when mounted on a FR4 board with minimum trace widths and no ground plane.

PC Board Dielectric	$\theta_{JA}$
FR4	200°C/W

**MSOP** Thermal Characteristics

For additional heat sink characteristics, please refer to Micrel Application Hint 17, "Calculating P.C. Board Heat Sink Area For Surface Mount Packages".

#### Thermal Evaluation Examples

For example, at 50°C ambient temperature, the maximum package power dissipation is:

$$P_{D(max)} = (125^{\circ}C - 50^{\circ}C) \div 200^{\circ}C/W$$
  
= 375mW

If the intent is to operate the 5V version from a 6V supply at the full 150mA load for both outputs in a 50°C maximum ambient temperature, make the following calculation:

$$P_{D(each regulator)} = (V_{IN} - V_{OUT}) \times I_{OUT} + (V_{IN} \times I_{GND})$$
  
= (6V - 5V) × 150mA + (6V × 2.5mA)  
= 165mW  
$$P_{D(both regulators)} = 2 \text{ regulators} \times 165mW$$
  
= 330mW

The actual total power dissipation of 330mW is below the 375mW package maximum, therefore, the regulator can be used.

Note that both regulators cannot always be used at their maximum current rating. For example, in a 5V input to 3.3V output application at 50°C, if one regulator supplies 150mA, the other regulator is limited to a much lower current. The first regulator dissipates:

$$P_D = (5V - 3.3V) \ 150 + 2.5mA \ (5V)$$

 $P_{D} = 267.5 mW$ 

Then, the load that the remaining regulator can dissipate must not exceed:

375 mW - 267.5 mW = 107.5 mW

This means, using the same 5V input and 3.3V output voltage, the second regulator is limited to about 60mA.

Taking advantage of the extremely low-dropout voltage characteristics of the MIC5210, power dissipation can be reduced by using the lowest possible input voltage to minimized the input-to-output voltage drop.



# MIC5211

Dual μCap™ 50mA LDO Voltage Regulator

### **Preliminary Information**

## **General Description**

The MIC5211 is a dual µCap<sup>™</sup> 50mA linear voltage regulator with very low dropout voltage (typically 20mV at light loads), very low ground current (225µA at 20mA output current), and better than 3% initial accuracy. This dual device comes in the miniature SOT-23-6 package, featuring independent logic control inputs.

The  $\mu$ Cap<sup>TM</sup> regulator design is optimized to work with low-value, low-cost ceramic capacitors. The outputs typically require only 0.1 $\mu$ F of output capacitance for stability.

Designed especially for hand-held, battery-powered devices, ground current is minimized using Micrel's proprietary Super ßeta PNP<sup>™</sup> technology to prolong battery life. When disabled, power consumption drops nearly to zero.

Key features include SOT-23-6 packaging, current limiting, overtemperature shutdown, and protection against reversed battery conditions.

The MIC5211 is available in dual 2.5V, 3.0V, 3.3V, 3.6V, and 5.0V versions. Certain mixed voltages are also available. Contact Micrel for other voltages.

### Features

- Stable with low-value ceramic capacitors
- 125mA peak output current per regulator
- Independent logic controls
- Low quiescent current
- Low dropout voltage
- Mixed voltages available
- Tight load and line regulation
- Low temperature coefficient
- Current and thermal limiting
- Reversed input polarity protection
- Zero off-mode current
- Dual regulator in tiny SOT-23 package
- Input range up to 16V

## **Applications**

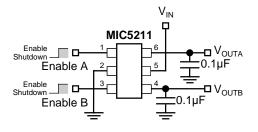
- Cellular telephones
- Laptop, notebook, and palmtop computers
- Battery-powered equipment
- Bar code scanners
- SMPS post regulator/dc-to-dc modules
- High-efficiency linear power supplies

Part Number	Marking	Voltage	Junction Temp. Range	Package
MIC5211-2.5BM6	LFCC	2.5	–40°C to +125°C	SOT-23-6
MIC5211-3.0BM6	LFGG	3.0	–40°C to +125°C	SOT-23-6
MIC5211-3.3BM6	LFLL	3.3	–40°C to +125°C	SOT-23-6
MIC5211-3.6BM6	LFQQ	3.6	–40°C to +125°C	SOT-23-6
MIC5211-5.0BM6	LFXX	5.0	–40°C to +125°C	SOT-23-6
Dual Voltage Regulators				
MIC5211-3.3/5.0BM6	LFLX	3.3/5.0	–40°C to +125°C	SOT-23-6

## Ordering Information

Other voltages available. Contact Micrel for details.

## **Typical Application**



 $\mu\text{Cap}$  is a trademark of Micrel, Inc.

Pin 1 Index Regulator Voltage Cu (Voura)	A Part Identificati B ENB AD AD A	3
Voltage	Code	
2.5V	С	
3V	G	
3.15V	Н	
3.3V	L	

Q

Х

# **Pin Description**

Pin Number	Pin Name	Pin Function
1	ENA	Enable/Shutdown A (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown.
2	GND	Ground
3	ENB	Enable/Shutdown B (Input): CMOS compatible input. Logic high = enable, logic low or open = shutdown.
4	OUTB	Regulator Output B
5	IN	Supply Input
6	OUTA	Regulator Output A

3.6V

5V

## **Absolute Maximum Ratings**

Supply Input Voltage (VIN)	–20V to +20V
Enable Input Voltage (V <sub>EN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited
Storage Temperature Range	–60°C to +150°C
Lead Temperature (soldering, 5 sec.)	260°C

## **Operating Ratings**

Supply Input Voltage (VIN)	2.5V to 16V
Enable Input Voltage (VEN)	0V to 16V
Junction Temperature (T <sub>J</sub> )	. −40°C to +125°C
6-lead SOT-23-6 (θ <sub>JA</sub> )	Note 1

Micrel

## **Electrical Characteristics**

 $V_{IN} = V_{OUT} + 1V$ ;  $I_L = 1mA$ ;  $C_L = 0.1\mu$ F, and  $V_{EN} \ge 2.0V$ ;  $T_J = 25^{\circ}$ C, **bold** values indicate  $-40^{\circ}$ C to  $+125^{\circ}$ C; for one-half of dual MIC5211; unless noted.

Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>O</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-3 -4		3 <b>4</b>	% %
$\Delta V_{O} / \Delta T$	Output Voltage Temperature Coeffcient	Note 2		50	200	ppm/°C
I <sub>PK</sub>	Peak Current			125		mA
$\Delta V_0 / V_0$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.008	0.3 <b>0.5</b>	% %
$\Delta V_0 / V_0$	Load Regulation	I <sub>L</sub> = 0.1mA to 50mA, <b>Note 3</b>		0.08	0.3 <b>0.5</b>	% %
V <sub>IN</sub> – V <sub>O</sub>	Dropout Voltage, Note 4	I <sub>L</sub> = 100μA		20		mV
		$I_L = 20 \text{mA}$		200	350	mV
		$I_L = 50 \text{mA}$		250	500	mV
I <sub>Q</sub>	Quiescent Current	$V_{EN} \le 0.4V$ (shutdown)		0.01	10	μΑ
I <sub>GND</sub>	Ground Pin Current	$V_{EN} \ge 2.0V$ (enabled), $I_L = 100\mu A$		180		μA
	Note 5	$I_L = 20 \text{mA}$		225	750	μA
		I <sub>L</sub> = 50mA		850	1200	μA
I <sub>GNDDO</sub>	Ground Pin Current at Dropout	$V_{IN} = 0.5V$ less than designed $V_{OUT}$ , Note 5		200	300	μΑ
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		180	250	mA
$\Delta V_O / \Delta P_D$	Thermal Regulation	Note 6		0.05		%/W

#### Enable Input

	Enable Input Voltage Level					
V <sub>IL</sub>		logic low (off)			0.6	V
V <sub>IH</sub>		logic high (on)	2.0			V
IIL	Enable Input Current	$V_{IL} \le 0.6V$		0.01	1	μΑ
I <sub>IH</sub>		$V_{IH} \ge 2.0V$		15	50	μΑ

General Note: Devices are ESD protected, however, handling precautions are recommended.

Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

Note 4: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

**Note 5:** Ground pin current is the quiescent current per regulator plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

**Note 6:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 50mA load pulse at  $V_{IN} = 16V$  for t = 10ms.

**Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its rated operating conditions. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{MAX} = (T_{J(max)} - T_A) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown.  $\theta_{JA}$  of the 6-lead SOT-23 is 220°C/W, mounted on a PC board.

1000

100

10

0.01

**DROPOUT VOLTAGE (V)** 

# **Typical Characteristics**

 $C_{IN} = 10\mu F$ 

0.1

 $C_{OUT} = 1\mu F$ 

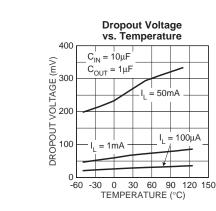
**Dropout Voltage** 

vs. Output Current

OUTPUT CURRENT (mA)

10

100



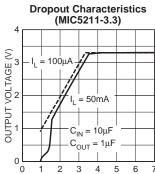
2.0

1 0

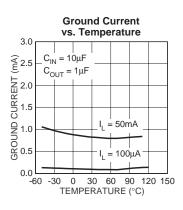
0.5

0.0

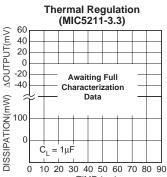
**GROUND CURRENT (mA)** 



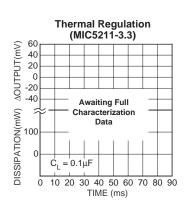
SUPPLY VOLTAGE (V)

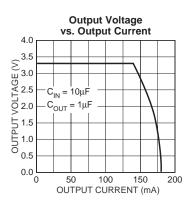


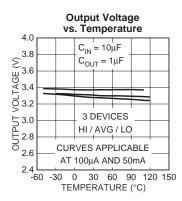
Thormal Pogulation



TIME (ms)







Short Circuit Current ys. Temperature 180 140 120 120 100 60 -30 0 30 60 90 120 150 TEMPERATURE (°C)

0 1 2 3 4 5 6 7 SUPPLY VOLTAGE (V)

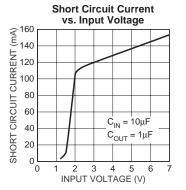
**Ground Current** 

vs. Supply Voltage

 $I_L = 50 \text{mA}$ 

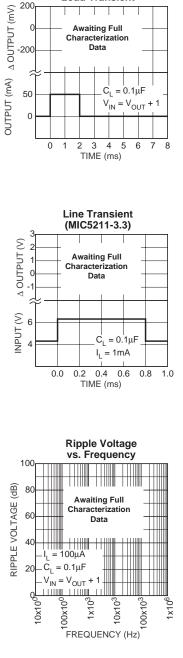
<sub>OUT</sub> = 3.3∖

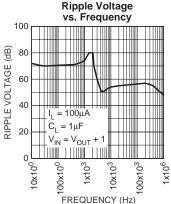
100µA

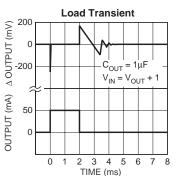


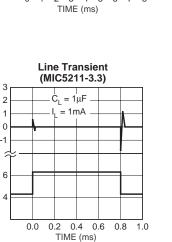
Section 5: Data Sheets

Load Transient









**Ripple Voltage** 

vs. Frequency

Awaiting Full

Characterization

Data

00x10<sup>3</sup>

1×10<sup>6</sup>

10x10<sup>3</sup>

.I<sub>L</sub> = 1mA  $C_{L} = 0.1 \mu F$ 

00×10<sup>C</sup>

 $V_{IN} = V_{OUT} + 1$ 

Tuii 1100 1100

1x10<sup>5</sup>

FREQUENCY (Hz)

A OUTPUT (V)

INPUT (V)

100

6

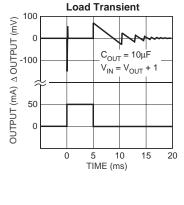
4(

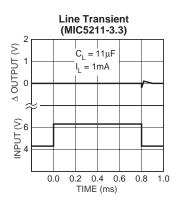
20

10×10<sup>0</sup>

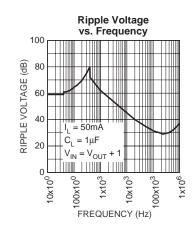
(dB)

**RIPPLE VOLTAGE** 

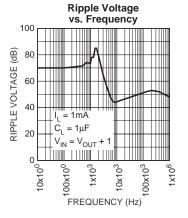


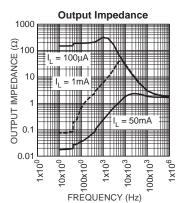


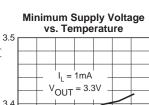
**Ripple Voltage** vs. Frequency 100 (qB) Awaiting Full **RIPPLE VOLTAGE** Characterization 60 Data 40 ++++++  $I_L = 50 \text{mA}$  $C_L = 0.1 \mu F$ 20  $V_{IN} = V_{OUT} + 1$ 10x10<sup>0</sup> 1×10<sup>6</sup> 1×10<sup>3</sup> 00×10<sup>C</sup> 10x10<sup>3</sup> 00x10<sup>3</sup> FREQUENCY (Hz)

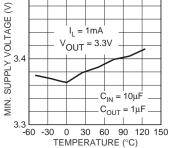


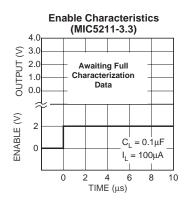
**Ripple Voltage** 

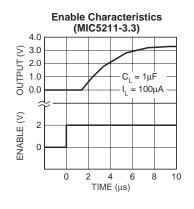


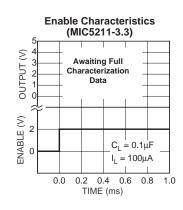


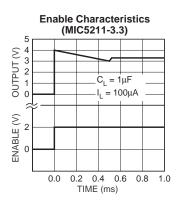




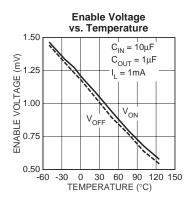


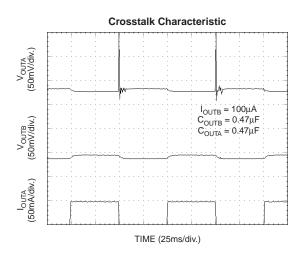






**Enable Current** vs. Temperature 40  $\dot{C}_{IN} = 10 \mu F$ ENABLE CURRENT (µA)  $C_{OUT} = 1 \mu F$  $I_L = 1mA$ 30 20 V<sub>EN</sub> = 5V  $V_{EN} = 2V$ 10 0 -60 0 0 30 60 90 120 150 TEMPERATURE (°C) -30





**Section 5: Data Sheets** 

### **Applications Information**

#### Enable/Shutdown

ENA and ENB (enable/shutdown) may be controlled separately. Forcing ENA/B high (>2V) enables the regulator. The enable inputs typically draw only  $15\mu$ A.

While the logic threshold is TTL/CMOS compatible, ENA/B may be forced as high as 20V, independent of V<sub>IN</sub>. ENA/B may be connected to the supply if the function is not required.

#### **Input Capacitor**

A  $0.1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or when a battery is used as the input.

### **Output Capacitor**

Typical PNP based regulators require an output capacitor to prevent oscillation. The MIC5211 is ultrastable, requiring only  $0.1\mu$ F of output capacitance per regulator for stability. The regulator is stable with all types of capacitors, including the tiny, low-ESR ceramic chip capacitors. The output capacitor value can be increased without limit to improve transient response.

The capacitor should have a resonant frequency above 500kHz. Ceramic capacitors work, but some dielectrics have poor temperature coefficients, which will affect the value of the output capacitor over temperature. Tantalum capacitors are much more stable over temperature, but typically are larger and more expensive. Aluminum electrolytic capacitors will also work, but they have electrolytes that freeze at about  $-30^{\circ}$ C. Tantalum or ceramic capacitors are recommended for operation below  $-25^{\circ}$ C.

### **No-Load Stability**

The MIC5211 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

### **Thermal Shutdown**

Thermal shutdown is independent on both halves of the dual MIC5211, however, an overtemperature condition in one half may affect the other half because of proximity.

#### **Thermal Considerations**

When designing with a dual low-dropout regulator, both sections must be considered for proper operation. The part is designed with thermal shutdown, therefore, the maximum junction temperature must not be exceeded. Since the dual regulators share the same substrate, the total power dissipation must be considered to avoid thermal shutdown. Simple thermal calculations based on the power dissipation of both regulators will allow the user to determine the conditions for proper operation.

The maximum power dissipation for the total regulator system can be determined using the operating temperatures and the thermal resistance of the package. In a minimum footprint configuration, the SOT-23-6 junction-to-ambient thermal resistance ( $\theta_{JA}$ ) is 220°C/W. Since the maximum junction temperature for this device is 125°C, at an operating temperature of 25°C the maximum power dissipation is:

$$P_{D(max)} = \frac{T_{J(max)} - T_{A}}{\theta_{JA}}$$

$$P_{D(max)} = \frac{125^{\circ}C - 25^{\circ}C}{220^{\circ}C/W}$$

 $P_{D(max)} = 455 mW$ 

The MIC5211-3.0 can supply 3V to two different loads independently from the same supply voltage. If one of the regulators is supplying 50mA at 3V from an input voltage of 4V, the total power dissipation in this portion of the regulator is:

$$P_{D1} = (V_{IN} - V_{OUT})I_{OUT} + V_{IN} \cdot I_{GND}$$
$$P_{D1} = (4V - 3V)50mA + 4V \cdot 0.85mA$$
$$P_{D1} = 53.4mW$$

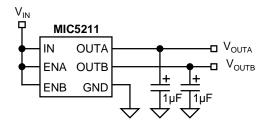
Up to approximately 400mW can be dissipated by the remaining regulator (455mW - 53.4mW) before reaching the thermal shutdown temperature, allowing up to 50mA of current.

$$P_{D2} = (V_{IN} - V_{OUT})I_{OUT} + V_{IN} \cdot I_{GND}$$
$$P_{D2} = (4V - 3V)50mA + 4V \cdot 0.85mA$$
$$P_{D2} = 53.4mW$$

The total power dissipation is:

 $P_{D1} + P_{D2} = 53.4 \text{mW} + 53.4 \text{mW}$  $P_{D1} + P_{D2} = 106.8 \text{mW}$ 

Therefore, with a supply voltage of 4V, both outputs can operate safely at room temperature and full load (50mA).



**Figure 1. Thermal Conditions Circuit** 

In many applications, the ambient temperature is much higher. By recalculating the maximum power dissipation at 70°C ambient, it can be determined if both outputs can supply full load when powered by a 4V supply.

$$P_{D(max)} = \frac{T_{J(max)} - T_{A}}{\theta_{JA}}$$
$$P_{D(max)} = \frac{125^{\circ}C - 70^{\circ}C}{220^{\circ}C/W}$$

$$P_{D(max)} = 250 mW$$

At 70°C, the device can provide 250mW of power dissipation, suitable for the above application.

When using supply voltages higher than 4V, do not exceed the maximum power dissipation for the device. If the device

is operating from a 7.2V-nominal two-cell lithium-ion battery and both regulators are dropping the voltage to 3.0V, then output current will be limited at higher ambient temperatures.

For example, at 70°C ambient the first regulator can supply 3.0V at 50mA output from a 7.2V supply; however, the second regulator will have limitations on output current to avoid thermal shutdown. The dissipation of the first regulator is:

 $P_{D1} = (7.2V - 3V)50mA + 7.2V \cdot 0.85mA$  $P_{D1} = 216mW$ 

Since maximum power dissipation for the dual regulator is 250mW at 70°C, the second regulator can only dissipate up to 34mW without going into thermal shutdown. The amount of current the second regulator can supply is:

$$P_{D2(max)} = 34mW$$

$$(7.2V - 3V)I_{OUT2(max)} = 34mW$$

$$4.2V \cdot I_{OUT2(max)} = 34mW$$

$$I_{OUT2(max)} = 8mA$$

The second regulator can provide up to 8mA output current, suitable for the keep-alive circuitry often required in handheld applications.

Refer to Application Hint 17 for heat sink requirements when higher power dissipation capability is needed. Refer to *Designing with Low Dropout Voltage Regulators* for a more thorough discussion of regulator thermal characteristics.

#### **Dual-Voltage Considerations**

For configurations where two different voltages are needed in the system, the MIC5211 has the option of having two independent output voltages from the same input. For example, a 3.3V rail and a 5.0V rail can be supplied from the MIC5211 for systems that require both voltages. Important considerations must be taken to ensure proper functionality of the part. The input voltage must be high enough for the 5V section to operate correctly, this will ensure the 3.3V section proper operation as well.

Both regulators live off of the same input voltage, therefore the amount of output current each regulator supplies may be limited thermally. The maximum power the MIC5211 can dissipate at room temperature is 455mW, as shown in the "Thermal Considerations" section. If we assume 6V input voltage and 50mA of output current for the 3.3V section of the regulator, then the amount of output current the 5V section can provide can be calculated based on the power dissipation.

$$\begin{split} \mathsf{P}_{\mathsf{D}} &= (\mathsf{V}_{\mathsf{GND}} - \mathsf{V}_{\mathsf{OUT}}) \, \mathsf{I}_{\mathsf{OUT}} + \mathsf{V}_{\mathsf{GND}} \cdot \mathsf{I}_{\mathsf{GND}} \\ \mathsf{P}_{\mathsf{D}(3.3\mathsf{V})} &= (\mathsf{6V} - 3.3\mathsf{V}) \, \mathsf{50\mathsf{mA}} + \mathsf{6V} \cdot \mathsf{0.85\mathsf{mA}} \\ \mathsf{P}_{\mathsf{D}(3.3\mathsf{V})} &= 140.1\mathsf{mW} \\ \mathsf{P}_{\mathsf{D}(\mathsf{max})} &= 455\mathsf{mW} \\ \mathsf{P}_{\mathsf{D}(\mathsf{max})} - \mathsf{P}_{\mathsf{D}(3.3\mathsf{V})} &= \mathsf{P}_{\mathsf{D}(\mathsf{5V})} \end{split}$$

 $P_{D(5V)} = 455mW - 140.1mW$  $P_{D(5V)} = 314.9mW$ 

Based on the power dissipation allowed for the 5V section, the amount of output current it can source is easily calculated.

 $P_{D(5V)} = 314.9mW$ 314.9mW = (6V - 5V) I<sub>MAX</sub> - 6V · I<sub>GND</sub>

 $(I_{GND}$  typically adds less than 5% to the total power dissipation and in this case can be ignored)

 $I_{MAX} = 314.9 \text{mA}$ 

 $I_{MAX}$  exceeds the maximum current rating of the device. Therefore, for this condition, the MIC5211 can supply 50mA of output current from each section of the regulator.



# **MIC5216**

500mA-Peak Output LDO Voltage Regulator

### **Preliminary Information**

## **General Description**

The MIC5216 is an efficient linear voltage regulator with high peak output current capability, very low dropout voltage, and better than 1% output voltage accuracy. Dropout is typically 10mV at light loads and less than 500mV at full load.

The MIC5216 is designed to provide a peak output current for startup conditions where higher inrush current is demanded. It features a 500mA peak output rating. Continuous output current is limited only by package and layout.

The MIC5216 has an internal undervoltage monitor with a flag output. It also can be enabled or shutdown by a CMOS or TTL compatible signal. When disabled, power consumption drops nearly to zero. Dropout ground current is minimized to help prolong battery life. Other key features include reversedbattery protection, current limiting, overtemperature shutdown, and low noise performance.

The MIC5216 is available in fixed output voltages in spacesaving SOT-23-5 and MM8<sup>TM</sup> 8-lead power MSOP packages. For higher power requirements see the MIC5209 or MIC5237.

### Features

- Error Flag indicates undervoltage fault
- Guaranteed 500mA-peak output over the full operating temperature range
- · Low 500mV maximum dropout voltage at full load
- Extremely tight load and line regulation
- Tiny SOT-23-5 and MM8<sup>™</sup> power MSOP-8 package
- Low-noise output
- Low temperature coefficient
- Current and thermal limiting
- Reversed-battery protection
- CMOS/TTL-compatible enable/shutdown control
- Near-zero shutdown current

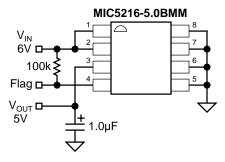
### Applications

- · Laptop, notebook, and palmtop computers
- Cellular telephones and battery-powered equipment
- Consumer and personal electronics
- PC Card  $V_{CC}$  and  $V_{PP}$  regulation and switching
- SMPS post-regulator/dc-to-dc modules
- High-efficiency linear power supplies

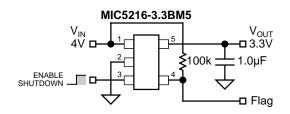
## Ordering Information

Part Number	Marking	Volts	Junction Temp. Range	Package
MIC5216-3.0BMM	—	3.0V	–40°C to +125°C	MSOP-8
MIC5216-3.3BMM	—	3.3V	–40°C to +125°C	MSOP-8
MIC5216-3.6BMM	—	3.6V	–40°C to +125°C	MSOP-8
MIC5216-5.0BMM	—	5.0V	–40°C to +125°C	MSOP-8
MIC5216-3.0BM5	LH30	3.0V	–40°C to +125°C	SOT-23-5
MIC5216-3.3BM5	LH33	3.3V	–40°C to +125°C	SOT-23-5
MIC5216-3.6BM5	LH36	3.6V	–40°C to +125°C	SOT-23-5
MIC5216-5.0BM5	LH50	5.0V	–40°C to +125°C	SOT-23-5

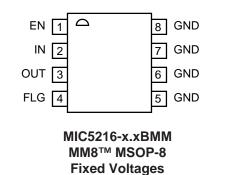
# **Typical Applications**

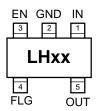


5V Low-Noise Regulator



3.3V Low-Noise Regulator





MIC5216-x.xBM5 SOT-23-5 Fixed Voltages

## **Pin Description**

Pin No. MSOP-8	Pin No. SOT-23-5	Pin Name	Pin Function
2	1	IN	Supply Input
5–8	2	GND	Ground: MSOP-8 pins 5 through 8 are internally connected.
3	5	OUT	Regulator Output
1	3	EN	Enable (Input): CMOS compatible control input. Logic high = enable; logic low or open = shutdown.
4	4	FLG	Error Flag (Output): Open-Collector output. Active low indicates an output undervoltage condition.

## **Absolute Maximum Ratings**

Supply Input Voltage (VIN)	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited
Junction Temperature (T <sub>J</sub> )	40°C to +125°C
Lead Temperature (Solder	ing, 5 sec.) 260°C

## **Operating Ratings**

Supply Input Voltage (V <sub>IN</sub> )	+2.5V to +12V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Package Thermal Resistance	see Note 1

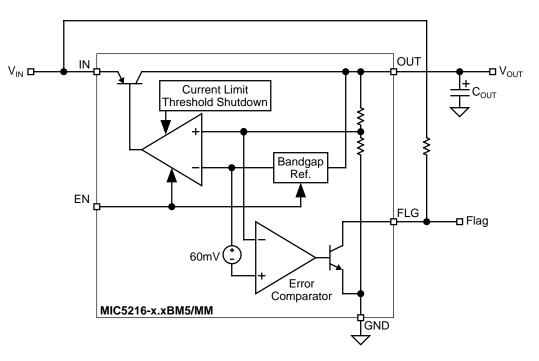
## **Electrical Characteristics**

$V_{IN} = V_{OUT} + 1.0V; C_{OUT} = 4.7\mu F, I_{OUT} =$	100. A.T. 25°C hald values indicate	4000 < T < 1000 uplace noted
$V_{IN} \equiv V_{OUT} \pm 1.0V$ , $V_{OUT} \equiv 4.7 \mu$ F, $I_{OUT} \equiv$	= $1000A$ , $1_1 = 25^{\circ}C$ , <b>bold</b> values indicate	$-40^{\circ}$ $C \leq 1_{1} \leq \pm 123^{\circ}$ $C$ . Unless noted.

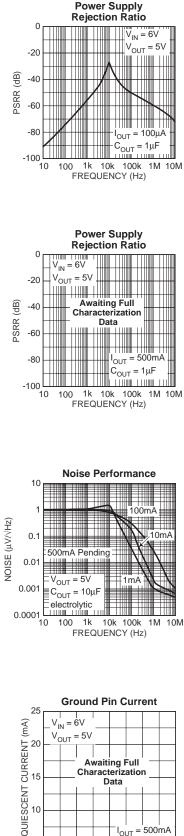
Symbol	Parameter	Conditions	Min	Typical	Мах	Units
V <sub>OUT</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-1 -2		1 <b>2</b>	% %
ΔV <sub>OUT</sub> /ΔT	Output Voltage Temperature Coefficient	Note 2		40		ppm/°C
$\Delta V_{OUT} / V_{OUT}$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 12V		0.009	0.05 <b>0.1</b>	%/V
$\Delta V_{OUT} / V_{OUT}$	Load Regulation	I <sub>OUT</sub> = 100μA to 500mA <b>Note 3</b>		0.05	0.5 <b>0.7</b>	%
V <sub>IN</sub> – V <sub>OUT</sub>	V <sub>IN</sub> – V <sub>OUT</sub> Dropout Voltage, <b>Note 4</b>	I <sub>OUT</sub> = 100μA		10	60 <b>80</b>	mV
	I <sub>OUT</sub> = 50mA		115	175 <b>250</b>	mV	
		I <sub>OUT</sub> = 150mA		165	300 <b>400</b>	mV
		I <sub>OUT</sub> = 500mA		300	500 <b>600</b>	mV
I <sub>GND</sub>	GND Ground Pin Current, <b>Notes 5, 6</b>	$V_{EN} \ge 3.0V, I_{OUT} = 100\mu A$		80	130 <b>170</b>	μA
	$V_{EN} \ge 3.0V, I_{OUT} = 50mA$		350	650 <b>900</b>	μΑ	
	$V_{EN} \ge 3.0V, I_{OUT} = 150mA$		1.8	2.5 <b>3.0</b>	mA	
	$V_{EN} \ge 3.0V, I_{OUT} = 500 \text{mA}$		8	20 <b>25</b>	mA	
	Ground Pin Quiescent Current,	$V_{EN} \le 0.4V$		0.05	3	μΑ
	Note 6	V <sub>EN</sub> ≤ 0.18V		0.10	8	μΑ
PSRR	Ripple Rejection	f = 120Hz		75		dB
I <sub>LIMIT</sub>	Current Limit	V <sub>OUT</sub> = 0V		700	1000	mA
$\Delta V_{OUT} / \Delta P_D$	Thermal Regulation	Note 7		0.05		%/W
e <sub>no</sub>	Output Noise	I <sub>OUT</sub> = 50mA, C <sub>OUT</sub> = 2.2μF		500		nV/√Hz
ENABLE Inp	ut		I			<u> </u>
V <sub>ENL</sub>	Enable Input Voltage	V <sub>EN</sub> = logic low (regulator shutdown)			0.4 <b>0.18</b>	V
V <sub>ENH</sub>		V <sub>EN</sub> = logic high (regulator enabled)	2.0			V
I <sub>ENL</sub>	Enable Input Current	$V_{ENL} \le 0.4V$		0.01	-1	μΑ
		$V_{\text{ENL}} \le 0.18 \text{V}$		0.01	-2	μΑ
I <sub>ENH</sub>		$V_{ENH} \ge 2.0V$		5	20 <b>25</b>	μΑ
Error Flag O	utput	- <b>·</b>				·
V <sub>ERR</sub>	Flag Threshold	undervoltage condition (below nominal)		-5	-8	%
V <sub>IL</sub>	Output Logic-Low Voltage	I <sub>L</sub> = 1mA, undervoltage condition		0.2	0.4	V
I <sub>FL</sub>	Flag Leakage Current	flag off, V <sub>FLAG</sub> = 0V to 12V		0.1	+1	μA

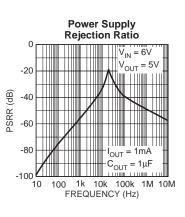
- **Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its operating ratings. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{D(max)} = (T_{J(max)} T_A) + \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. See Table 1 and the "Thermal Considerations" section for details.
- Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.
- **Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 100mA to 500mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.
- Note 4: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.
- Note 5: Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.
- **Note 6:** V<sub>EN</sub> is the voltage externally applied to devices with the EN (enable) input pin.
- **Note 7:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 500mA load pulse at  $V_{IN} = 12V$  for t = 10ms.

## **Block Diagrams**



**MIC5216 Fixed Regulator with External Components** 





**Power Supply Ripple Rejection** vs. Voltage Drop 60 500mA pending <u>ଜ</u>୍ଜ 50 040 30 20 20 1mA 10mA = 100mA OUT RIPPL 10 COUT -1μF 0 0 0.1 0.2 0.3 0.4 VOLTAGE DROP (V)

**Ground Pin Current** 

Awaiting Full

Characterization

10

LOAD CURRENT (mA)

Data

500

100

100

10

1

0.1

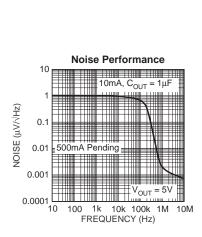
0.01

0.1

QUIESCENT CURRENT (mA)

 $V_{IN} = 6V$ 

V<sub>OUT</sub> = 5V



**Power Supply** 

**Rejection Ratio** 

= 100m/

100k 1M 10M

OUT

FREQUENCY (Hz)

 $C_{OUT} = 1 \mu F$ 

0

-20

-40

-60

-80

-100

10 100

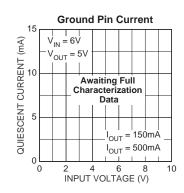
PSRR (dB)

V<sub>IN</sub> = 6V

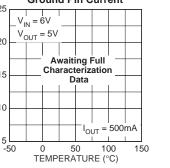
V<sub>OUT</sub> = 5V

1k 10k

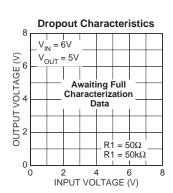
**Ground Pin Current** 1.0  $V_{IN} = 6V$ (mA)  $V_{OUT} = 5V$ 0.8 CURRENT Awaiting Full 0.6 Characterization Data 0.4 ONIESCENT 0.2 I<sub>OUT</sub> = 100μA 0 -50 50 100 150 0 TEMPERATURE (°C)

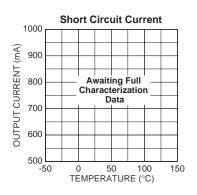


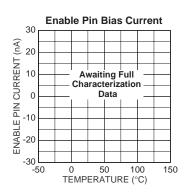
Micrel

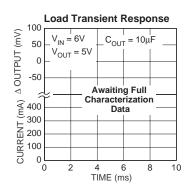


**Ground Pin Current** 300  $V_{IN} = 6V$ QUIESCENT CURRENT (µA) 00 00  $V_{OUT} = 5V$ Awaiting Full Characterization Data  $I_{OUT} = 100 \mu A$ 0 0 2 4 6 8 10 INPUT VOLTAGE (V)





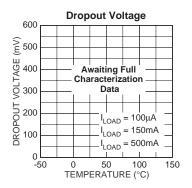


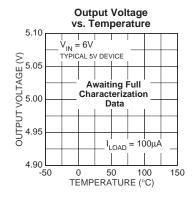




V<sub>IN</sub> = 6V

 $V_{OUT} = 5V$ 





Line Transient

Awaiting Full

Characterization

Data

400 600

TIME (µs)

**Enable Pin Delay** 

Awaiting Full

Characterization Data

 $C_{OUT} = 1\mu F$ 

 $I_{OUT} = 10 \text{m}A$ 

6

8

10

 $C_{OUT} = 1\mu F$ 

 $I_{LOAD} = 1 \text{mA}$ 

800 1000

 $V_{OUT} = 5V$ 

300

200

100

0

8

6

4

2.0

(\\\\_\_\_\_\_) 1.5 1.0 1.0 1.0 1.0 0.5

INPUT (V)

Δ

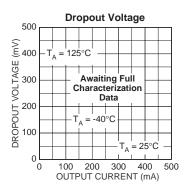
2

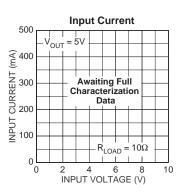
0

0 200

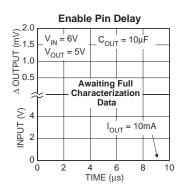
∆ OUTPUT (mV)

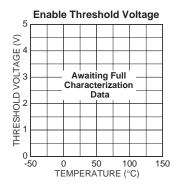
INPUT (V)

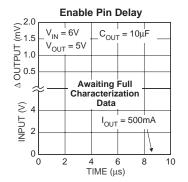


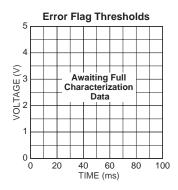


Load Transient Response 100 CURRENT (mA) A OUTPUT (mV)  $V_{OUT} = 5V$  $C_{OUT} = 1\mu F$ 50  $V_{IN} = 6V$ 0 -50 Awaiting Full Characterization Data 400 300 200 100 0 0 2 8 10 4 6 TIME (µs)









## **Applications Information**

The MIC5216 is designed for 150mA to 200mA output current applications where a high current spike (500mA) is needed for short, startup conditions. Basic application of the device will be discussed initially followed by a more detailed discussion of higher current applications.

#### Enable/Shutdown

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic. If the enable/ shutdown feature is not required, connect EN to IN (supply input). See Figure 5.

#### Input Capacitor

A  $1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

#### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation.  $1\mu$ F minimum is recommended. Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (equivalent series resistance) of about  $5\Omega$  or less and a resonant frequency above 1MHz. Ultralow-ESR capacitors could cause oscillation and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but more expensive. Many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, so solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is needed for stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

### **No-Load Stability**

The MIC5216 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

#### **Error Flag Ouput**

The error flag is an open-collector output and is active (low) when an undervoltage of approximately 5% below the nominal output voltage is detected. A pullup resistor from IN to FLAG is shown in all schematics.

If an error indication is not required, FLAG may be left open and the pullup resistor may be omitted.

### **Thermal Considerations**

The MIC5216 is designed to provide 200mA of continuous current in two very small profile packages. Maximum power dissipation can be calculated based on the output current and the voltage drop across the part. To determine the maximum power dissipation of the package, use the thermal resistance, junction-to-ambient, of the device and the following basic equation.

$$P_{D(MAX)} = \frac{\left(T_{J(MAX)} - T_{A}\right)}{\theta_{IA}}$$

 $T_{J(MAX)}$  is the maximum junction temperature of the die, 125°C, and  $T_A$  is the ambient operating temperature.  $\theta_{JA}$  is layout dependent; table 1 shows examples of thermal resistance, junction-to-ambient, for the MIC5216.

Package	θ <sub>JA</sub> Recommended Minimum Footprint	θ <sub>JA</sub> 1" Square Copper Clad	θ <sub>JC</sub>
MM8™ (MM)	160°C/W	70°C/W	30°C/W
SOT-23-5 (M5)	220°C/W	170°C/W	130°C/W

#### Table 1. MIC5216 Thermal Resistance

The actual power dissipation of the regulator circuit can be determined using one simple equation.

$$P_{D} = (V_{IN} - V_{OUT}) I_{OUT} + V_{IN} I_{GND}$$

Substituting  $P_{D(MAX)}$  for  $P_D$  and solving for the operating conditions that are critical to the application will give the maximum operating conditions for the regulator circuit. For example, if we are operating the MIC5216-3.3BM5 at room temperature, with a minimum footprint layout, we can determine the maximum input voltage for a set output current.

$$P_{D(MAX)} = \frac{(125^{\circ}C - 25^{\circ}C)}{220^{\circ}C/W}$$

 $P_{D(MAX)} = 455 \text{mW}$ 

The thermal resistance, junction-to-ambient, for the minimum footprint is 220°C/W, taken from table 1. The maximum power dissipation number cannot be exceeded for proper operation of the device. Using the output voltage of 3.3V, and an output current of 150mA, we can determine the maximum input voltage. Ground current, maximum of 3mA for 150mA of output current, can be taken from the Electrical Characteristics section of the data sheet.

$$\begin{split} &455\text{mW} = (\text{V}_{\text{IN}} - 3.3\text{V}) \ 150\text{mA} + \text{V}_{\text{IN}} \times 3\text{mA} \\ &\text{V}_{\text{IN}} \left( \frac{455\text{mW} + 3.3\text{V} \ (150\text{mA})}{150\text{mA} + 3\text{mA}} \right) \\ &\text{V}_{\text{IN}} \ = \ 6.2\text{V}_{\text{MAX}} \end{split}$$

Therefore, a 3.3V application at 150mA of output current can accept a maximum input voltage of 6.2V in a SOT-23-5 package. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to the Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.

### **Peak Current Applications**

The MIC5216 is designed for applications where high startup currents are demanded from space constrained regulators. This device will deliver 500mA start-up current from a SOT-23-5 or MM8 package, allowing high power from a very low profile device. The MIC5216 can subsequently provide output current that is only limited by the thermal characteristics of the device. You can obtain higher continuous currents from the device with the proper design. This is easily proved with some thermal calculations.

If we look at a specific example, it may be easier to follow. The MIC5216 can be used to provide up to 500mA continuous

output current. First, calculate the maximum power dissipation of the device, as was done in the thermal considerations section. Worst case thermal resistance ( $\theta_{JA} = 220^{\circ}C/W$  for the MIC5216-x.xBM5), will be used for this example.

$$P_{D(MAX)} = \frac{\left(T_{J(MAX)} - T_{A}\right)}{\theta_{JA}}$$

Assuming room temperature, we have a maximum power dissipation number of

$$P_{D(MAX)} = \frac{(125^{\circ}C - 25^{\circ}C)}{220^{\circ}C/W}$$
$$P_{D} = 455mW$$

520mA

Then we can determine the maximum input voltage for a fivevolt regulator operating at 500mA, using worst case ground current.

$$\begin{split} \mathsf{P}_{\mathsf{D}(\mathsf{max})} &= 455 \mathsf{mW} = (\mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}}) \, \mathsf{I}_{\mathsf{OUT}} + \mathsf{V}_{\mathsf{IN}} \, \mathsf{I}_{\mathsf{GND}} \\ \mathsf{I}_{\mathsf{OUT}} &= 500 \mathsf{mA} \\ \mathsf{V}_{\mathsf{OUT}} &= 5\mathsf{V} \\ \mathsf{I}_{\mathsf{GND}} &= 20 \mathsf{mA} \\ 455 \mathsf{mW} &= (\mathsf{V}_{\mathsf{IN}} - 5\mathsf{V}) \, 500 \mathsf{mA} + \mathsf{V}_{\mathsf{IN}} \times 20 \mathsf{mA} \\ 2.995 \mathsf{W} &= 520 \mathsf{mA} \times \mathsf{V}_{\mathsf{IN}} \\ \mathsf{V}_{\mathsf{IN}(\mathsf{max})} &= \frac{2.955 \mathsf{W}}{520 \mathsf{mA}} = 5.683 \mathsf{V} \end{split}$$

Therefore, to be able to obtain a constant 500mA output current from the 5216-5.0BM5 at room temperature, you need extremely tight input-output voltage differential, barely above the maximum dropout voltage for that current rating.

You can run the part from larger supply voltages if the proper precautions are taken. Varying the duty cycle using the enable pin can increase the power dissipation of the device by maintaining a lower average power figure. This is ideal for applications where high current is only needed in short bursts. Figure 1 shows the safe operating regions for the MIC5216-x.xBM5 at three different ambient temperatures and at different output currents. The data used to determine this figure assumed a minimum footprint PCB design for minimum heat sinking. Figure 2 incorporates the same factors as the first figure, but assumes a much better heat sink. A 1"square copper trace on the PC board reduces the thermal resistance of the device. This improved thermal resistance improves power dissipation and allows for a larger safe operating region.

Figures 3 and 4 show safe operating regions for the MIC5216x.xBMM, the power MSOP package part. These graphs show three typical operating regions at different temperatures. The lower the temperature, the larger the operating region. The graphs were obtained in a similar way to the graphs for the MIC5216-x.xBM5, taking all factors into consideration and using two different board layouts, minimum footprint and 1" square copper PC board heat sink. (For further discussion of PC board heat sink characteristics, refer to Application Hint 17, "Designing PC Board Heat Sinks".

The information used to determine the safe operating regions can be obtained in a similar manner to that used in determining typical power dissipation, already discussed. Determining the maximum power dissipation based on the layout is the first step, this is done in the same manner as in the previous two sections. Then, a larger power dissipation number multiplied by a set maximum duty cycle would give that maximum power dissipation number for the layout. This is best shown through an example. If the application calls for 5V at 500mA for short pulses, but the only supply voltage available is 8V, then the duty cycle has to be adjusted to determine an average power that does not exceed the maximum power dissipation for the layout.

$$Avg.P_{D} = \left(\frac{\% DC}{100}\right) \left(V_{IN} - V_{OUT}\right) I_{OUT} + V_{IN} I_{GND}$$

$$455mW = \left(\frac{\% DC}{100}\right) (8V - 5V) 500mA + 8V \times 20mA$$

$$455mW = \left(\frac{\% Duty Cycle}{100}\right) 1.66W$$

$$0.274 = \frac{\% Duty Cycle}{100}$$

% Duty Cycle Max = 27.4%

With an output current of 500mA and a three-volt drop across the MIC5216-xxBMM, the maximum duty cycle is 27.4%.

Applications also call for a set nominal current output with a greater amount of current needed for short durations. This is a tricky situation, but it is easily remedied. Calculate the average power dissipation for each current section, then add the two numbers giving the total power dissipation for the regulator. For example, if the regulator is operating normally at 50mA, but for 12.5% of the time it operates at 500mA output, the total power dissipation of the part can be easily determined. First, calculate the power dissipation of the device at 50mA. We will use the MIC5216-3.3BM5 with 5V input voltage as our example.

$$P_{D} \times 50mA = (5V - 3.3V) \times 50mA + 5V \times 650\muA$$
$$P_{D} \times 50mA = 173mW$$

However, this is continuous power dissipation, the actual on-time for the device at 50mA is (100%-12.5%) or 87.5% of the time, or 87.5% duty cycle. Therefore, PD must be multiplied by the duty cycle to obtain the actual average power dissipation at 50mA.

 $P_D \times 50 \text{mA} = 0.875 \times 173 \text{mW}$ 

$$P_{D} \times 50 mA = 151 mW$$

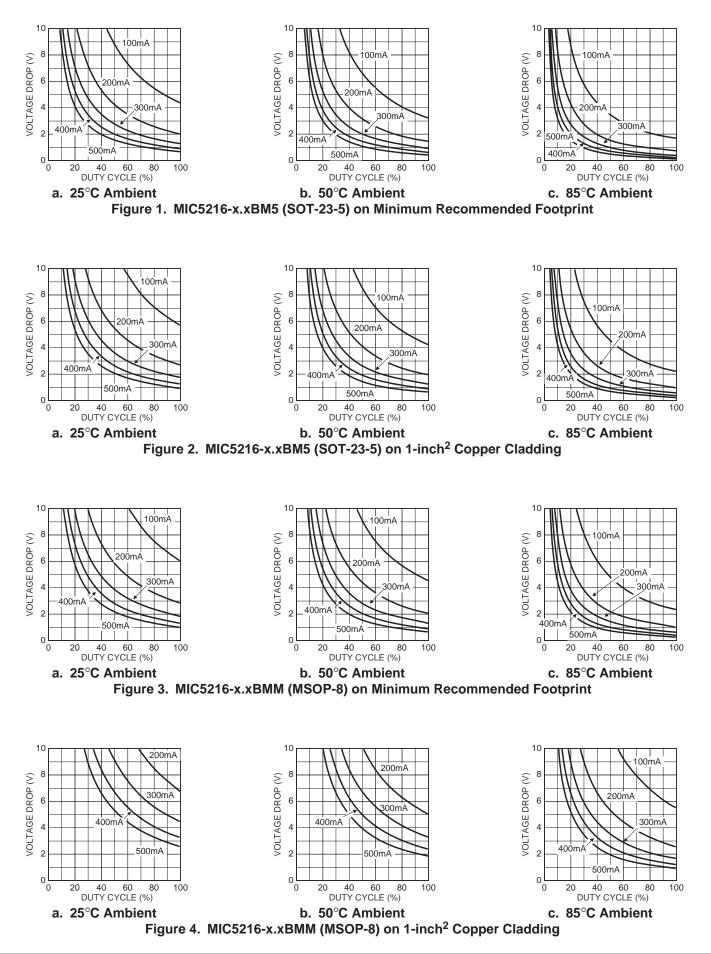
The power dissipation at 500mA must also be calculated.

 $P_{D} \times 500 \text{mA} = (5\text{V} - 3.3\text{V}) 500 \text{mA} + 5\text{V} \times 20 \text{mA}$ 

$$P_D \times 500 \text{mA} = 950 \text{mW}$$

This number must be multiplied by the duty cycle at which it would be operating, 12.5%.

$$P_D \times = 0.125 \times 950 \text{mW}$$
  
 $P_D \times = 119 \text{mW}$ 



The total power dissipation of the device under these conditions is the sum of the two power dissipation figures.

 $P_{D(total)} = P_D \times 50mA + P_D \times 500mA$  $P_{D(total)} = 151mW + 119mW$  $P_{D(total)} = 270mW$ 

The total power dissipation of the regulator is less than the maximum power dissipation of the SOT-23-5 package at room temperature, on a minimum footprint board and therefore would operate properly.

Multilayer boards with a ground plane, wide traces near the pads, and large supply-bus lines will have better thermal conductivity.

For additional heat sink characteristics, please refer to Micrel Application Hint 17, "Designing P.C. Board Heat Sinks", included in Micrel's *Databook*. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.

#### **Fixed Regulator Circuits**

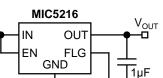


Figure 5. Low-Noise Fixed Voltage Regulator

Figure 5 shows a basic MIC5216-x.xBMx fixed-voltage regulator circuit. A  $1\mu$ F minimum output capacitor is required for basic fixed-voltage applications.

The flag output is an open-collector output and requires a pull-up resistor to the input voltage. The flag indicates an undervoltage condition on the output of the device.



# **MIC5219**

### 500mA-Peak Output LDO Voltage Regulator

### **Preliminary Information**

### **General Description**

The MIC5219 is an efficient linear voltage regulator with high peak output current capability, very low dropout voltage, and better than 1% output voltage accuracy. Dropout is typically 10mV at light loads and less than 500mV at full load.

The MIC5219 is designed to provide a peak output current for startup conditions where higher inrush current is demanded. It features a 500mA peak output rating. Continuous output current is limited only by package and layout.

The MIC5219 can be enabled or shut down by a CMOS or TTL compatible signal. When disabled, power consumption drops nearly to zero. Dropout ground current is minimized to help prolong battery life. Other key features include reversedbattery protection, current limiting, overtemperature shutdown, and low noise performance with an ultra-low-noise option.

The MIC5219 is available in adjustable or fixed output voltages in space-saving SOT-23-5 and MM8<sup>™</sup> 8-lead power MSOP packages. For higher power requirements see the MIC5209 or MIC5237.

### Features

- Guaranteed 500mA-peak output over the full operating temperature range
- Low 500mV maximum dropout voltage at full load
- Extremely tight load and line regulation
- Tiny SOT-23-5 and MM8<sup>™</sup> power MSOP-8 package
- Ultra-low-noise output
- Low temperature coefficient
- · Current and thermal limiting
- Reversed-battery protection
- CMOS/TTL-compatible enable/shutdown control
- Near-zero shutdown current

### Applications

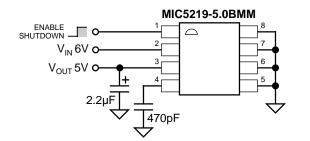
- Laptop, notebook, and palmtop computers
- · Cellular telephones and battery-powered equipment
- Consumer and personal electronics
- PC Card V<sub>CC</sub> and V<sub>PP</sub> regulation and switching
- SMPS post-regulator/dc-to-dc modules
- High-efficiency linear power supplies

### **Ordering Information**

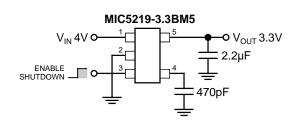
Part Number	Marking	Volts	Junction Temp. Range	Package
MIC5219-3.0BMM	_	3.0V	–40°C to +125°C	MSOP-8
MIC5219-3.3BMM	_	3.3V	–40°C to +125°C	MSOP-8
MIC5219-3.6BMM	_	3.6V	–40°C to +125°C	MSOP-8
MIC5219-5.0BMM	_	5.0V	–40°C to +125°C	MSOP-8
MIC5219BMM	_	Adj.	–40°C to +125°C	MSOP-8
MIC5219-3.0BM5	LG30	3.0V	–40°C to +125°C	SOT-23-5
MIC5219-3.3BM5	LG33	3.3V	–40°C to +125°C	SOT-23-5
MIC5219-3.6BM5	LG36	3.6V	–40°C to +125°C	SOT-23-5
MIC5219-5.0BM5	LG50	5.0V	–40°C to +125°C	SOT-23-5
MIC5219BM5	LGAA	Adj.	–40°C to +125°C	SOT-23-5

Other voltages available. Consult Micrel for details.

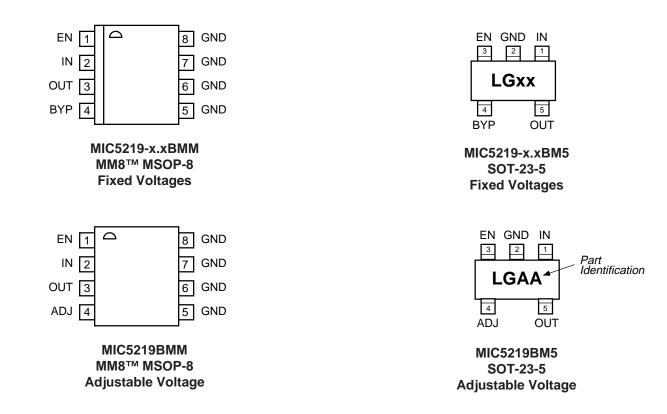
### **Typical Applications**



5V Ultra-Low-Noise Regulator



3.3V Ultra-Low-Noise Regulator



### **Pin Description**

Pin No. MSOP-8	Pin No. SOT-23-5	Pin Name	Pin Function
2	1	IN	Supply Input
5–8	2	GND	Ground: MSOP-8 pins 5 through 8 are internally connected.
3	5	OUT	Regulator Output
1	3	EN	Enable (Input): CMOS compatible control input. Logic high = enable; logic low or open = shutdown.
4 (fixed)	4 (fixed)	BYP	Reference Bypass: Connect external 470pF capacitor to GND to reduce output noise. May be left open.
4 (adj.)	4 (adj.)	ADJ	Adjust (Input): Feedback input. Connect to resistive voltage-divider network.

### Absolute Maximum Ratings

# **Operating Ratings**

Supply Input Voltage (VIN)	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Lead Temperature (Soldering, 5 sec.)	260°C

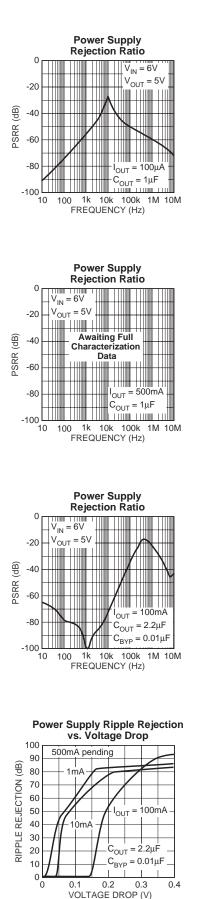
Supply Input Voltage (V <sub>IN</sub> )	+2.5V to +12V
Enable Input Voltage (V <sub>EN</sub> )	0V to V <sub>IN</sub>
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Package Thermal Resistance	see Table 1

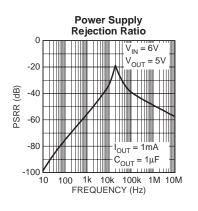
### **Electrical Characteristics**

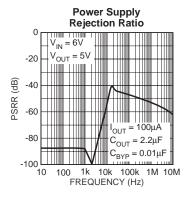
Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>OUT</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-1 -2		1 <b>2</b>	% %
ΔV <sub>OUT</sub> /ΔT	Output Voltage Temperature Coefficient	Note 2		40		ppm/°C
$\Delta V_{OUT} / V_{OUT}$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 12V		0.009	0.05 <b>0.1</b>	%/V
$\Delta V_{OUT} / V_{OUT}$	Load Regulation	I <sub>OUT</sub> = 100μA to 500mA <b>Note 3</b>		0.05	0.5 <b>0.7</b>	%
V <sub>IN</sub> – V <sub>OUT</sub>	Dropout Voltage, Note 4	I <sub>OUT</sub> = 100μA		10	60 <b>80</b>	mV
		I <sub>OUT</sub> = 50mA		115	175 <b>250</b>	mV
		I <sub>OUT</sub> = 150mA		165	300 <b>400</b>	mV
		I <sub>OUT</sub> = 500mA		300	500 <b>600</b>	mV
I <sub>GND</sub> G	Ground Pin Current, Notes 5, 6	$V_{EN} \ge 3.0V, I_{OUT} = 100\mu A$		80	130 <b>170</b>	μΑ
		$V_{EN} \ge 3.0V, I_{OUT} = 50mA$		350	650 <b>900</b>	μΑ
		$V_{EN} \ge 3.0V, I_{OUT} = 150mA$		1.8	2.5 <b>3.0</b>	mA
		$V_{EN} \ge 3.0V, I_{OUT} = 500mA$		8	20 <b>25</b>	mA
	Ground Pin Quiescent Current,	$V_{EN} \le 0.4V$		0.05	3	μΑ
	Note 6	$V_{EN} \le 0.18V$		0.10	8	μΑ
PSRR	Ripple Rejection	f = 120Hz		75		dB
I <sub>LIMIT</sub>	Current Limit	$V_{OUT} = 0V$		700	1000	mA
$\Delta V_{OUT} / \Delta P_{D}$	Thermal Regulation	Note 7		0.05		%/W
e <sub>no</sub>	Output Noise	$I_{OUT} = 50$ mA, $C_{OUT} = 2.2\mu$ F, $C_{BYP} = 0$		500		nV/√Hz
		$I_{OUT} = 50$ mA, $C_{OUT} = 2.2\mu$ F, $C_{BYP} = 470$ pF		300		nV/√Hz
ENABLE Inp	ut					

V <sub>ENL</sub>	Enable Input Logic-Low Voltage	V <sub>EN</sub> = logic low (regulator shutdown)			0.4 <b>0.18</b>	V
		V <sub>EN</sub> = logic high (regulator enabled)	2.0			V
I <sub>ENL</sub>	Enable Input Current	$V_{ENL} \le 0.4V$		0.01	-1	μΑ
		$V_{ENL} \leq 0.18V$		0.01	-2	μΑ
I <sub>ENH</sub>		$V_{ENH} \ge 2.0V$		5	20 <b>25</b>	μA

- **Note 1:** Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its operating ratings. The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_{J(max)}$ , the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is calculated using:  $P_{D(max)} = (T_{J(max)} T_A) + \theta_{JA}$ . Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. See Table 1 and the "Thermal Considerations" section for details.
- Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.
- **Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 100mA to 500mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.
- Note 4: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.
- **Note 5:** Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.
- Note 6: V<sub>EN</sub> is the voltage externally applied to devices with the EN (enable) input pin.
- **Note 7:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 500mA load pulse at  $V_{IN} = 12V$  for t = 10ms.
- Note 8: C<sub>BYP</sub> is an optional, external bypass capacitor connected to devices with a BYP (bypass) or ADJ (adjust) pin.







**Power Supply** 

Rejection Ratio

Awaiting Full

Characterization Data

.....

I<sub>OUT</sub>  $C_{OUT} = 2.2 \mu F$ 

100 1k 10k 100k 1M 10M FREQUENCY (Hz)

= 500mA

 $C_{BYP} = 0.01$ 

/<sub>IN</sub> = 6V

 $V_{OUT} = 5V$ 

-20

-60

-80

-100

10

10

0.1

0.01

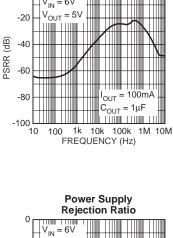
0.001

0.0001

10

NOISE (µV/√Hz)

PSRR (dB) -40

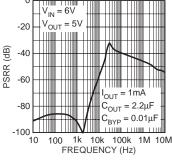


**Power Supply** 

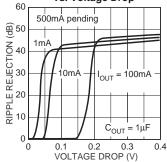
**Rejection Ratio** 

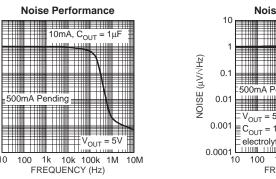
= 6V

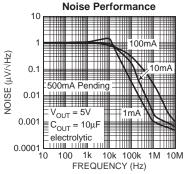
0



Power Supply Ripple Rejection vs. Voltage Drop









NOISE (µV/VHz)

10

1

0.1

0.01

0.001

0.0001

10

1

0.1

0.01

0.001

25

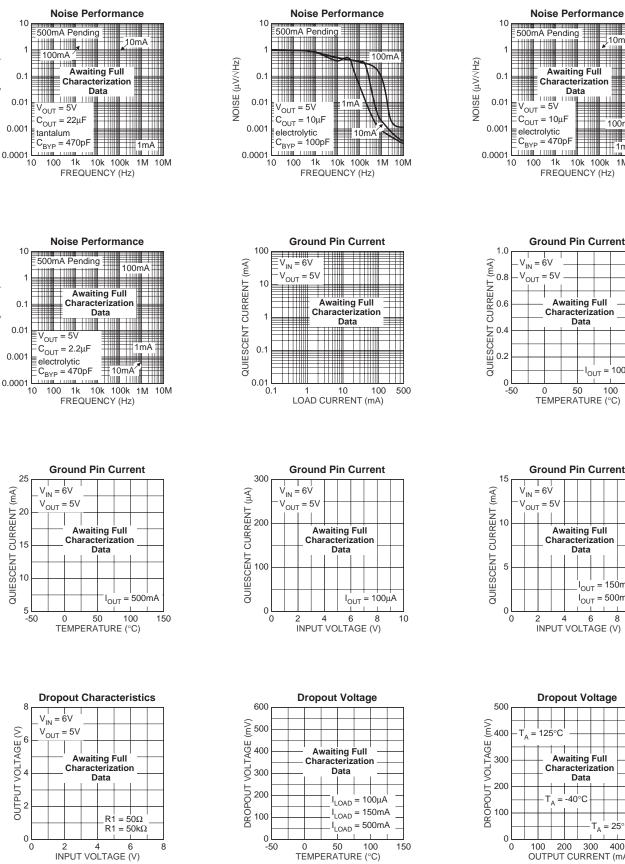
8

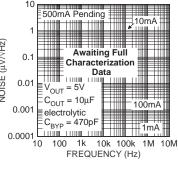
OUTPUT VOLTAGE (V) N P 9

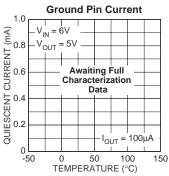
(mA)

NOISE (µV/VHz)

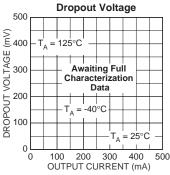
### **Typical Characteristics**



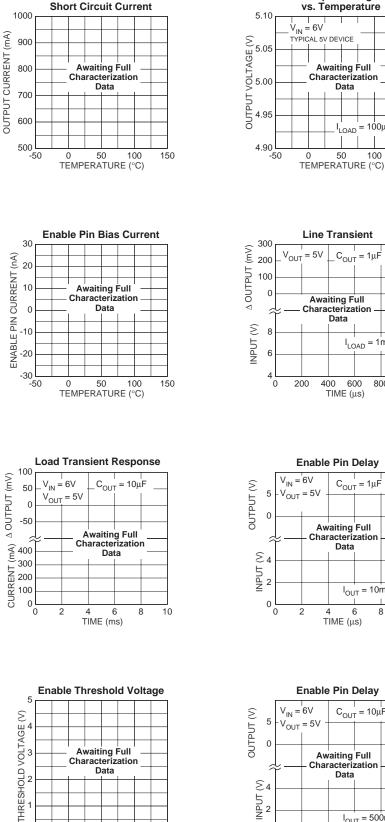


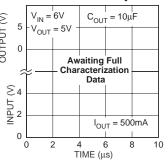


**Ground Pin Current**  $V_{IN} = 6V$  $V_{OUT} = 5V$ Awaiting Full Characterization Data I<sub>OUT</sub> = 150mÅ  $I_{OUT} = 500 \text{mA}$ 6 10 4 8 INPUT VOLTAGE (V)



### **Typical Characteristics**





**Output Voltage** 

Data

50

LOAD = 100μA

 $C_{OUT} = 1\mu F$ 

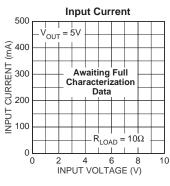
 $I_{LOAD} = 1 mA$ 

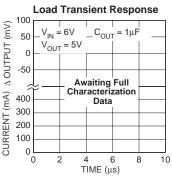
 $C_{OUT} = 1\mu F$ 

800 1000

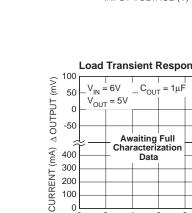
100

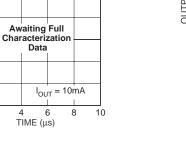
150

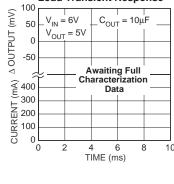




Enable Pin Delay OUTPUT (V) V<sub>IN</sub> = 6V  $C_{OUT} = 10 \mu F$ 5  $V_{OUT} = 5V$ 0 Awaiting Full Characterization Data (>) 4 101 2  $I_{OUT} = 10 \text{mA}$ 0 0 2 4 6 8 10 TIME (µs)







Characterization

Data

0 50 100 TEMPERATURE (°C)

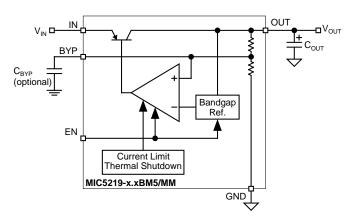
150

**Section 5: Data Sheets** 

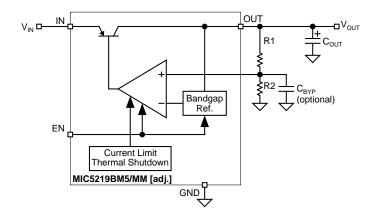
0

-50

### **Block Diagrams**







**Ultra-Low-Noise Adjustable Regulator** 

### **Applications Information**

The MIC5219 is designed for 150mA to 200mA output current applications where a high current spike (500mA) is needed for short, startup conditions. Basic application of the device will be discussed initially followed by a more detailed discussion of higher current applications.

#### Enable/Shutdown

Forcing EN (enable/shutdown) high (> 2V) enables the regulator. EN is compatible with CMOS logic. If the enable/ shutdown feature is not required, connect EN to IN (supply input). See Figure 5.

#### Input Capacitor

A  $1\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

#### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation. The minimum size of the output capacitor is dependent upon whether a reference bypass capacitor is used. 1µF minimum is recommended when  $C_{BYP}$  is not used (see Figure 5). 2.2µF minimum is recommended when  $C_{BYP}$  is 470pF (see Figure 6). For applications <3V, the output capacitor should be increased to 22µF minimum to reduce start-up overshoot. Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (equivalent series resistance) of about  $5\Omega$  or less and a resonant frequency above 1MHz. Ultra-low-ESR capacitors could cause oscillation and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, so solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is needed for stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

#### **No-Load Stability**

The MIC5219 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

#### **Reference Bypass Capacitor**

BYP is connected to the internal voltage reference. A 470pF capacitor ( $C_{BYP}$ ) connected from BYP to GND quiets this reference, providing a significant reduction in output noise (ultra-low-noise performance).  $C_{BYP}$  reduces the regulator phase margin; when using  $C_{BYP}$ , output capacitors of 2.2µF or greater are generally required to maintain stability.

The start-up speed of the MIC5219 is inversely proportional to the size of the reference bypass capacitor. Applications requiring a slow ramp-up of output voltage should consider larger values of  $C_{BYP}$ . Likewise, if rapid turn-on is necessary, consider omitting  $C_{BYP}$ .

#### **Thermal Considerations**

The MIC5219 is designed to provide 200mA of continuous current in two very small profile packages. Maximum power dissipation can be calculated based on the output current and the voltage drop across the part. To determine the maximum power dissipation of the package, use the thermal resistance, junction-to-ambient, of the device and the following basic equation.

$$P_{D(max)} = \frac{\left(T_{J(max)} - T_{A}\right)}{\theta_{JA}}$$

 $T_{J(MAX)}$  is the maximum junction temperature of the die, 125°C, and  $T_A$  is the ambient operating temperature.  $\theta_{JA}$  is layout dependent; table 1 shows examples of thermal resistance, junction-to-ambient, for the MIC5219.

Package	θ <sub>JA</sub> Recommended Minimum Footprint	θ <sub>JA</sub> 1" Square 2 oz. Copper	θ <sup>JC</sup>
MM8™ (MM)	160°C/W	70°C/W	30°C/W
SOT-23-5 (M5)	220°C/W	170°C/W	130°C/W

Table 1. MIC5219 Thermal Resistance

The actual power dissipation of the regulator circuit can be determined using one simple equation.

$$\mathsf{P}_{\mathsf{D}} = (\mathsf{V}_{\mathsf{IN}} - \mathsf{V}_{\mathsf{OUT}}) \mathsf{I}_{\mathsf{OUT}} + \mathsf{V}_{\mathsf{IN}} \mathsf{I}_{\mathsf{GND}}$$

Substituting  $P_{D(MAX)}$  for  $P_D$  and solving for the operating conditions that are critical to the application will give the maximum operating conditions for the regulator circuit. For example, if we are operating the MIC5219-3.3BM5 at room temperature, with a minimum footprint layout, we can determine the maximum input voltage for a set output current.

$$P_{D(max)} = \frac{(125^{\circ}C - 25^{\circ}C)}{220^{\circ}C/W}$$

 $P_{D(max)} = 455 mW$ 

The thermal resistance, junction-to-ambient, for the minimum footprint is 220°C/W, taken from table 1. The maximum power dissipation number cannot be exceeded for proper operation of the device. Using the output voltage of 3.3V, and an output current of 150mA, we can determine the maximum input voltage. Ground current, maximum of 3mA for 150mA of output current, can be taken from the Electrical Characteristics section of the data sheet.

$$\begin{split} 455\text{mW} &= (\text{V}_{\text{IN}} - 3.3\text{V}) \times 150\text{mA} + \text{V}_{\text{IN}} \times 3\text{mA} \\ 455\text{mW} &= (150\text{mA}) \times \text{V}_{\text{IN}} + 3\text{mA} \times \text{V}_{\text{IN}} - 495\text{mW} \\ 950\text{mW} &= 153\text{mA} \times \text{V}_{\text{IN}} \\ \text{V}_{\text{IN}} &= 6.2\text{V}_{\text{MAX}} \end{split}$$

Therefore, a 3.3V application at 150mA of output current can accept a maximum input voltage of 6.2V in a SOT-23-5 package. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to the Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.

#### **Peak Current Applications**

The MIC5219 is designed for applications where high startup currents are demanded from space constrained regulators. This device will deliver 500mA start-up current from a SOT-23-5 or MM8 package, allowing high power from a very low profile device. The MIC5219 can subsequently provide output current that is only limited by the thermal characteristics of the device. You can obtain higher continuous currents from the device with the proper design. This is easily proved with some thermal calculations.

If we look at a specific example, it may be easier to follow. The MIC5219 can be used to provide up to 500mA continuous output current. First, calculate the maximum power dissipation of the device, as was done in the thermal considerations section. Worst case thermal resistance ( $\theta_{JA} = 220^{\circ}C/W$  for the MIC5219-x.xBM5), will be used for this example.

$$\mathsf{P}_{\mathsf{D}(\mathsf{max})} = \frac{\left(\mathsf{T}_{\mathsf{J}(\mathsf{max})} - \mathsf{T}_{\mathsf{A}}\right)}{\theta_{\mathsf{J}\mathsf{A}}}$$

Assuming a 25°C room temperature, we have a maximum power dissipation number of

$$P_{D(max)} = \frac{(125^{\circ}C - 25^{\circ}C)}{220^{\circ}C/W}$$

 $P_{D(max)} = 455 mW$ 

Then we can determine the maximum input voltage for a fivevolt regulator operating at 500mA, using worst case ground current.

$$\begin{split} \mathsf{P}_{\mathsf{D}(\mathsf{max})} &= 455 \mathsf{mW} = (\mathsf{V}_\mathsf{IN} - \mathsf{V}_\mathsf{OUT}) \ \mathsf{I}_\mathsf{OUT} + \mathsf{V}_\mathsf{IN} \ \mathsf{I}_\mathsf{GND} \\ \mathsf{I}_\mathsf{OUT} &= 500 \mathsf{mA} \\ \mathsf{V}_\mathsf{OUT} &= 5\mathsf{V} \\ \mathsf{I}_\mathsf{GND} &= 20 \mathsf{mA} \\ 455 \mathsf{mW} &= (\mathsf{V}_\mathsf{IN} - 5\mathsf{V}) \ 500 \mathsf{mA} + \mathsf{V}_\mathsf{IN} \times 20 \mathsf{mA} \\ 2.995 \mathsf{W} &= 520 \mathsf{mA} \times \mathsf{V}_\mathsf{IN} \end{split}$$

$$V_{IN(max)} = \frac{2.955W}{520mA} = 5.683V$$

Therefore, to be able to obtain a constant 500mA output current from the 5219-5.0BM5 at room temperature, you need extremely tight input-output voltage differential, barely above the maximum dropout voltage for that current rating.

You can run the part from larger supply voltages if the proper precautions are taken. Varying the duty cycle using the enable pin can increase the power dissipation of the device by maintaining a lower average power figure. This is ideal for applications where high current is only needed in short bursts. Figure 1 shows the safe operating regions for the MIC5219-x.xBM5 at three different ambient temperatures and at different output currents. The data used to determine this figure assumed a minimum footprint PCB design for minimum heat sinking. Figure 2 incorporates the same factors as the first figure, but assumes a much better heat sink. A 1" square copper trace on the PC board reduces the thermal resistance of the device. This improved thermal resistance improves power dissipation and allows for a larger safe operating region. Figures 3 and 4 show safe operating regions for the MIC5219x.xBMM, the power MSOP package part. These graphs show three typical operating regions at different temperatures. The lower the temperature, the larger the operating region. The graphs were obtained in a similar way to the graphs for the MIC5219-x.xBM5, taking all factors into consideration and using two different board layouts, minimum footprint and 1" square copper PC board heat sink. (For further discussion of PC board heat sink characteristics, refer to Application Hint 17, "Designing PC Board Heat Sinks".)

The information used to determine the safe operating regions can be obtained in a similar manner to that used in determining typical power dissipation, already discussed. Determining the maximum power dissipation based on the layout is the first step, this is done in the same manner as in the previous two sections. Then, a larger power dissipation number multiplied by a set maximum duty cycle would give that maximum power dissipation number for the layout. This is best shown through an example. If the application calls for 5V at 500mA for short pulses, but the only supply voltage available is 8V, then the duty cycle has to be adjusted to determine an average power that does not exceed the maximum power dissipation for the layout.

$$Avg.P_{D} = \left(\frac{\% DC}{100}\right) \left(V_{IN} - V_{OUT}\right) I_{OUT} + V_{IN} I_{GND}$$

$$455mW = \left(\frac{\% DC}{100}\right) (8V - 5V) 500mA + 8V \times 20mA$$

$$455mW = \left(\frac{\% Duty Cycle}{100}\right) 1.66W$$

$$0.274 = \frac{\% Duty Cycle}{100}$$

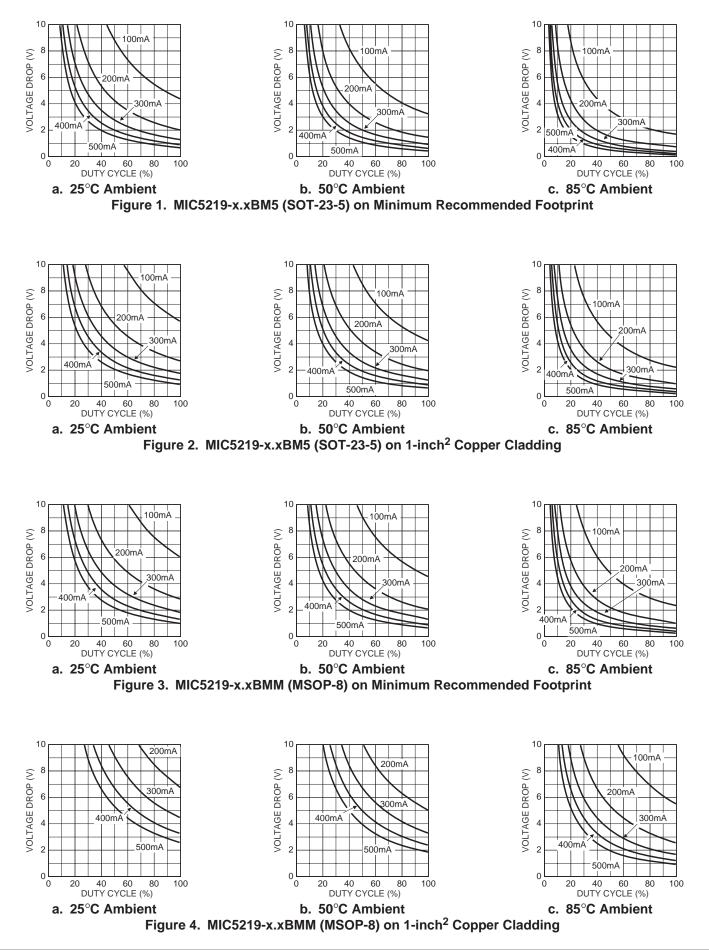
$$\% Duty Cycle Max = 27.4\%$$

With an output current of 500mA and a three-volt drop across the MIC5219-xxBMM, the maximum duty cycle is 27.4%.

Applications also call for a set nominal current output with a greater amount of current needed for short durations. This is a tricky situation, but it is easily remedied. Calculate the average power dissipation for each current section, then add the two numbers giving the total power dissipation for the regulator. For example, if the regulator is operating normally at 50mA, but for 12.5% of the time it operates at 500mA output, the total power dissipation of the part can be easily determined. First, calculate the power dissipation of the device at 50mA. We will use the MIC5219-3.3BM5 with 5V input voltage as our example.

$$P_{D} \times 50\text{mA} = (5\text{V} - 3.3\text{V}) \times 50\text{mA} + 5\text{V} \times 650\mu\text{A}$$
$$P_{D} \times 50\text{mA} = 173\text{mW}$$

However, this is continuous power dissipation, the actual on-time for the device at 50mA is (100%-12.5%) or 87.5% of the time, or 87.5% duty cycle. Therefore,  $P_D$  must be multiplied by the duty cycle to obtain the actual average power dissipation at 50mA.



 $P_D \times 50 \text{mA} = 0.875 \times 173 \text{mW}$ 

$$P_D \times 50 mA = 151 mW$$

The power dissipation at 500mA must also be calculated.

 $P_D \times 500mA = (5V - 3.3V) 500mA + 5V \times 20mA$ 

$$P_{D} \times 500 \text{mA} = 950 \text{mW}$$

This number must be multiplied by the duty cycle at which it would be operating, 12.5%.

 $P_{D} \times = 0.125 \times 950 \text{mW}$ 

 $P_D \times = 119 mW$ 

The total power dissipation of the device under these conditions is the sum of the two power dissipation figures.

 $P_{D(total)} = P_D \times 50mA + P_D \times 500mA$  $P_{D(total)} = 151mW + 119mW$  $P_{D(total)} = 270mW$ 

The total power dissipation of the regulator is less than the maximum power dissipation of the SOT-23-5 package at room temperature, on a minimum footprint board and therefore would operate properly.

Multilayer boards with a ground plane, wide traces near the pads, and large supply-bus lines will have better thermal conductivity.

For additional heat sink characteristics, please refer to Micrel Application Hint 17, "Designing P.C. Board Heat Sinks", included in Micrel's *Databook*. For a full discussion of heat sinking and thermal effects on voltage regulators, refer to Regulator Thermals section of Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.

#### Fixed Regulator Circuits

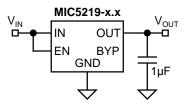
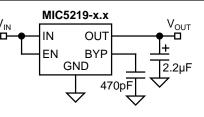


Figure 5. Low-Noise Fixed Voltage Regulator

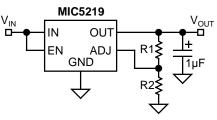
Figure 5 shows a basic MIC5219-x.xBMX fixed-voltage regulator circuit. A 1 $\mu$ F minimum output capacitor is required for basic fixed-voltage applications.



#### Figure 6. Ultra-Low-Noise Fixed Voltage Regulator

Figure 6 includes the optional 470pF noise bypass capacitor between BYP and GND to reduce output noise. Note that the minimum value of  $C_{OUT}$  must be increased when the bypass capacitor is used.

#### Adjustable Regulator Circuits



#### Figure 7. Low-Noise Adjustable Voltage Regulator

Figure 7 shows the basic circuit for the MIC5219 adjustable regulator. The output voltage is configured by selecting values for R1 and R2 using the following formula:

$$V_{OUT} = 1.242 V \left(\frac{R2}{R1} + 1\right)$$

Although ADJ is a high-impedance input, for best performance, R2 should not exceed  $470k\Omega$ .

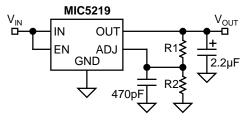


Figure 8. Ultra-Low-Noise Adjustable Application.

Figure 8 includes the optional 470pF bypass capacitor from ADJ to GND to reduce output noise.



# **MIC5237**

### 500mA Low-Dropout Voltage Regulator

### **Preliminary Information**

### **General Description**

The MIC5237 is a general-purpose low-dropout regulator capable of 500mA output current with better than 3% output voltage accuracy. Using Micrel's proprietary Super ßeta PNP<sup>™</sup> process with a PNP pass element, these regulators feature less than 300mV dropout voltage and typically 8mA ground current at full load.

Designed for applications that require moderate current over a broad input voltage range, including hand-held and batterypowered devices, the MIC5237 is intended for applications that can tolerate moderate voltage drop at higher current.

Key features include low ground current to help prolong battery life, reversed-battery protection, current limiting, overtemperature shutdown, and thermally efficient packaging. The MIC5237 is available in fixed output voltages only.

For space-critical applications and improved performance, see the MIC5209 and MIC5219. For output current requirements up to 750mA, see the MIC2937.

### Features

- Guaranteed 500mA output over the full operating temperature range
- Low 300mV typical dropout voltage at full load
- Extremely tight load and line regulation
- · Current and thermal limiting
- Reversed-battery protection
- TO-220 and TO-263 packages
- Low temperature coefficient
- No-load stability
- Low-noise output

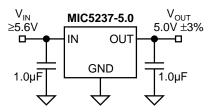
### Applications

- · Portable and laptop computers
- Desktop computer
- Battery chargers
- SMPS post-regulator/dc-to-dc modules
- Consumer and personal electronics

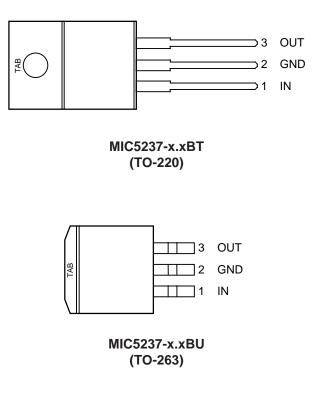
### **Ordering Information**

Part Number	Voltage	Junct. Temp. Range	Package
MIC5237-2.5BT	2.5V	–40°C to +125°C	TO-220
MIC5237-2.5BU	2.5V	–40°C to +125°C	TO-263
MIC5237-3.3BT	3.3V	–40°C to +125°C	TO-220
MIC5237-3.3BU	3.3V	–40°C to +125°C	TO-263
MIC5237-5.0BT	5.0V	–40°C to +125°C	TO-220
MIC5237-5.0BU	5.0V	–40°C to +125°C	TO-263

### **Typical Application**



### **Pin Configuration**



### **Pin Description**

Pin No.	Pin Name	Pin Function
1	IN	Supply Input
2, TAB	GND	Ground: TO-220 and TO-263 pin 2 and TAB are internally connected.
3	OUT	Regulator Output

### **Absolute Maximum Ratings**

Input Voltage (V <sub>IN</sub> )	–20V to +20V
Power Dissipation (P <sub>D</sub> )	Internally Limited
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Lead Temperature (soldering, 5 sec.).	260°C

### **Operating Ratings**

Input Voltage (V <sub>IN</sub> )	+2.5V to +16V
Junction Temperature (T <sub>J</sub> )	–40°C to +125°C
Package Thermal Resistance	
TO-220 (θ <sub>JA</sub> )	55°C/W
TO-220 (θ <sub>JC</sub> )	
TO-263 (θ <sub>JC</sub> )	3°C/W

### **Electrical Characteristics**

Symbol	Parameter	Conditions	Min	Typical	Max	Units
V <sub>OUT</sub>	Output Voltage Accuracy	variation from nominal V <sub>OUT</sub>	-3 -5		3 5	% %
$\Delta V_{OUT} / \Delta T$	Output Voltage Temperature Coefficient	Note 2		40		ppm/°C
$\Delta V_{OUT} / V_{OUT}$	Line Regulation	$V_{IN} = V_{OUT} + 1V$ to 16V		0.015	0.05 <b>0.1</b>	%/V %/V
$\Delta V_{OUT} / V_{OUT}$	Load Regulation	I <sub>OUT</sub> = 100μA to 500mA, <b>Note 3</b>		0.05	0.5 <b>0.7</b>	% %
V <sub>IN</sub> – V <sub>OUT</sub>	Dropout Voltage, Note 4	I <sub>OUT</sub> = 100μA		10	70 <b>90</b>	mV mV
		I <sub>OUT</sub> = 50mA		115	190 <b>280</b>	mV mV
		I <sub>OUT</sub> = 150mA	165	165	350 <b>450</b>	mV mV
		I <sub>OUT</sub> = 500mA		300	600 <b>700</b>	mV mV
I <sub>GND</sub>	Ground Pin Current, Note 5	I <sub>OUT</sub> = 100μA		80	130 <b>170</b>	μA μA
		I <sub>OUT</sub> = 50mA		350	650 <b>900</b>	μΑ μΑ
		I <sub>OUT</sub> = 150mA		1.8	2.5 <b>3.0</b>	mA mA
		I <sub>OUT</sub> = 500mA		8	15 <b>20</b>	mA mA
PSRR	Ripple Rejection	f = 120Hz		75		dB
I <sub>LIMIT</sub>	Current Limit	V <sub>OUT</sub> = 0V		700	900 <b>1000</b>	mA
$\overline{\Delta V_{OUT} / \Delta P_D}$	Thermal Regulation	Note 6		0.05		%/W
e <sub>no</sub>	Output Noise	$V_{OUT} = 5.0V, I_{OUT} = 50mA,$ $C_{OUT} = 2.2\mu F$		500		nV/√Hz

 $V_{IN} = V_{OUT} + 1.0V$ ;  $C_{OUT} = 4.7\mu$ F,  $I_{OUT} = 100\mu$ A;  $T_{II} = 25^{\circ}$ C, **bold** values indicate  $-40^{\circ}$ C  $\leq T_{II} \leq +125^{\circ}$ C; unless noted.

Note 1: Absolute maximum ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of its operating ratings. The maximum allowable power dissipation is a function of the maximum junction temperature, T<sub>J(max)</sub>, the junction-to-ambient thermal resistance, θ<sub>JA</sub>, and the ambient temperature, T<sub>A</sub>. The maximum allowable power dissipation at any ambient temperature is calculated using: P<sub>D(max)</sub> = (T<sub>J(max)</sub> - T<sub>A</sub>) + θ<sub>JA</sub>. Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown. See the "Thermal Considerations" section for details.

Note 2: Output voltage temperature coefficient is defined as the worst case voltage change divided by the total temperature range.

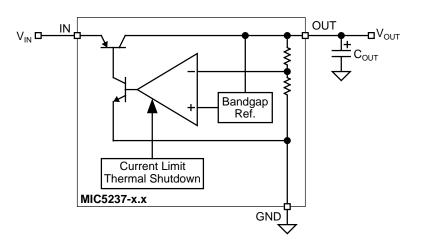
**Note 3:** Regulation is measured at constant junction temperature using low duty cycle pulse testing. Parts are tested for load regulation in the load range from 100µA to 500mA. Changes in output voltage due to heating effects are covered by the thermal regulation specification.

Note 4: Dropout voltage is defined as the input to output differential at which the output voltage drops 2% below its nominal value measured at 1V differential.

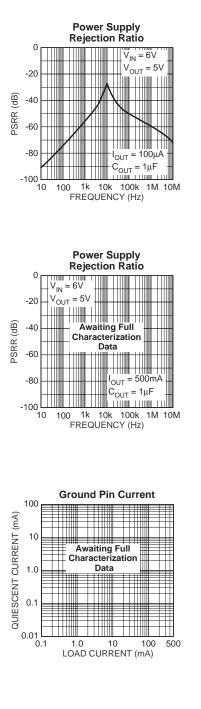
Note 5: Ground pin current is the regulator quiescent current plus pass transistor base current. The total current drawn from the supply is the sum of the load current plus the ground pin current.

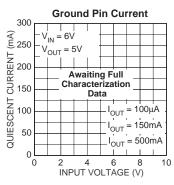
**Note 6:** Thermal regulation is defined as the change in output voltage at a time "t" after a change in power dissipation is applied, excluding load or line regulation effects. Specifications are for a 500mA load pulse at  $V_{IN} = 16V$  for t = 10ms.

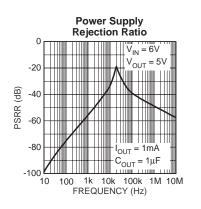
### **Block Diagram**

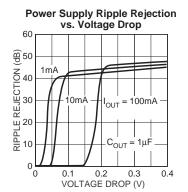


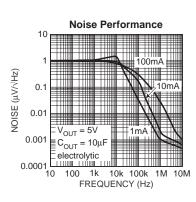












**Power Supply** 

**Rejection Ratio** 

= 100mA

1M 10M

OUT  $C_{OUT} = 1\mu F$ 

1k 10k 100k

FREQUENCY (Hz)

= 6V'IN

= 5'

0

-20

-40

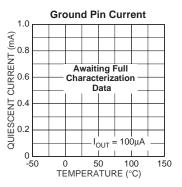
-60

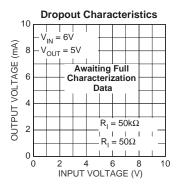
-80

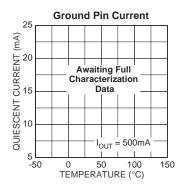
-100

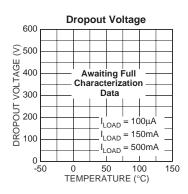
10 100

PSRR (dB)

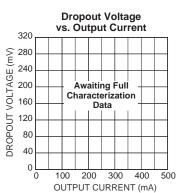


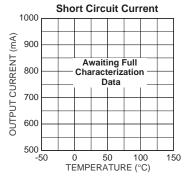


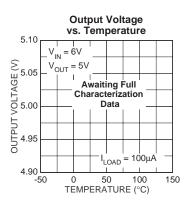


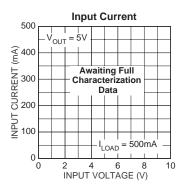


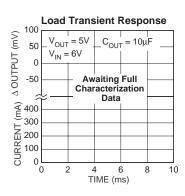
### **Typical Characteristics**

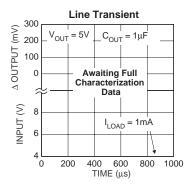


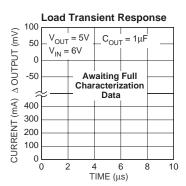












### **Applications Information**

The MIC5237 is intended for general-purpose use and can be implemented in a wide variety of applications where 500mA of output current is needed. It is available in several voltage options for ease of use. For voltage options that are not available on the MIC5237, consult the MIC5209 for a 500mA adjustable LDO regulator, or the MIC5219 for applications that require only short-duration peak output current.

#### **Input Capacitor**

A 1 $\mu$ F capacitor should be placed from IN to GND if there is more than 10 inches of wire between the input and the ac filter capacitor or if a battery is used as the input.

#### **Output Capacitor**

An output capacitor is required between OUT and GND to prevent oscillation.  $1\mu$ F minimum is recommended for standard applications. Larger values improve the regulator's transient response. The output capacitor value may be increased without limit.

The output capacitor should have an ESR (equivalent series resistance) of about  $5\Omega$  or less and a resonant frequency above 1MHz. Ultralow-ESR capacitors can cause low-amplitude oscillations and/or underdamped transient response. Most tantalum or aluminum electrolytic capacitors are adequate; film types will work, but are more expensive. Since many aluminum electrolytics have electrolytes that freeze at about  $-30^{\circ}$ C, solid tantalums are recommended for operation below  $-25^{\circ}$ C.

At lower values of output current, less output capacitance is needed for output stability. The capacitor can be reduced to  $0.47\mu$ F for current below 10mA or  $0.33\mu$ F for currents below 1mA.

For 2.5V applications a  $22\mu$ F output capacitor is recommended to reduce startup voltage overshoot.

#### **No-Load Stability**

The MIC5237 will remain stable and in regulation with no load (other than the internal voltage divider) unlike many other voltage regulators. This is especially important in CMOS RAM keep-alive applications.

#### **Thermal Considerations**

Proper thermal design can be accomplished with some basic design criteria and some simple equations. The following information is required to implement a regulator design.

V<sub>OUT</sub> = output voltage

I<sub>OUT</sub> = output current

 $T_A$  = ambient operating temperature

The regulator ground current,  $I_{GND}$ , can be measured or read from the data sheet. Assuming the worst case scenario is good design procedure, and the corresponding ground cur-

rent number can be obtained from the data sheet. First, calculate the power dissipation of the device. This example uses the MIC5237-5.0BT, a 13V input, and 500mA output current, which results in 20mA of ground current, worst case. The power dissipation is the sum of two power calculations: voltage drop  $\times$  output current and input voltage  $\times$  ground current.

$$P_{D} = [(V_{IN} - V_{OUT}) \times I_{OUT}] + (V_{IN} \times I_{GND})$$
$$P_{D} = [(13V - 5V) \times 500\text{mA}] + (13V \times 20\text{mA})$$
$$P_{D} = 4.260\text{W}$$

From this number, the heat sink thermal resistance is determined using the regulator's maximum operating junction temperature ( $T_{J(max)}$ ) and the ambient temperature ( $T_A$ ) along with the power dissipation number already calculated.

$$T_{J(MAX)} = 125^{\circ}C$$
  
 $\theta_{JC} = \text{junction-to-case thermal resistance}$   
 $\theta_{CS} = \text{case-to-sink thermal resistance}$   
 $\theta_{JA} = \text{junction-to-ambient thermal resistance}$   
 $\theta_{CA} = \text{sink-to-ambient thermal resistance}$ 

To determine the heat sink thermal resistance, the junctionto-case thermal resistance of the device must be used along with the case-to-heat sink thermal resistance. These numbers show the heat-sink thermal resistance required at  $T_A = 25^{\circ}$ C that does not exceed the maximum operating junction temperature.

$$\theta_{JA} = \frac{T_{J(max)} - T_{A}}{P_{D}}$$

$$\theta_{SA} = \theta_{JA} - \theta_{JC}$$

 $\theta_{CS}$  is approximately 1°C/W and  $\theta_{JC}$  for the TO-220 is 3°C/W in this example.

$$\theta_{JA} = \frac{125 - 25}{4.260W}$$
  

$$\theta_{JA} = 23.5^{\circ}C/W$$
  

$$\theta_{SA} = 23.5^{\circ}C/W - (3^{\circ}C/W + 1^{\circ}C/W)$$
  

$$\theta_{SA} = 19.5^{\circ}C/W$$

Therefore, a heat sink with a thermal resistance of 19.5° C/W will allow the part to operate safely and it will not exceed the maximum junction temperature of the device. The heat sink can be reduced by limiting power dissipation, by reducing the input voltage or output current. Either the TO-220 or TO-263 package can operate reliably at 2W of power dissipation without a heat sink. Above 2W, a heat sink is recommended.

For a full discussion on voltage regulator thermal effects, please refer to "Thermal Management" in Micrel's *Designing with Low-Dropout Voltage Regulators* handbook.



# MIC5156/5157/5158

### Super LDO<sup>™</sup> Regulator Controller

### **General Description**

The MIC5156, MIC5157, and MIC5158 Super Low-Dropout (LDO) Regulator Controllers are single IC solutions for highcurrent low-dropout linear voltage regulation. Super LDO<sup>TM</sup> Regulators have the advantages of an external N-channel power MOSFET as the linear pass element.

The MIC5156/7/8 family features a dropout voltage as low as the  $R_{DS(ON)}$  of the external power MOSFET multiplied by the output current. The output current can be as high as the largest MOSFETs can provide.

The MIC5156/7/8 family operates from 3V to 36V. The MIC5156 requires an external gate drive supply to provide the higher voltage needed to drive the gate of the external MOSFET. The MIC5157 and MIC5158 each have an internal charge pump tripler to produce the gate drive voltage. The tripler is capable of providing enough voltage to drive a logic-level MOSFET to 3.3V output from a 3.5V supply and is clamped to 17.5V above the supply voltage. The tripler requires three external capacitors.

The regulator output is constant-current limited when the controller detects 35mV across an optional external sense resistor. An active-low open-collector flag indicates a low voltage of 8% or more below nominal output. A shutdown (low) signal to the TTL-compatible enable control reduces controller supply current to less than 1µA while forcing the output voltage to ground.

The MIC5156-3.3 and MIC5156-5.0 controllers have internally fixed output voltages. The MIC5156 [adjustable] output is configured using two external resistors. The MIC5157 is a fixed output controller which is externally configured to select either 3.3V, 5.0V, or 12V. The MIC5158 can be configured as a fixed 5V controller or programmed to any voltage from 1.3V to 36V using two external resistors.

The MIC5156 is available in an 8-pin plastic DIP, ceramic DIP, or SOIC package. The MIC5157 and MIC5158 are available in a 14-pin plastic DIP, ceramic DIP, or SOIC. The plastic DIP and SOIC versions operate from  $-40^{\circ}$ C to  $+85^{\circ}$ C. The ceramic DIP versions cover the  $-55^{\circ}$ C to  $+125^{\circ}$ C military temperature range.

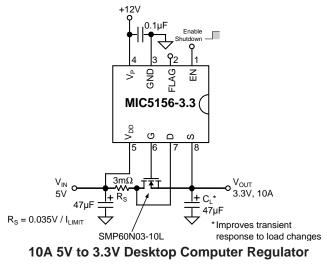
### **Features**

- 4.5mA typical operating current
- <1µA typical standby current</li>
- Low external parts count
- Optional current limit (35mV typical threshold)
- 1% initial output voltage tolerance in most configurations
- 2% output voltage tolerance over temperature
- Fixed output voltages of 3.3V, 5.0V (MIC5156)
- Fixed output voltages of 3.3V, 5.0V, 12V (MIC5157)
- Programmable (1.3 to 36V) with 2 resistors (MIC5156/8)
- Internal charge pump voltage tripler (MIC5157/8)
- Enable pin to activate or shutdown the regulator
- Internal gate-to-source protective clamp
- All versions available in DIP and SOIC

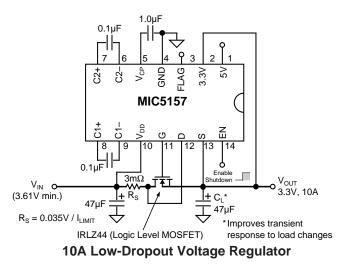
### Applications

- Ultra-high current ultra-low dropout voltage regulator
- Constant high-current source
- Low parts count 5.0V to 3.3V computer supply
- Low noise/low-dropout SMPS post regulator
- High-current, current-limited switch

### **Typical Applications**



Super LDO is a trademark of Micrel, Inc.



### **Ordering Information MIC5156**

Part Number	Temperature Range	Voltage	Package
MIC5156-3.3BN -40°C to +85°C		3.3V	8-pin P-DIP
MIC5156-5.0BN	–40°C to +85°C	5.0V	8-pin P-DIP
MIC5156BN	–40°C to +85°C	Adjustable	8-pin P-DIP
MIC5156-3.3BM	–40°C to +85°C	3.3V	8-pin SOIC
MIC5156-5.0BM	–40°C to +85°C	5.0V	8-pin SOIC
MIC5156BM	–40°C to +85°C	Adjustable	8-pin SOIC
MIC5156-3.3AJ	–55°C to +125°C	3.3V	8-pin CerDIP
MIC5156-5.0AJ	–55°C to +125°C	5.0V	8-pin CerDIP
MIC5156AJ	–55°C to +125°C	Adjustable	8-pin CerDIP

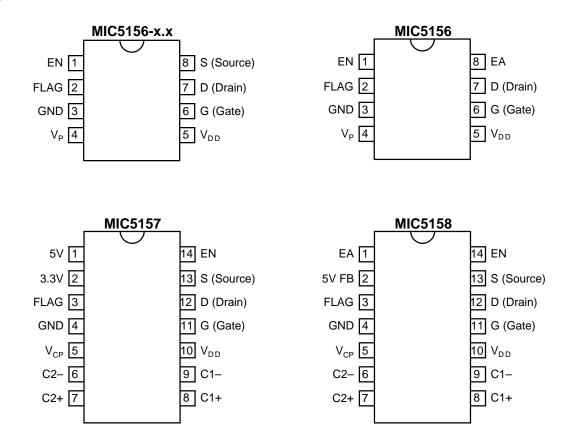
### **Ordering Information MIC5157**

Part Number	Temperature Range	Voltage	Package
MIC5157BN	–40°C to +85°C	Selectable	14-pin P-DIP
MIC5157BM	–40°C to +85°C	Selectable	14-pin SOIC
MIC5157AJ	–55°C to +125°C	Selectable	14-pin CerDIP

### **Ordering Information MIC5158**

Part Number	Temperature Range	Voltage	Package
MIC5158BN	–40°C to +85°C	5.0V/Adj.	14-pin P-DIP
MIC5158BM	–40°C to +85°C	5.0V/Adj.	14-pin SOIC
MIC5158AJ	–55°C to +125°C	5.0V/Adj.	14-pin CerDIP

### **Pin Configuration**



### Pin Description MIC5156

Pin Number	Pin Name	Pin Function	
1	EN	Enable (Input): TTL high enables regulator; TTL low shuts down regulator.	
2	FLAG	Output Flag (Output): Open collector output is active (low) when V <sub>OUT</sub> is more than 8% below nominal output. Circuit has 3% hysteresis.	
3	GND	Circuit ground.	
4	V <sub>P</sub>	N-channel Gate Drive Supply Voltage: User supplied voltage for driving the gate of the external MOSFET.	
5	V <sub>DD</sub>	Supply Voltage (Input): Supply voltage connection. Connect sense resistor (R <sub>S</sub> ) to V <sub>DD</sub> if current limiting used. Connect supply bypass capacitor to ground near device.	
6	G	Gate (Output): Drives the gate of the external MOSFET.	
7	D	Drain and Current Limit (Input): Connect to external MOSFET drain and external sense resistor (current limit), or connect to V <sub>DD</sub> and external MOSFET drain (no current limit).	
8 (3.3V, 5V)	S	Source (Input): Top of internal resistive divider chain. Connect directly to the load for best load regulation.	
8 (adjustable)	EA	Error Amplifier (Input): Connect to external resistive divider.	

## Pin Description MIC5157, MIC5158

Pin Number	Pin Name	Pin Function	
1 (MIC5157)	5V	5V Configuration (Input): Connect to S (source) pin for 5V output.	
1 (MIC5158)	EA	Error Amplifier (Input): Connect to external resistive divider to obtain adjust- able output.	
2 (MIC5157)	3.3V	3.3V Configuration (Input): Connect to S (source) pin for 3.3V output.	
2 (MIC5158)	5V FB	5V Feedback (Input): Connect to EA for fixed 5V output.	
3	FLAG	Output Voltage Flag (Output): Open collector is active (low) when V <sub>OUT</sub> is 8% or more below its nominal value.	
4	GND	Circuit ground.	
5	V <sub>CP</sub>	Voltage Tripler Output [Filter Capacitor]. Connect a 1 to 10µF capacitor to ground.	
6	C2-	Charge Pump Capacitor 2: Second stage of internal voltage tripler. Connect a 0.1µF capacitor from C2+ to C2–.	
7	C2+	Charge Pump Capacitor 2: See C2– pin 6.	
8	C1+	Charge Pump Capacitor 1: First stage of internal voltage tripler. Connect a $0.1\mu$ F capacitor from C1+ to C1–.	
9	C1-	Charge Pump Capacitor 1: See C1+ pin 8.	
10	V <sub>DD</sub>	Supply Voltage (Input): Supply voltage connection. Connect sense resistor $(R_S)$ to $V_{DD}$ if current limiting used. Connect supply bypass capacitor to ground near device.	
11	G	Gate (Output): Connect to External MOSFET gate.	
12	D	Drain and Current Limit (Input): Connect to external MOSFET drain and external sense resistor (current limit), or connect to V <sub>DD</sub> and external MOSFET drain (no current limit).	
13 (MIC5157)	S	Source and 3.3V/5V Configuration: Top of internal resistor chain. Connect to source of external MOSFET for 3.3V, 5V, and 12V operation. Also see 3.3V and 5V pin descriptions.	
13 (MIC5158)	s	Source (Input): Top of internal resistor chain. Connect to top of external resistive divider and source of external MOSFET.	
14	EN	Enable (Input): TTL high enables regulator; TTL low shuts down regulator.	

### **Absolute Maximum Ratings**

V <sub>DD</sub>	
EN	
V <sub>G</sub> (MIC5156)	55V
V <sub>CP</sub> (MIC5157/8)	55V
V <sub>SOURCE</sub>	
FLAG	
Operating Junction Temperature	
T <sub>J</sub>	150°C

Ambient Temperature F T <sub>A</sub> (MIC515xBM/BN) T <sub>A</sub> (MIC515xAJ)		
Storage Temperature		–65°C to +150°C
Lead Temperature		
(soldering 10s)		300°C
Package $\theta_{JA}$	MIC5156	MIC5157/8
Plastic DIP	100°C/W	90°C/W
Ceramic DIP	125°C/W	110°C/W
SOIC	160°C/W	120°C/W

#### Symbol Condition (Note 1) Min Parameter Тур Max Units $V_{DD}$ V Supply Voltage 3 36 Supply Current MIC5156 10 mΑ Operating, V<sub>FN</sub> = 5V 2.7 DD(ON) Shutdown, $V_{EN} = 0V$ 0.1 5 μΑ DD(OFF) 4.5 10 mΑ I<sub>DD(ON)</sub> Supply Current MIC5157/8 Operating, V<sub>EN</sub> = 5V Shutdown, $V_{FN} = 0V$ 0.1 5 μΑ IDD(OFF) **Enable Input Threshold** High 2.4 1.3 V VIH VIL Low 1.3 0.8 V EN I<sub>B</sub> **Enable Input Bias Current** $V_{EN} = 2.4V$ 20 25 μΑ V<sub>CP</sub> Max. Charge Pump Voltage $V_{CP} - V_{DD}, V_{DD} > 10V$ 17.5 18.5 V Charge Pump Frequency 160 kHz f<sub>CP</sub> Maximum Gate Drive Voltage $V_{SOURCE} = 0V$ V<sub>OUT MAX</sub> $V_{DD} = 3.5V$ $V_{DD} = 5V$ (MIC5157/8) 5 9 V 7.0 9 11.3 15 V $V_{DD}^{--} = 12V$ 24 30 V 28 Minimum Gate Drive Voltage 1.0 V V<sub>OUT MIN</sub> $V_{SOURCE} > V_{OUT(NOM)}$ $V_{LIM}$ **Current Limit Threshold** $V_{DD} - V_D @ I_{LIM}$ 28 35 42 mV Vs Source Voltage Short G (gate) to (S) source, Note 2 MIC5156-3.3 3.267 3.3 3.333 V MIC5156-5.0 4.950 5.0 5.050 V MIC5157, 3.3V pin to S pin (3.3V config.) 3.250 3.3 3.350 V MIC5157, 5V pin to S pin (5V config.) 4.950 5.050 V 5.0 MIC5157, V<sub>DD</sub> = 7V, (12V config.) 11.70 12 12.30 V MIC5158, 5V FB pin to EA pin (5V config.) 4.925 5.0 5.075 V V V<sub>BG</sub> Bandgap Reference Voltage MIC5156 [adjustable] and MIC5158 1.222 1.235 1.248 $5V < V_{DD} < 15V, V_{OUT} = 3.3V$ $V_{LR}$ **Output Voltage Line Regulation** 2 7 mV Gate to Source Clamp 14 16.6 20 V V<sub>GS MAX</sub> % of nominal V<sub>SOURCE</sub> $V_{FT}$ Flag Comparator Threshold 92 % % of nominal V<sub>SOURCE</sub> $V_{FH}$ Flag Comparator Hysteresis 3 % $V_{SAT}$ Flag Comparator Sat. Voltage 0.09 V $I_{FLAG} = 1mA$ 0.2

### **Electrical Characteristics**

**General Note:** Devices are ESD sensitive. Handling precautions recommended.

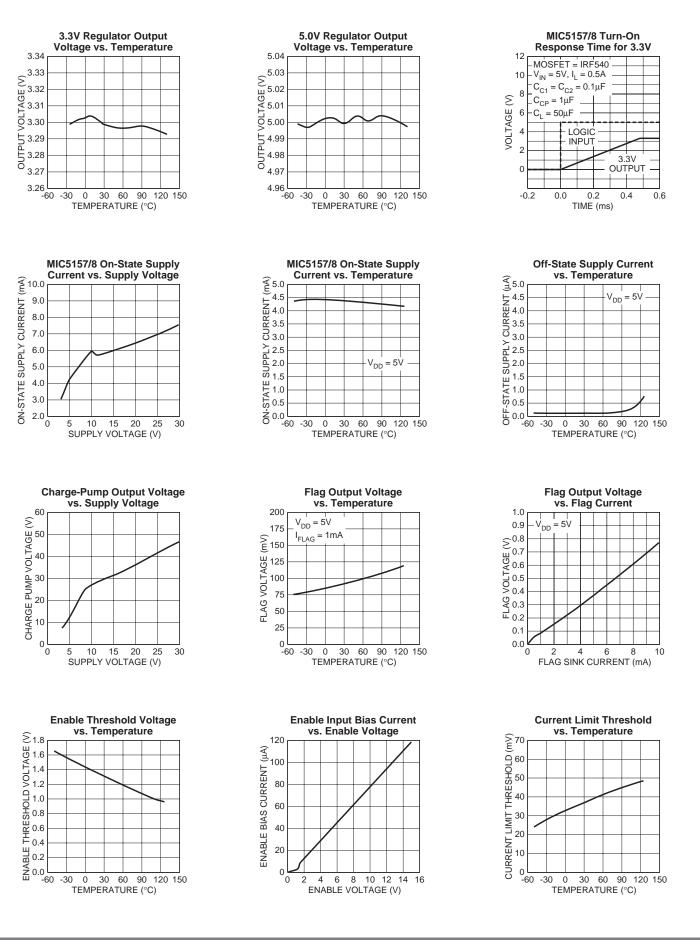
Note 1:  $T_A = 25^{\circ}C$ ,  $V_{DD} = 5V$ ,  $V_{EN} = 5V$ , unless noted.

**Note 2:** Test configuration. External MOSFET not used.

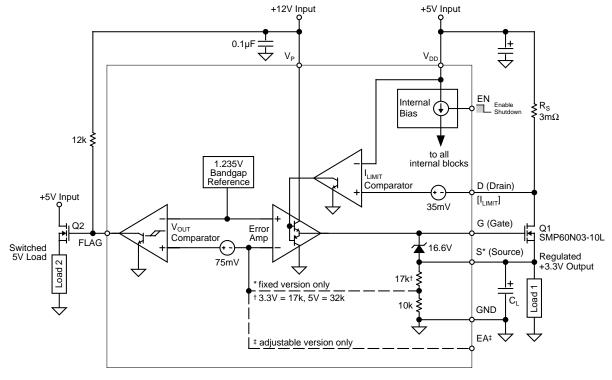
Micrel

### **Typical Characteristics**



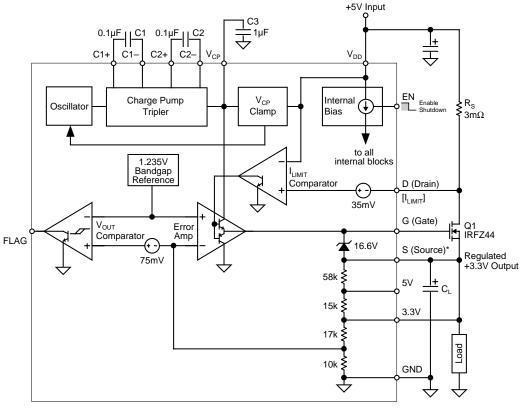


### **Block Diagram MIC5156**



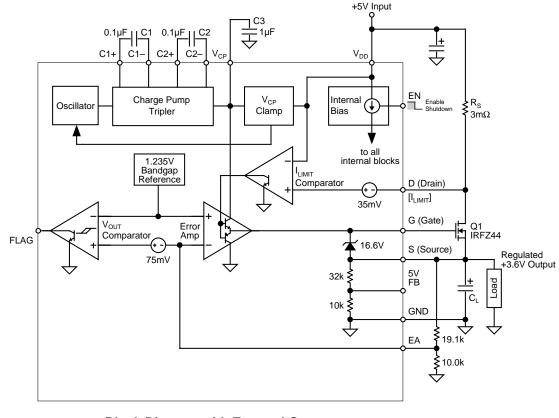
Block Diagram with External Components Fixed 3.3V Power Supply with 5.0V Load Switch

### **Block Diagram MIC5157**



Block Diagram with External Components Fixed 3.3V 10A Power Supply

### **Block Diagram MIC5158**



Block Diagram with External Components Adjustable Power Supply, 3.6V Configuration

### **Functional Description**

A *Super LDO Regulator* is a complete regulator built around Micrel's *Super LDO Regulator Controller*.

Refer to Block Diagrams MIC5156, MIC5157, and MIC5158.

#### **Version Differences**

The MIC5156 requires an external voltage for MOSFET gate drive and is available in 3.3V fixed output, 5V fixed output, or adjustable output versions. With 8-pins, the MIC5156 is the smallest of the Super LDO Regulator Controllers.

The MIC5157 and MIC5158 each have an internal charge pump which provides MOSFET gate drive voltage. The MIC5157 has a selectable fixed output of 3.3V, 5V, or 12V. The MIC5158 may be configured for a fixed 5V or adjustable output.

### Enable (EN)

With at least 3.0V on  $V_{DD}$ , applying a TTL low to EN places the controller in shutdown mode. A TTL high on EN enables the internal bias circuit which powers all internal circuitry. EN must be pulled high if unused. The voltage applied to EN may be as high as 36V.

The controller draws less than  $1\mu A$  in shutdown mode.

#### **Gate Enhancement**

The Super LDO Regulator Controller manages the gate-tosource enhancement voltage for an external N-channel MOSFET (regulator pass element) placed between the supply and the load. The gate-to-source voltage may vary from 1V to 16V depending upon the supply and load conditions.

Because the source voltage (output) approaches the drain voltage (input) when the regulator is in dropout and the MOSFET is fully enhanced, an additional higher supply voltage is required to produce the necessary gate-to-source enhancement. This higher gate drive voltage is provided by an external gate drive supply (MIC5156) or by an internal charge pump (MIC5157 and MIC5158).

#### Gate Drive Supply Voltage (MIC5156 only)

The gate drive supply voltage must not be more than 14V above the supply voltage ( $V_P - V_{DD} < 14V$ ). The minimum necessary gate drive supply voltage is:

$$V_P = V_{OUT} + V_{GS} + 1$$

where:

V<sub>P</sub> = gate drive supply voltage

V<sub>OUT</sub> = regulator output voltage

V<sub>GS</sub> = gate-to-source voltage for full MOSFET gate enhancement

The error amplifier uses the gate drive supply voltage to drive the gate of the external MOSFET. The error amplifier output can swing to within 1V of  $V_p$ .

#### Charge Pump (MIC5157/5158 only)

The charge pump tripler creates a dc voltage across reservoir capacitor C3. External capacitors C1 and C2 provide the necessary storage for the stages of the charge pump tripler.

The tripler's approximate dc output voltage is:

$$V_{CP} \approx 3 (V_{DD} - 1)$$

where:

V<sub>CP</sub> = charge pump output voltage

 $V_{DD}$  = supply voltage

The  $V_{CP}$  clamp circuit limits the charge pump voltage to 16V above  $V_{DD}$  by gating the charge pump oscillator ON or OFF as required. The charge pump oscillator operates at 160kHz.

The error amplifier uses the charge pump voltage to drive the gate of the external MOSFET. It provides a constant load of about 1mA to the charge pump. The error amplifier output can swing to within 1V of  $V_{CP}$ .

Although the MIC5157/8 is designed to provide gate drive using its internal charge pump, an external gate drive supply voltage can be applied to  $V_{CP}$ . When using an external gate drive supply,  $V_{CP}$  must not be forced more than 14V higher than  $V_{DD}.$ 

When constant loads are driven, the ON/OFF switching of the charge pump may be evident on the output waveform. This is caused by the charge pump switching ON and rapidly increasing the supply voltage to the error amplifier. The period of this small charge pump excitation is determined by a number of factors: the input voltage, the 1mA op-amp load, any dc leakage associated with the MOSFET gate circuit, the size of the charge pump capacitors, the size of the charge pump reservoir capacitor, and the characteristics of the input voltage and load. The period is lengthened by increasing the charge pump reservoir capacitor (C3). The amplitude is reduced by weakening the charge pump—this is accomplished by reducing the size of the pump capacitors (C1 and C2). If this small burst is a problem in the application, use a  $10\mu$ F reservoir capacitor at C3 and  $0.01\mu$ F pump capacitors

at C1 and C2. Note that the recovery time to repetitive load transients may be affected with small pump capacitors.

#### Gate-to-Source Clamp

A gate-to-source protective voltage clamp of 16.6V protects the MOSFET in the event that the output voltage is suddenly forced to zero volts. This prevents damage to the external MOSFET during shorted load conditions. Refer to "Charge Pump" for normal clamp circuit operation.

The source connection required by the gate-to-source clamp is not available on the adjustable version of the MIC5156.

#### **Output Regulation**

At start-up, the error amplifier feedback voltage (EA), or internal feedback on fixed versions, is below nominal when compared to the internal 1.235V bandgap reference. This forces the error amplifier output high which turns on external MOSFET Q1. Once the output reaches regulation, the controller maintains constant output voltage under changing input and load conditions by adjusting the error amplifier output voltage (gate enhancement voltage) according to the feedback voltage.

#### **Out-of-Regulation Detection**

When the output voltage is 8% or more below nominal, the open-collector FLAG output (normally high) is forced low to signal a fault condition. The FLAG output can be used to signal or control external circuitry. The FLAG output can also be used to shut down the regulator using the EN control.

#### **Current Limiting**

Super LDO Regulators perform constant-current limiting (not foldback). To implement current limiting, a sense resistor ( $R_S$ ) must be placed in the "power" path between V<sub>DD</sub> and D (drain).

If the voltage drop across the sense resistor reaches 35mV, the current limit comparator reduces the error amplifier output. The error amplifier output is decreased only enough to reduce the output current, keeping the voltage across the sense resistor from exceeding 35mV.

### **Application Information**

#### **MOSFET Selection**

Standard N-channel enhancement-mode MOSFETs are acceptable for most Super LDO regulator applications.

Logic-level N-channel enhancement-mode MOSFETs may be necessary if the external gate drive voltage is too low (MIC5156), or the input voltage is too low, to provide adequate charge pump voltage (MIC5157/8) to enhance a standard MOSFET.

#### **Circuit Layout**

For the best voltage regulation, place the source, ground, and error amplifier connections as close as possible to the load. See figures (1a) and (1b).

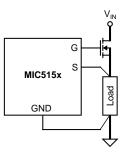
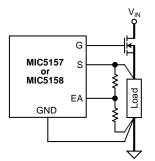
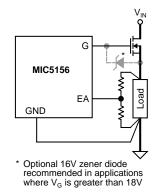


Figure 1a. Connections for Fixed Output



#### Figure 1b. Connections for Adjustable Output



#### Figure 1c. MIC5156 Connections for Adjustable Output

#### **MOSFET Gate-to-Source Protection**

When using the adjustable version of the MIC5156, an external 16V zener diode placed from gate-to-source is recommended for MOSFET protection. All other versions of the Super LDO regulator controller use the internal gate-to-source clamp.

### **Output Voltage Configuration**

#### Fixed Configurations

The MIC5156-3.3 and MIC5156-5.0 are preset for 3.3V and 5.0V respectively.

The MIC5157 operates at 3.3V when the 3.3V pin is connected to the S (source) pin; 5.0V when the 5.0V pin is connected to the S pin; or 12V if the 3.3V and 5.0V pins are open.

The MIC5158 operates at a fixed 5V (without an external resistive divider) if the 5V FB pin is connected to EA.

### Adjustable Configurations

Micrel's MIC5156 [adjustable] and MIC5158 require an external resistive divider to set the output voltage from 1.235V to 36V. For best results, use a  $10k\Omega$  resistor for R2. See equation (1) and figure (2).

1) 
$$R_1 = 1 \times 10^4 \left( \frac{V_{OUT}}{1.235} - 1 \right)$$

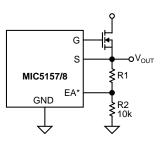


Figure 2. Typical Resistive Divider

### **Input Filter Capacitor**

The Super LDO requires an input bypass capacitor for accommodating wide changes in load current and for decoupling the error amplifier and charge pump. A medium to large value low-ESR (equivalent series resistance) capacitor is best, mounted close to the device.

### **Output Filter Capacitor**

An output filter capacitor may be used to reduce ripple and improve load regulation. Stable operation does not require a large capacitor, but for transient load regulation the size of the output capacitor may become a consideration. Common aluminum electrolytic capacitors perform nicely; very low-ESR capacitors are not necessary. Increased capacitance (rather than reduced ESR) is preferred. The capacitor value should be large enough to provide sufficient  $I = C \times dV/dt$ current consistent with the required transient load regulation quality. For a given step increase in load current, the output voltage will drop by about  $dV = I \times dt/C$ , where I represents the increase in load current over time t. This relationship assumes that all output current was being supplied via the MOSFET pass device prior to the load increase. Small  $(0.01\mu$ F to  $10\mu$ F) film capacitors parallel to the load will further improve response to transient loads.

Some linear regulators specify a minimum required output filter capacitance because the capacitor determines the dominant pole of the system, and thereby stabilizes the system. This is not the situation for the MIC5156/7/8; its dominant pole is determined within its error amplifier.

#### **Current Limiting**

Current sensing requires a low-value series resistance ( $R_s$ ) between  $V_{DD}$  and D (drain). Refer to the typical applications. The internal current-limiting circuit limits the voltage drop across the sense resistor to 35mV. Equation (2) provides the sense resistor value required for a given maximum current.

2) 
$$R_{S} = \frac{35mV}{I_{LIM}}$$

where:

R<sub>S</sub> = sense resistor value

 $I_{LIM}$  = maximum output current

Most current-limited applications require low-value resistors. See *Application Hints 21 and 25* for construction hints.

#### Non-Current Limited Applications

For circuits not requiring current limiting, do not use a sense resistor between  $V_{DD}$  and D (drain). See figure (3). The controller will not limit current when it does not detect a 35mV drop from  $V_{DD}$  to D.

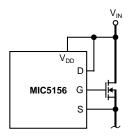


Figure 3. No Current Limit

#### 3.3V Microprocessor Applications

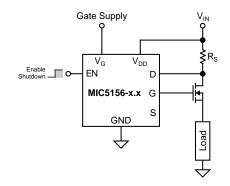
For computer designs that use 3.3V microprocessors with 5V logic, the FLAG output can be used to suppress the 5V supply until the 3.3V output is in regulation. Refer to the external components shown with the MIC5156 Block Diagram.

#### **SMPS Post Regulator Application**

A Super LDO regulator can be used as a post regulator for a switch-mode power supply. The Super LDO regulator can provide a significant reduction in peak-to-peak ripple voltage.

#### **High-Current Switch Application**

All versions of the MIC5156/7/8 may be used for currentlimited, high-current, high-side switching with or without voltage regulation. See figure (4a). Simply leave the "S" terminal open. A 16V zener diode from the gate to the source of the MOSFET protects the MOSFET from overdrive during fault conditions.



#### Figure 4a. High-Side Switch

If a MIC5157 or MIC5158 is used and is shutdown for a given time, the charge pump reservoir  $V_{CP}$  will bleed off. If recharging the reservoir causes an unacceptable delay in the load reaching its operating voltage, do not use the EN pin for on/ off control. Instead, use the MIC5158, hold EN high to keep the charge pump in continuous operation, and switch the MOSFET on or off by overriding the error amplifier input as shown in figure (4b).

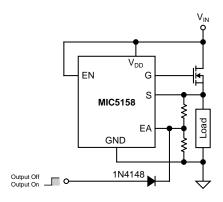


Figure 4b. Fast High-Side Switch

#### **Battery Charger Application**

The MIC5158 may be used in constant-current applications such as battery chargers. See figure (5). The regulator supplies a constant-current ( $35mV \div R3$ ) until the battery approaches the float voltage:

$$V_{FL} = 1.235 \left(1 + \frac{R1}{R2}\right)$$

where:

 $V_{FI}$  = float voltage

At float voltage, the MOSFET is shut off. A trickle charge is supplied by R4.

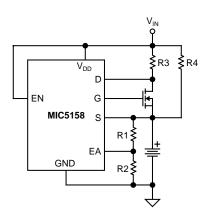


Figure 5. Battery Charger Concept

#### **Uninterruptible Power Supply**

The MIC5157 and two N-channel MOSFETs provide battery switching for uninterruptible power as shown in figure (6). Two MOSFETs are placed source-to-source to prevent current flow through their body diodes when switched off. The Super LDO regulator is continuously enabled to achieve fast battery switch-in. Careful attention must be paid to the ac-line monitoring circuitry to ensure that the output voltage does not fall below design limits while the battery is being switched in.

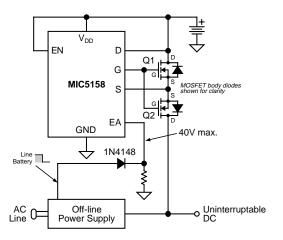


Figure 6. UPS Power Supply Concept

# Section 6. Package Information

Packaging for Automatic Handling	
Tape & Reel	
Ammo Pack	
Pricing	
Tape & Reel Standards	
Packages Available in Tape & Reel	
Package Orientation	
Linear Regulator Packages	
8-Pin Plastic DIP (N)	
14-Pin Plastic DIP (N)	
8-Pin SOIC (M)	
14-Pin SOIC (M)	
TO-92 (Z)	
SOT-223 (S)	
SOT-143 (M4)	
SOT-23 (M3)	
SOT-23-5 (M5)	
MSOP-8 [MM8 <sup>TM</sup> ] (MM)	
3-Lead TO-220 (T)	
5-Lead TO-220 (T)	
5-Lead TO-220 Vertical Lead Bend Option (-LB03)	
5-Lead TO-220 Horizontal Lead Bend Option (-LB02)	
3-Lead TO-263 (U)	
5-Lead TO-263 (U)	
Typical 3-Lead TO-263 PCB Layout	
Typical 5-Lead TO-263 PCB Layout	
3-Lead TO-247 (WT)	
5-Lead TO-247 (WT)	

# Packaging for Automatic Handling

### Tape & Reel

Surface mount and TO-92 devices are available in tape and reel packaging. Surface mount components are retained in an embossed carrier tape by a cover tape. TO-92 device leads are secured to a backing tape by a cover tape. The tape is spooled on standard size reels.

### Ammo Pack

TO-92 devices are also available in an "ammo pack." TO-92 devices are secured to a backing tape by a cover tape and are fanfolded into a box. Ammo packs contain the same quantity, feed direction, and component orientation as a reel.

To order, specify the complete part number with the suffix "AP" (example<sup>†</sup>: MICxxxxx**Z** AP).

### Pricing

Contact the factory for price adder and availability.

# Tape & Reel Standards

Embossed tape and reel packaging conforms to:

- 8mm & 12mm Taping of Surface Mount Components for Automatic Handling, EIA-481-1\*
- 16mm and 24mm Embossed Carrier Taping of Surface Mount Components for Automatic Handling, EIA-481-2\*
- 32mm, 44mm and 56mm Embossed Carrier Taping of Surface Mount Components for Automatic Handling, EIA-481-3\*

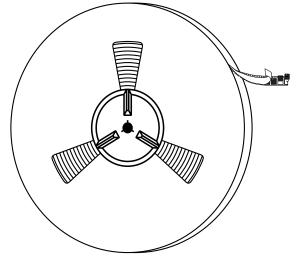
Part Number <sup>†</sup>	Package Description	Quantity / Reel	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MICxxxxxM T&R	8-lead SOIC	2,500	13"	12mm	8mm
	14-lead SOIC	2,500	13"	16mm	8mm
	16-lead SOIC	2,500	13"	16mm	8mm
MICxxxxWM T&R	16-lead wide SOIC	1,000	13"	16mm	12mm
	18-lead wide SOIC	1,000	13"	16mm	12mm
	20-lead wide SOIC	1,000	13"	24mm	12mm
	24-lead wide SOIC	1,000	13"	24mm	12mm
<i>MICxxxx</i> SM T&R	28-lead SSOP	1,000	13"	16mm	12mm
MICxxxxxV T&R	20-lead PLCC	1,000	13"	16mm	12mm
	28-lead PLCC	500	13"	24mm	16mm
	44-lead PLCC	500	13"	32mm	24mm
<i>MICxxxxx</i> <b>M4</b> T&R	SOT-143	3,000	7"	8mm	4mm
<i>MICxxxxx</i> <b>M3</b> T&R	SOT-23	3,000	7"	8mm	4mm
<i>MICxxxxx</i> <b>M5</b> T&R	SOT-23-5	3,000	7"	8mm	4mm
<i>MICxxxxx</i> <b>S</b> T&R	SOT-223	2,500	13"	16mm	12mm
<i>MICxxxxx</i> <b>U</b> T&R	3-lead TO-263	750	13"	24mm	16mm
	5-lead TO-263	750	13"	24mm	16mm
<i>MICxxxxx<b>Z</b></i> T&R	TO-92	2,000	14 <sup>1</sup> /4" <sup>‡</sup>		1/2"

### Packages Available in Tape & Reel

\* Standards are available from: Electronic Industries Associations, EIA Standards Sales Department, tel: (202) 457-4966

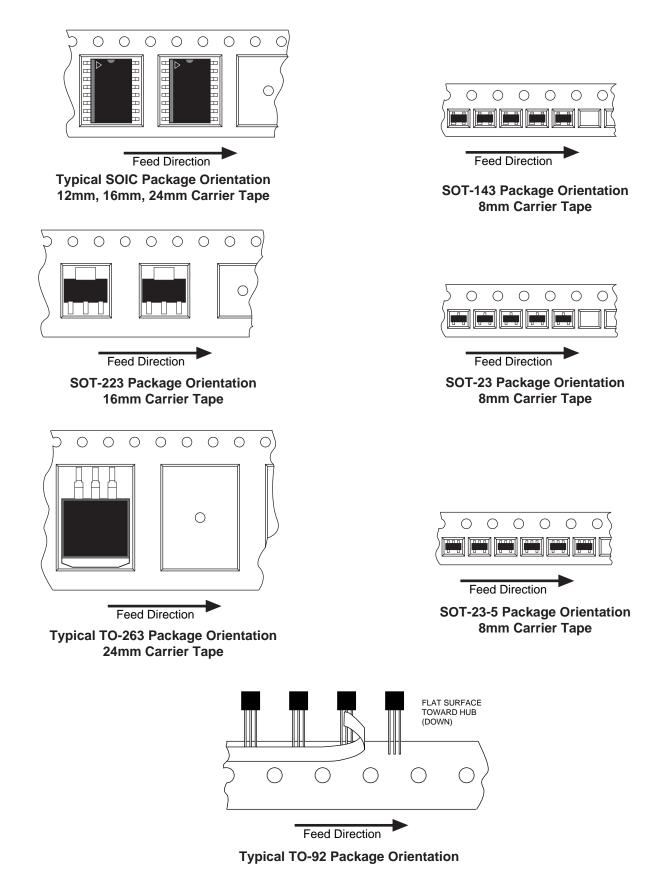
<sup>†</sup> xxxxx = base part number + temperature designation. Example: MIC5201BM T&R

<sup>‡</sup> Cardboard reel

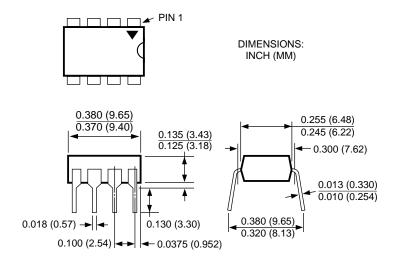


Typical 13" Reel for Surface Mount Components

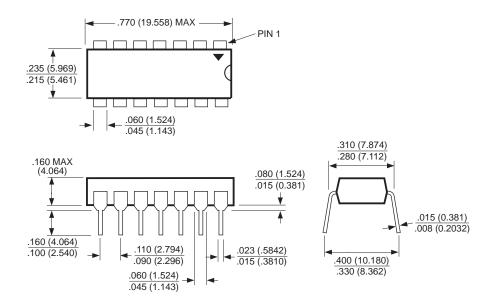
# **Package Orientation**



# **Linear Regulator Packages**

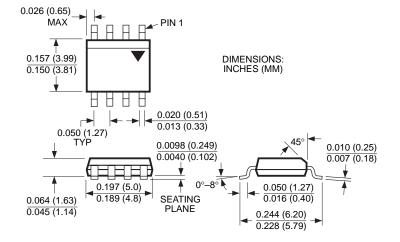




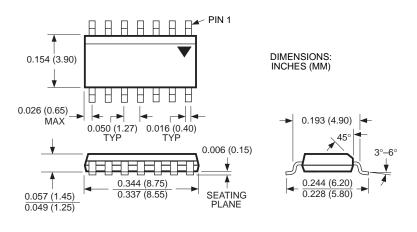


14-Pin Plastic DIP (N)

**Note:** Pin 1 is denoted by one or more of the following: a notch, a printed triangle, or a mold mark.

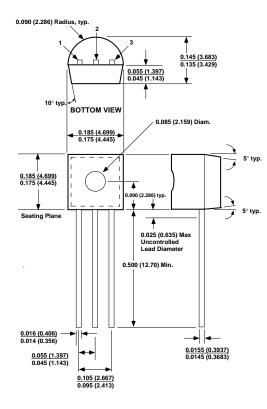




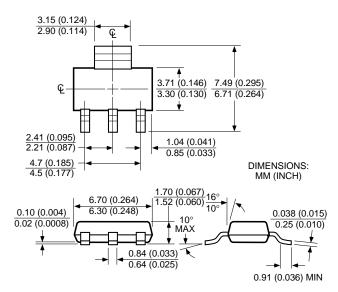


14-Pin SOIC (M)

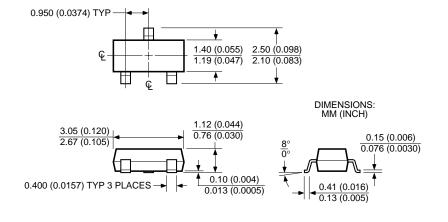
**Note:** Pin 1 is denoted by one or more of the following: a notch, a printed triangle, or a mold mark.



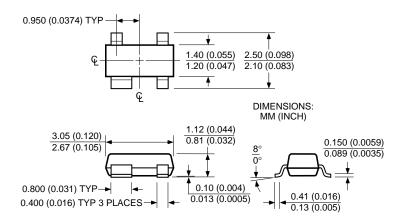




SOT-223 (S)

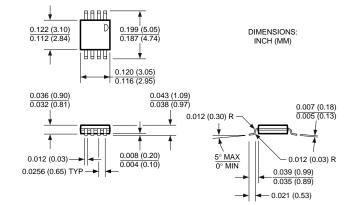




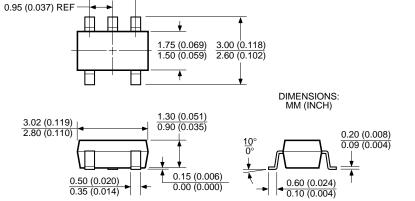


SOT-143 (M4)

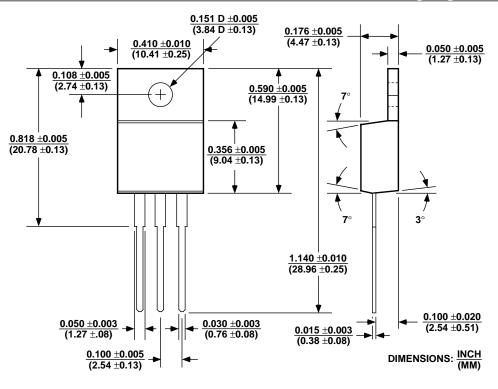
### MSOP-8 [MM8™] (MM)



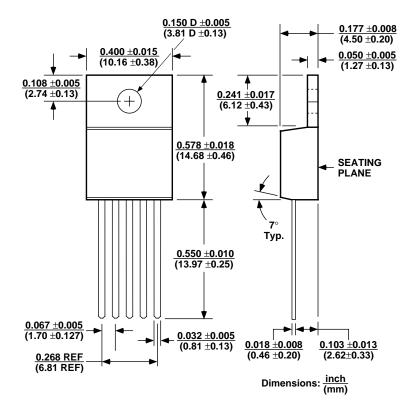




1.90 (0.075) REF -



3-Lead TO-220 (T)



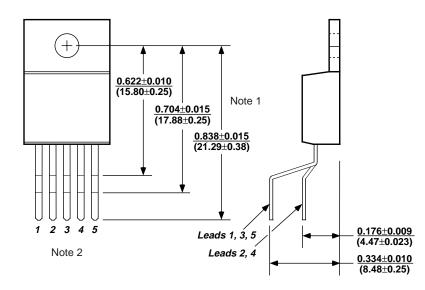
5-Lead TO-220 (T)

Part Number	Package	Lead Form
MICxxxxyT	5-lead TO-220	none (straight)
MICxxxxyT-LB03	5-lead TO-220	vertical, staggered leads, 0.704" seating
MICxxxxyT-LB02	5-lead TO-220	horizontal, staggered leads

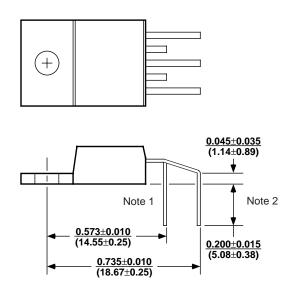
### TO-220 Lead Bend Options Contact Factory for Availability

MICxxxx = base part number, y = temperature range, T = TO-220

\* Leads not trimmed after bending.



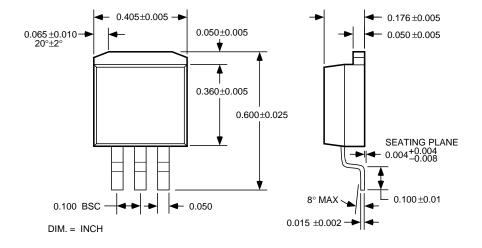




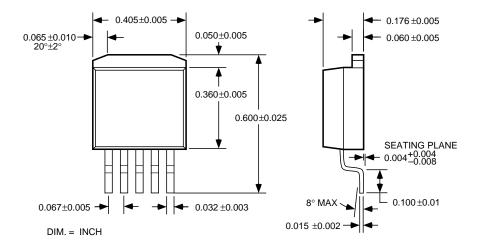
### 5-Lead TO-220 Horizontal Lead Bend Option (-LB02)

Note 1. Lead protrusion through printed circuit board subject to change.

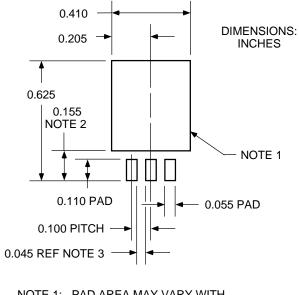
Note 2. Lead ends may be curved or square.





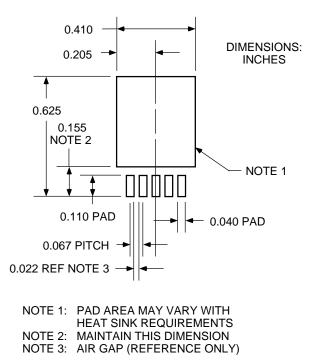


5-Lead TO-263 (U)

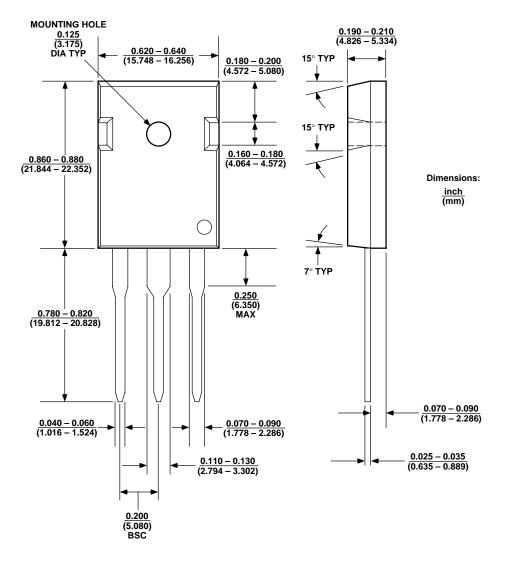


NOTE 1:	PAD AREA MAY VARY WITH
	HEAT SINK REQUIREMENTS
NOTE 2:	MAINTAIN THIS DIMENSION
NOTE 3:	AIR GAP (REFERENCE ONLY)

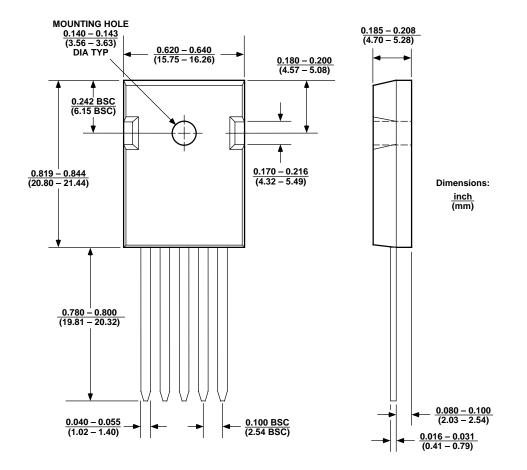




Typical 5-Lead TO-263 PCB Layout



3-Lead TO-247 (WT)



5-Lead TO-247 (WT)

# **Section 7. Appendices**

## List of Appendices

Appendix A. Table of Standard 1% Resistor Values	
Appendix B. Table of Standard $\pm$ 5% and $\pm$ 10% Resistor Values	337
Appendix C. LDO SINK for the HP 48 Calculator	338

## Appendix A. Table of Standard 1% Resistor Values

100	215	464
102	221	475
105	226	487
107	232	499
110	237	511
113	243	523
115	249	536
118	255	549
121	261	562
124	267	576
127	274	590
130	280	604
133	287	619
137	294	634
140	301	649
143	309	665
147	316	681
150	324	698
154	332	715
158	340	732
162	348	750
165	357	768
169	365	787
174	374	806
178	383	825
182	392	845
187	402	866
191	412	887
196	422	909
200	432	931
205	442	953
210	453	976

This table shows three significant digits for standard  $\pm 1\%$  resistor values. These significant digits are multiplied by powers of 10 to determine resistor values. For example, standard resistor values are 0.100 $\Omega$ , 1.00 $\Omega$ , 1.00 $\Omega$ , 1.00 $\Omega$ , 1.00 $\Omega$ , 100 $\Omega$ , etc.

## Appendix B. Table of Standard $\pm 5\%$ and $\pm 10\%$ Resistor Values

(±10% values in **bold**)

10	)
11	
12	
13	
15	
16	
18	
20	
22	
24	
27	
30	
33	
36	
39	
43	
47	
51	
56	
62	
68	
75	
82	
91	

This table shows two significant digits for the standard  $\pm 5\%$  and  $\pm 10\%$  resistor values. These significant digits are multiplied by powers of 10 to determine resistor values. For example, standard resistor values are  $0.1\Omega$ ,  $1.0\Omega$ ,  $1.0\Omega\Omega$ ,  $1.0M\Omega$ ,  $10M\Omega$ , etc.

## Appendix C. LDO SINK for the HP 48 Calculator

The following program, written for the HP 48 calculator, will calculate all power dissipation and heat sink related parameters and ease your design optimization process. It will also graph the resulting heat sink characteristics versus input voltage. The program listing follows the user information. It was written on a HP 48S and runs on both the "S" and the 48G(X) version of the calculator. If you would like to receive the program electronically, send e-mail to Micrel at apps@micrel.com and request program "LDO SINK for the HP48". It will be sent via return e-mail.

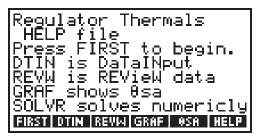
## Using LDO SINK

After loading the program, change to the directory containing it. In the example shown, it is loaded into {HOME MICREL LDO SINK}.

The first screen you will see looks like this:

£	HOME	MICREL	LDO	SINK	ŀ	
4	:					
2	:					
1	:					
F	IRST D	TIN RE	MM G	iraf	0SA	HELP

Pressing the white  $\mathtt{HELP}\xspace$  function key displays a screen of on-line help.

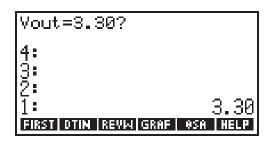


Pressing either FIRST or DTIN will start the program and prompt you for the most commonly changed data. REVW brings up a list of data already entered. GRAF draws the heat sink  $\theta$ SA versus input voltage. SOLVR begins the built-in solve routine that allows you to solve for any variable numerically.

Let's run the program. Press FIRST to begin. Your screen shows:



After a brief pause, the output voltage prompt appears:



Enter a new number and press  $\leftarrow$  CONT to continue. If the data previously entered is still correct, you may simply press  $\leftarrow$  CONT to retain it. Proceed through the list, entering data as prompted and pressing  $\leftarrow$  CONT to continue. You will be prompted for

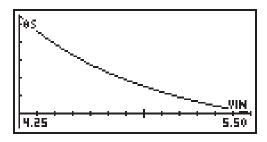
- ${\tt Vout}$   $\,$  the desired regulator output voltage  $\,$
- Iout regulator output current
- Vmax the maximum input voltage
- Vmin the lowest input voltage (used only by the graphing routine
- θjc thermal resistance, junction to case (from the device data sheet)
- $\theta_{\texttt{CS}}$  thermal resistance from the case to the heat sink

After these data are entered, the Review screen appears and confirms your entries.

==Regulator Thermals== Output V: 3.30
Output I: 3.00
Vin: 5.50 0jc: 2.00
0.50 Ambient Temp: 50.00°C
GRAF SOLUS REUM UMAX UMIN NEXT

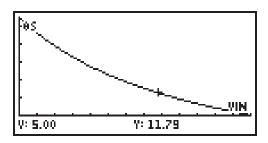
Ambient temperature was not on the list of prompted data. If you wish to change it, press ON (CANCEL) followed by the white NEXT key. Enter the ambient temperature followed by the white TA key. Press the white NEXT key twice to get to the calculation menu. Another variable used but not prompted for is TJM, the maximum junction temperature for the regulator.

You may now press GRAF to calculate and view the  $\theta_{\text{Sa}}$  versus Vin graph, or SOLVR to start the numerical solve routine. If we press GRAF, the following is displayed:



This shows the thermal resistance of the heat sink as the input voltage varies from a low of 4.25V to a high of 5.50V. Pressing ON/CANCEL at this time returns you to the stack display, with  $\theta_{sa}$  at the maximum input voltage displayed.

NOTE: the x-axis is shown beneath the HP 48 graph menu. Press the minus (–) key to toggle between the menu and axis display. Pressing TRACE followed by (X, Y) puts the HP 48 in trace mode and displays the coordinate values of the plot. Press the cursor keys to move around the plot and show voltage (V) versus  $\theta_{Sa}$  and displays the coordinate values of the plot. Press the cursor keys to move around the plot and show voltage (V) versus  $\theta_{Sa}$  and displays the coordinate values of the plot. Press the cursor keys to move around the plot and show voltage (V) versus  $\theta_{Sa}$  and displays the coordinate values of the plot. Press the cursor keys to move around the plot and show voltage (V) versus  $\theta_{Sa}$  (y-axis). Here the cursor has been moved to a Vin of 5.00V and shows a required maximum  $\theta_{Sa}$  of 11.79 C/W.



Pressing ON/CANCEL returns you to the calculation menu. If you hit the white SOLVR key, the HP 48 Solve application is started and you may solve for any of the variables numerically.

4: 3:		
13.		
12:		
	J	

Enter a value and press its white function key to modify variables. Use the HP 48 NXT key to access  $\theta_{jc}$  and  $\theta_{CS}$ . Solve for a variable by pressing the  $\leftarrow$  key followed by the variable's white function key. Press  $\rightarrow$  VIEW (HP 48G) or  $\leftarrow$  REVIEW (HP 48S) to review all variable values.

## **Program Listing**

For those without the HP 48 compatible serial cable or e-mail access, here is the program listing for LDO SINK. "SINK" is installed as a directory. It is 1948.5 bytes long and has a checksum of # 35166d.

STO CLEAR VMAX "Vmax=" VMAX + "?" + PROMPT 'VMAX' STO CLEAR VMIN "Vmin=" VMIN + "?" + PROMPT 'VMIN' STO CLEAR  $\theta JC "\theta jc = " \theta JC +$ "?" + PROMPT ' $\theta$ JC' STO CLEAR  $\theta$ CS " $\theta cs = " \theta cs + "?" +$ PROMPT ' $\theta$ CS' STO REVW >> REVW « CLLCD "==Regulator Thermals==" 1 DISP "Output V: " VO + 2 DISP "Output I: " IO + 3 DISP "Vin: VMAX VMAX 'VIN' STO + 4 DISP "Ambient Temp: " TA + "°C" + 7 DISP " θJC + "θjc: 5 DISP "θcs:  $\theta$ CS + 6 DISP NEX1 TMENU 3 FREEZE >> GRAF « CLLCD "Regulator Thermals Graphing  $\theta$ sa vs Vin" 2 FIX 1 DISP '(TJM-TA)/((1.02\*VIN-VO)\*  $IO) - \theta JC - \theta CS'$  STEQ FUNCTION 'VIN' INDEP VMIN VMAX XRNG VMIN VMAX 'VIN' STO EQ EVAL R+C AXES { "Vin" " $\theta$ S" } AXES AUTO ERASE DRAW DRAX LABEL VMAX 'VIN' STO EQ EVAL 1 TRNC "θsa(min)" →TAG PICTURE >> θsa 1.19549150037 HELP

```
« CLLCD
```

Designing With LDO Regulators

"Regulator Thermals HELP file Press FIRST to begin. DTIN is DaTaINput REVW is REVieW data GRAF shows  $\theta$ sa SOLVR solves numericly" 1 DISP 3 FREEZE ≫ NEX1 { GRAF { "SOLVR" « HS STEQ 30 MENU » } REVW VMAX VMIN { "NEXT" « NEX2 TMENU » } } NEX2 { VO IO VIN TA TJM { "NEXT" « NEX3 TMENU » } } NEX3 {  $\theta$ JC  $\theta$ CS "" "" HELP { "NEXT" « NEX1 TMENU » } } Variables θJC 2 -VMAX 5.5 VMIN 4.25 HS  $\theta sa=(TJM-TA)/$ ((1.02\*VIN-VO)\*IO)- $\theta JC - \theta CS'$ PPAR { (4.25, 6.47110814478)(5.5, 22.6889168766)VIN 0 { (4.25, 8.5864745011)"Vin" "θS" } FUNCTION Y } EQ  $\theta sa = (TJM - TA) /$ ((1.02\*VIN-VO)\*IO)- $\theta JC - \theta CS'$  $\theta CS$  .5 IO 6 VO 3.3 VIN 5.5 TJM 125 TA 75 END

# Section 8. Low-Dropout Voltage Regulator Glossary

Dropout (Voltage)	The minimum value of input-to-output voltage differential required by the regulator. Usually defined as the minimum additional volt- age needed before the regulator's output voltage dips below its normal in-regulation value, and regulation ceases. For example, if an output of 5V is desired, and the regulator has a dropout volt- age ( $V_{DO}$ ) of 0.3V, then at least 5.3V is required on the regulator input.
Enable	Digital input allowing ON/OFF control of the regulator. Also called "control or " <u>shutdown</u> " (see Shutdown, below). Enable denotes positive logic—a high level enables the regulator.
Error Flag	A digital indicator that signals an error condition. Micrel LDOs have optional error flags that indicate the output is not in-regulation be- cause of overcurrent faults, low input voltage faults, or excessively high input voltage faults.
Forced Convection	Heat flow away from a source, such as a regulator or heat sink, aided by forced air flow (usually provided by a fan). See <u>Natural</u> <u>Convection</u> .
Ground Current	The portion of regulator supply current that flows to ground in- stead of to the load. This is wasted current and should be mini- mized. Ground current is composed of <u>quiescent current</u> and base current. (See quiescent current, below). Base current is reduced by using Micrel's proprietary <u>Super βeta PNP<sup>TM</sup></u> process, giving Micrel LDOs the best performance in the industry.
Heat Sink	A conductor of heat attached to a regulator package to increase its power handling ability.
LDO	Low DropOut. Jargon for a linear, low drop out voltage regulator.
Line Transient	The change in regulator output caused by a sudden change in input voltage.
Linear Regulator	A regulator that uses linear control blocks and pass elements, as opposed to a <u>switching regulator</u> . Linear regulators are simple to use, require no magnetic components, and produce extremely clean, well regulated output. Their efficiency varies greatly with input voltage. Linear regulators have approximately the same <i>out-</i> <i>put current</i> as <i>input current</i> .
Load Dump	An automotive industry term for a large positive voltage spike that is created when the alternator's load is suddenly disconnected due to a system fault. The automotive industry considers an elec- tronic component "load dump protected" if it can survive a +60V transient for at least 100msec.

Micrel Semiconductor	Designing With LDO Regulators
Load Transient	The change in output voltage caused by a sudden change in load current.
Natural Convection	Heat flow away from a hot source, such as a regulator or heat sink, unaided by a fan. See <u>Forced Convection</u> .
Overtemperature Shutdown	A protection feature of Micrel regulators that disables the output when the regulator temperature rises above a safe threshold.
Overvoltage Shutdown	A protection feature of some Micrel regulators that disables the output when the input voltage rises above a certain threshold.
Post Regulator	A method of reducing output ripple by following a <u>switching regu-</u> lator with a linear regulator.
Quiescent Current	Current used by the regulator for housekeeping. Quiescent cur- rent does not contribute to the load and should be minimized. In a PNP LDO, ground current equals quiescent when the output cur- rent is 0mA.
Reversed-Battery Protection	A regulator with reversed battery protection will not be destroyed if the input supply polarity is backwards. A related feature allows Micrel LDOs to effectively act as an "ideal" diode, protecting the load from this backward polarity condition, or allowing the outputs of different output-voltage regulators to be "ORed" without dam- age.
Shutdown	Digital input allowing ON/OFF control of the regulator. Also called "control" or " <u>enable</u> ". Shutdown denotes negative logic—a logic low enables the regulator.
Super ßeta PNP™	Micrel's trademarked name for a power semiconductor process combining good high voltage operation with high transistor beta (current gain). Compared to standard power PNP transistor betas of only 8 to 10, Super ßeta PNP-processed transistors feature nominal betas of 50 to 100. LDO efficiency depends on high beta: efficiency at high load current is proportional to the PNP pass transistor beta. High beta means low ground current which im- proves efficiency; this allows high output with less wasted power than other monolithic linear regulators, either standard or low-drop- out.
Super LDO	The MIC5156, MIC5157, and/or MIC5158. Linear regulator con- trollers that drive external N-channel power MOSFETs. Output current and dropout voltage are dependant upon the MOSFET employed. Using the Super LDO with large MOSFETs allow ex- tremely low dropout voltage and very high output currents.
Switching Regulator	Also known as SMPS (Switch Mode Power Supply). Voltage regu- lator topology that uses ON/OFF switching to efficiently regulate voltage. Magnetics (inductors and/or transformers) are generally used. Ideal switching regulators have nearly the same <i>output power</i> as <i>input power</i> , resulting in very high efficiency. Switching regula- tors usually have inferior output characteristics, such as noise and voltage regulation, compared to linear regulators.

# **Section 9. References**

## **Thermal Information**

Micrel Databook, Micrel Inc., San Jose, CA. Tel: + 1 (408) 944-0800

MIL-STD-275E: Printed Wiring for Electronic Equipment. (31 December 1984)

*Innovative Thermal Management Solutions*, Wakefield Engineering, 60 Audubon Road, Wakefield, MA 01880. Tel: + 1 (617) 245-5900

Spoor, Jack: Heat Sink Applications Handbook, 1974, Aham, Inc.

*Technical Reports and Engineering Information Releases*, Thermalloy Inc., Dallas Texas. Tel: + 1 (214) 243-4321

Thermal Management, AAVID™ Engineering, Inc., Laconia, NH. Tel: + 1 (603) 528-3400

Thermal Management Solutions, Thermalloy Inc., Dallas Texas. Tel: + 1 (214) 243-4321

## **4-Lead Resistor Manufacturers**

Dale Electronics, Columbus, NE. Tel: + 1 (402)563-6506

Vishay Resistors, Malvern, PA. Tel: + 1 (215) 644-1300

# **Section 10. Index**

## Α

Accuracy. See Voltage accuracy

## В

Bandgap. *See* References (voltage) Battery 26

## С

Capacitance 26 Capacitors 25 across battery 26 bypass 26 effective series resistance 25 filter 26 Cellular telephones 47 Computer power supplies 39 Copper wire resistance 70 Current source 37 Super LDO 37 using op amps 37

## D

Design issues 10 Dropout 341 Dropout voltage 10

## Ε

Efficiency 11, 32 Enable pin 341 Error Flag 341

## F

Filter capacitor. *See* Capacitors Forced Convection 341

### G

Glossary 341 Ground current 10, 341 Ground loop 26

### Η

Heat sink 27, 48, 341 charts for high current regulators 51 for surface mount packages 57 mounting multiple devices 55 reading manufacturer's graphs 53 selection 53 size reduction via power sharing resistor 54 High input voltage operation 34

## I

Inrush surge, controlling 34 Isolation 47

## Κ

Kelvin sensing 26, 70

## L

Layout 25 Lead bending 27 Lead forming. *See* Lead bending Line transient 341 Linear regulator 341 Linear regulator benefits 9 Load dump 341 Load transient 342 LP2950/2951 102

### Μ

MIC29150/29300/29500/29750 Series 140 MIC2920A/29201/29202/29204 76 MIC29310/29312 155 MIC2937A/29371/29372 85 MIC2940A/2941A 94 MIC2950/2951 116 MIC29510/29512 163 MIC2954 130 MIC29710/29712 171 MIC39150/39151 179 MIC39300/39301 188 MIC5156/5157/5158 310 MIC5200 197 MIC5201 203 MIC5202 211 MIC5203 217 MIC5205 223 MIC5206 231 MIC5207 238 MIC5208 246 MIC5209 252 MIC5210 263 MIC5211 272

MIC5216 280 MIC5219 291 MIC5237 303 Microprocessor supplies 39 accuracy 43 dropout requirement 39 heat sink calculations 52 multiple output 44 using a current-boosted MIC2951 41 using a monolithic LDO 40 using the MIC5156 40 using the MIC5158 41

## Ν

Natural convection 342 Noise 32 effects on VCOs 46 reference. *See* References (voltage): noise

## 0

Overtemperature shutdown 342 Overvoltage shutdown 64, 342

### Ρ

Packages 64 Packaging 14-Pin Plastic DIP (N) 324 14-Pin SOIC (M) 325 3-Lead TO-220 (T) 329 5-Lead TO-220 (T) 329 8-Pin MSOP (MM8) 328 8-Pin Plastic DIP (N) 324 8-Pin SOIC (M) 325 SOT-143 (M4) 327 SOT-223 (S) 326 SOT-23 (M3) 327 SOT-23-5 (M5) 328 TO-220 Horizontal Lead Bend Option -LB02 330 TO-220 Vertical Lead Bend Option -LB03 330 TO-247 (WT) 333, 334 TO-263 (U) 331 TO-263 PCB Layout 332 TO-92 (Z) 326 Packaging for Automatic Handling 322 package orientation 323 Tape & Reel 322 Paralleling regulators bipolar 65 on one heat sink 55 Super LDO 68 Portable equipment 46 Post regulator 342 Power dissipation by package type, graph 17 Preregulator 34

## Q

Quiescent current 342

### R

References (bibliography) 343 References (voltage) 28, 29, 32 noise 32 Resistance Copper Wire (table) 70 Printed Circuit Board (table) 71 Resistors Standard ±5% and ±10% Value Table 337 Standard 1% Value Table 336 Reversed-battery protection 63, 342

## S

Sequencing multiple supplies 45, 47 Shutdown 342 Sleep mode 47 Split supplies, problems with 33 Stability 32, 65 Super Beta PNP regulators 61 dropout voltage 62 family list 61 ground current 63 overvoltage shutdown 64 paralleling 65 reverse-polarity characteristics 63 simplified schematic 62 "Super LDO" 67, 342 comparison to monolithics 68 current limit 70 current limit sense resistor 70 unique applications 68 Switching regulators 342 comparison to LDO 12

## Т

Thermals 48 calculator program 52, 338 definition of parameters 48 electrical analogy 48 example calculations 52 heat flow 49 maximum junction temperature 50 primer 48 thermal resistance 49 Transients 28 improving response 42 Troubleshooting guide 60

## V

Voltage accuracy 26, 28, 29

	_			+	_				_						+		_	$\left  \right $					+	_	_			_		_		$\vdash$	
			++	+	+		+ +	+	_			$\vdash$			++	++	_	$\left  \right $	++		++	++	+ +		-			+		-		++	++-
	-			++	+													+					+		+			+		+		++	
	_																															$\vdash$	
	_			+	_		+					$\vdash$			+	++	_		+		+	++		_	_							$\vdash$	++-
	_				-																							-				++	
				+																								+		-			
	_			+											_	$\rightarrow$								_				_				$\vdash$	
	_			+			+		_								_															++	
				++			++					$\vdash$		+	+	++			++		++	++		-	-			+		-		++	++-
$\square$				+	+		$\parallel$	+		+		$\square$			+	+	+	Н	+			+	+1								$\square$	$\square$	
+ +	-	$\vdash$	++	+	+		++	+		+	$\vdash$	$\left  \right $	$\left  \right $	+	+	+	+	$\left  \right $	+		++	+	+		+	++	+	_	+		++	++	+
$\left  + \right $	+	++	++	+	+	$\vdash$	++	+		+	$\vdash$	$\left  \right $		+	+	+	+	+	+		++	++	+		+	+		+	+	+	++	++	+
			++	++			++					+		++				+			++					++			+	-	++	++	++
$\square$		$\square$		$\square$								$\square$				$\square$		ЦĨ	$\square$				$\square$						$\square$			$+ \square$	+ -
+ +	+	$\vdash$	++	+	_						$\vdash$	$\vdash$	$\left  \right $	$\left  \right $			_	$\left  \right $	+						_	+			$\left  \right $	_	++	++	++
$\left  + \right $				+	+	$\vdash$	+				$\vdash$	$\left  \right $	+	++			+	+	+		++		+		-				+	-	+	++-	
	-			++	+													+							-			+		-		++	
	_				_		+					$\square$				+			+		++	++		_								$\vdash$	+
	_			++	+				_							+	_	$\vdash$					+	_	_			_		_		$\vdash$	
					+													+							-			-				++-	
	_				_		+ +									+			+			+ +		_								$\vdash$	
				++	+		+		_			$\vdash$			+	++	_	++	+		++	+	+	_	-		-	+		-		$\vdash$	++-
					-																											++	
					+																											$\square$	
	_				_		+					$\square$			+	++	_		+		++	++		_								$\vdash$	++
	_			++	+-		+		_			$\vdash$			+	++	_	$\vdash$	+		+	++	+	_	_			+		-		$\vdash$	++-
$\left  + \right $		++	++	+	+	$\vdash$	+				$\vdash$	$\vdash$	++	++			+	+	+		++	++			+			+	+	-	++	++	+
	+	$\vdash$	++	$\uparrow \uparrow$	+		$\uparrow \uparrow$				$\vdash$						+	$\uparrow \uparrow$			++	++	+		+		+	+	++	+		++	
		$\square$	++	+	_		$\parallel$				$\vdash$			$\square$	+	+	_	$\square$	+		+		+		_	+			$\square$	_		++	++
	_	$\vdash$	++	+	_	$\vdash$	+	+		+	$\vdash$	$\vdash$		$\vdash$		+	_	+	+		+						+	_	+	-	$\vdash$	++	+
	+	++	++	++	+	$\vdash$	++	+	+	+	$\vdash$	$\left  \right $	++	++	+	+	+	+	++	+	++	++	+		+	++	+	+	++	+	++	++	++
								$\square$										$\square$	$\square$				$\square$										
+ +	_	$\square$	++		_	$\square$	$\parallel$				$\square$						_	$\square$	+		$\parallel$		+			+				_	$\left  \right $	++	+
$\left  + \right $	+	++	++	+	+	$\vdash$	++	+		+	$\vdash$	$\vdash$	$\left  \right $	++		+	+	+	+		++	++	+	+	+	++	+	+	+	-	++	++	++
	+	++	++	++	+	$\vdash$	++	+			$\vdash$	$\vdash$	++	++	+	+	+	+	+		++	++			+	++		+	+	+	++	++	++
		$\square$					$\parallel$				$\vdash$			$\square$			-	$\square$			++								$\square$			++	
$\square$				+	+			+							+	+	+		+				+									$\square$	
		$\vdash$	++	++	+	$\vdash$	++	+	+	+	$\vdash$	$\left  \right $	++	++	+	+	+	++	+	+	++	++	+		+	+	+	+	++	+	++	++	++
		1 1	++	+	-	$\vdash$	++	+			$\vdash$	$\vdash$		+	+	+	+	$\vdash$	+	-	++	++	+		-	++		+	+	-	$\vdash$	++	+
				+ +	-		++	+			$\vdash$	+		++			+	+	+		++	++			+	++		+	+	+	++	++	++
								_		-																+ +	+	-	1		1 1	+-+-	

# Section 11. Worldwide Representatives and Distributors

### **CONTENTS**

Micrel Sales Offices	
U.S. Sales Representatives	
U.S. Distributors	
International Sales Representatives and Distributors	

### **Micrel Sales Offices**

MICREL SEMICONDUCTOR CORPORATE OFFICE

Tol: (408)

Tel: (408) 944-0800 Fax: (408) 944-0970

### MICREL WORLD WIDE WEBSITE

http://www.micrel.com

### MICREL RESOURCE CENTER

literature requests only (800) 401-9572

### MICREL EASTERN AREA SALES OFFICE

93 Branch St. Medford, NJ 08055

1849 Fortune Dr.

San Jose, CA 95131

Tel: (609) 654-0078 Fax: (609) 654-0989

### MICREL CENTRAL AREA SALES OFFICE

Suite 450C-199 120 South Denton Tap Coppell, TX 75019

Tel: (972) 393-3603 Fax: (972) 393-9186

### MICREL WESTERN AREA SALES OFFICE

 3250 Scott Blvd.
 Tel: (408) 914-7670

 Santa Clara, CA 95054
 Fax: (408) 914-7878

### MICREL MEXICO, CENTRAL AMERICA, AND SOUTH AMERICA SALES OFFICE

Suite 450C-199 120 South Denton Tap Coppell, TX USA 75019

Tel: + 1 (972) 393-3603 Fax: + 1 (972) 393-9186

### MICREL SEMICONDUCTOR ASIA LTD.

4F. Jinsol Building 826-14, Yeoksam-dong Kangnam-ku Te Seoul 135-080 Fa Korea

Tel: + 82 (2) 3466-3000 Fax: + 82 (2) 3466-2999

### MICREL SEMICONDUCTOR, TAIWAN

12F-10, No. 237 Sec. 2, Fu-Hsing South Rd. Tel: + 886 (2) 2705-4976 Taipei, Taiwan, R.O.C. Fax: + 886 (2) 3466-2999

### MICREL EUROPE TECHNICAL CENTER

 Clere House
 Tel: + 44 (1635) 524455

 21 Old Newtown Road
 Tel: + 44 (1635) 524455

 Newbury
 Fax: + 44 (1635) 524466

 United Kingdom RG 147DP
 Fax: + 44 (1635) 524466



Tel: (256) 533-2444

Tel: (408) 944-0800

Tel: (602) 438-7424

Fax: (602) 414-1125

Tel: (408) 944-0800

Tel: (619) 279-0420

Fax: (619) 279-7650

Tel: (714) 739-8891

Fax: (714) 739-1604

Tel: (203) 288-7005

Fax: (203) 281-4233

Tel: (609) 933-1541

Fax: (609) 933-1520

Tel: (813) 572-8895 Fax: (813) 572-8896

Tel: (407) 365-3283

Fax: (407) 365-3727

Tel: (678) 380-5080 Fax: (678) 380-5081

Fax: (256) 536-4031

## **U.S. Sales Representatives**

MARYLAND

Tri-Mark, Inc. 1131L Benfield Blvd.

Millersville, MD 21108

**MASSACHUSETTS** 

125 Conant Rd.

Weston, MA 02193

99 South Bedford St.

Burlington, MA 01803

### ALABAMA

CSR Electronics
Suite 931
303 Williams Ave.
Huntsville. AL 35801

### ALASKA

contact factory

### ARIZONA

S & S Technologies Suite 121 4545 South Wendler Dr. Tempe, AZ 85282

### ARKANSAS

contact factory

### CALIFORNIA (NORTHERN)

BAE Sales, Inc.	
Suite 315W	
2001 Gateway Pl.	Tel: (408) 452-8133
San Jose, CA 95110	Fax: (408) 452-8139

### CALIFORNIA (SOUTHERN)

CK Associates	
Suite 102	
8333 Clairmont Mesa Blvd.	
San Diego, CA 92111	

Select	Electronics

Bldg. F, Suite 106 14730 Beach Blvd. La Mirada, CA 90638

### **COLORADO**

Waugaman Associates, Ir	IC.
Suite 202	

1300 Plaza Court North Tel: (303) 926-0002 Lafayette, CO 80026 Fax: (303) 926-0828

### CONNECTICUT

Datcom Technologies One Evergreen Ave. Hamden, CT 06518

### DELAWARE

Harwood Associates
242 Welsh Ave.
Bellmawr, NJ 08031

### FLORIDA

3696 Ulmerton Rd.

Clearwater, FL 33762

Suite 222 1750 West Broadway St. Oviedo, FL 32765

### GEORGIA

CSR Electronics, Inc.
Suite 120
3555 Koger Blvd.
Duluth, GA 30338

### HAWAII

contact factory

### **IDAHO (NORTHERN)**

**ECS/SPS Electronics** Suite 120 9311 Southeast 36th Mercer Island, WA 98040

### **IDAHO (SOUTHERN)**

Waugaman Associates, Inc. 876 East Vine St. Salt Lake City, UT 84107

### ILLINOIS (NORTHERN)

Sumer, Inc. 1675 Hicks Rd.

### ILLINOIS (SOUTHERN)

**IRI of Kansas** Suite 149 4203 Earth City Expressway Earth City, MO 63045

### INDIANA

Technology Marketing Corpo	<b>ration</b>
1526 East Greyhound Pass	Tel: (317) 844-8462
Carmel, IN 46032	Fax: (317) 573-5472
4630-10 West Jefferson Blvd.	Tel: (219) 432-5553
Fort Wayne, IN 46804	Fax: (219) 432-5555
1218 Appletree Ln.	Tel: (765) 454-2000
Kokomo, IN 46902	Fax: (765) 457-3822
IOWA	

#### J

Fel: (319) 393-2232 1 С ax: (319) 393-0109

**IRI of Kansas** Suite 240 10000 College Blvd. Tel: (913) 338-2400 Overland Park, KS 66210 Fax: (913) 338-0404 13 Woodland Dr. Tel: (316) 775-2565 Augusta, KS 67010 Fax: (316) 775-3577

### KENTUCKY

#### Тес Sui 100 3) 253-1808 6) 253-1662 Lex

LOUISIANA

### MAINE

3D Sales Suite 116 99 South Bedford St. Burlington, MA 01803

Tel:	(408) 944-0800

# Fax: (801) 261-0830

Tel: (847) 991-8500

Rolling Meadows, IL 60008 Fax: (847) 991-0474

> Tel: (314) 298-8787 Fax: (314) 298-9843

### 10

I.R. Sales Engineering	
930 St. Andrews, NE	Т
Cedar Rapids, IA 52402	Fa

### KANSAS

chnology Marketing Corporation			
ite 1A			
0 Trade St.	Tel:	(606)	
xington, KY 40511	Fax:	(606)	

contact factory

Tel:	(206) 232-9301	
Fax:	(206) 232-1095	
Tel:	(801) 261-0802	

## MICHIGAN

Suite 116

**Technology Marketing Corporation** Suite 109 25882 Orchard Lake Rd. Tel: (248) 473-8733 Farmington Hills, MI 48336 Fax: (248) 473-8840

Byrne Associates (Digital Equipment Corp. only)

3D Sales (except Digital Equipment Corp.)

Tel: (410) 729-7350

Fax: (410) 729-7364

Tel: (781) 899-3439

Fax: (781) 899-0774

Tel: (781) 229-2999

Fax: (781) 229-2033

### **MINNESOTA**

The Twist Company	
3433 Broadway St., NE	Tel: (613) 331-1212
Minneapolis, MN 55413	Fax: (613) 331-8783

### MISSISSIPPI

CSR Electronics	
Suite 931	
303 Williams Ave.	Tel: (205) 533-2444
Huntsville, AL 35801	Fax: (205) 536-4031

Tel: (314) 298-8787 Earth City, MO 63045 Fax: (314) 298-9843

### MONTANA

Suite 202	
	(303) 926-0002 (303) 926-0828

### NEBRASKA

J.R. Sales Engineering	
1930 St. Andrews, NE	Tel: (319) 393-2232
Cedar Rapids, IA 52402	Fax: (319) 393-0109

### NEVADA (NORTHERN)

BAE Sales, Inc.	
Suite 315W	
2001 Gateway Pl.	Tel: (408) 452-8133
San Jose, CA 95110	Fax: (408) 452-8139

### NEVADA (CLARK COUNTY)

S & S Technologies	
Suite 121	
4545 South Wendler Dr.	Tel: (602) 438-7424
Tempe, AZ 85282	Fax: (602) 414-1125

### **NEW HAMPSHIRE**

3D Sales	
Suite 116	
99 South Bedford St.	Tel: (781) 229-2999
Burlington, MA 01803	Fax: (781) 229-2033

Tel: (408) 944-0800

Tel: (781) 229-2999

Fax: (781) 229-2033

Hu MISSOURI

**IRI of Kansas** Suite 149 4203 Earth City Expressway

NEW JERSEY (NORTHERN)		OKLAHOMA		TEXAS (EL PASO COUNTY)	
Harwood Associates		contact factory	Tel: (408) 944-0800	S & S Technologies	
34 Lancaster Ave. Maplewood, NJ 07040	Tel: (973) 763-0706 Fax: (973) 763-2432	OREGON		Suite 121 4545 South Wendler Dr.	Tel: (602) 438-7424
		ECS/SPS Electronic Sales Inc	ornorated	Tempe, AZ 85282	Fax: (602) 414-1125
NEW JERSEY (SOUTHER	(N)	128 North Shore Cir.	Tel: (503) 697-7768	UTAH	
Harwood Associates 242 Welsh Ave.	Tel: (609) 933-1541	Oswego, OR 97034	Fax: (503) 697-7764	Waugaman Associates, Inc.	
Bellmawr, NJ 08031	Fax: (609) 933-1520	PENNSYLVANIA (EAST)		876 East Vine St. Salt Lake City, UT 84107	Tel: (801) 261-0802 Fax: (801) 261-0830
329 East Elm Ave.	Tel: (609) 783-2689	Harwood Associates		,,	( ,
Lindenwold, NJ 08021	Fax: (609) 783-5332	242 Welsh Ave.	Tel: (609) 933-1541	VERMONT	
NEW MEXICO		Bellmawr, NJ 08031	Fax: (609) 933-1520	3D Sales	
		PENNSYLVANIA (WEST)		Suite 116	
S & S Technologies				99 South Bedford St.	Tel: (781) 229-2999
Suite 121 4545 South Wendler Dr.	Tel: (602) 438-7424	Technology Marketing Corpor	ation	Burlington, MA 01803	Fax: (781) 229-2033
Tempe, AZ 85282	Fax: (602) 414-1125	Suite 206A 20399 Route 19 North	Tel: (724) 779-2140	VIRGINIA	
		Cranberry Township, PA 16066			
NEW YORK (METRO)				Tri-Mark, Inc.	
Harwood Associates		RHODE ISLAND		1131L Benfield Blvd. Millersville, MD 21108	Tel: (410) 729-7350 Fax: (410) 729-7364
25 High St.	Tel: (516) 673-1900	3D Sales		Willersville, WD 21100	Tax. (410) 723-7304
Huntington, NY 11743	Fax: (516) 673-2848	Suite 116		WASHINGTON	
		99 South Bedford St.	Tel: (781) 229-2999		
NEW YORK (UPSTATE)		Burlington, MA 01803	Fax: (781) 229-2033	ECS/SPS Electronics Suite 120	Tel: (206) 232-9301
Harwood Associates		SOUTH DAKOTA		9311 Southeast 36th	Tel: (503) 697-7768
25 High St.	Tel: (516) 673-1900			Mercer Island, WA 98040	Fax: (206) 232-1095
Huntington, NY 11743	Fax: (516) 673-2848	contact factory	Tel: (408) 944-0800		
NORTH CAROLINA		SOUTH CAROLINA		WASHINGTON D.C.	
CSR Electronics, Inc.				Tri-Mark, Inc.	
Suite 2		CSR Electronics, Inc. Suite 2		1131L Benfield Blvd. Millersville, MD 21108	Tel: (410) 729-7350 Fax: (410) 729-7364
5848 Faringdon Pl.	Tel: (919) 878-9200	5848 Faringdon Pl.	Tel: (919) 878-9200	Willersville, WD 21100	Fax. (410) 729-7304
Raleigh, NC 27609	Fax: (919) 878-9117	Raleigh, NC 27609	Fax: (919) 878-9117	WEST VIRGINIA	
NORTH DAKOTA		TENNEOOFE		Technology Marketing Corner	otion
NORTH DAROTA		TENNESSEE		Technology Marketing Corpor Suite 206A	ation
contact factory	Tel: (408) 944-0800	CSR Electronics		20399 Route 19 North	Tel: (724) 779-2140
оню		Suite 931	T-1 (005) 500 0444	Cranberry Township, PA 16066	Fax: (724) 779-4785
OHIO		303 Williams Ave. Huntsville, AL 35801	Tel: (205) 533-2444 Fax: (205) 536-4031	MISCONSIN	
Technology Marketing Corp	oration		1 4.4. (200) 000 1001	WISCONSIN	
Suite 3	Tal: (512) 004 6720	TEXAS		Sumer, Inc.	
7775 Cooper Rd. Cincinnati, OH 45242	Tel: (513) 984-6720 Fax: (513) 936-6515	Bravo Sales		13555 Bishops Ct.	Tel: (414) 784-6641
		Suite 150		Brookfield, WI 53005	Fax: (414) 784-1436
Suite 200		515 Capital of TX Hwy. South	Tel: (512) 328-7550	WYOMING	
One Independence PI. 4807 Rockside Rd.	Tel: (216) 520-0150	Austin, TX 78746	Fax: (512) 328-7426		
Cleveland, OH 44131	Fax: (216) 520-0190	Suite 375		Waugaman Associates, Inc. Suite 202	
		16801 Addison Rd.	Tel: (972) 250-2900	Suite 202 1300 Plaza Court North	Tel: (303) 926-0002
		Dallas, TX 75248	Fax: (972) 250-2905	Lafayette, CO 80026	Fax: (303) 926-0828
		Suite 308			
		Willowbrook Pl. 1			
		17314 State Hwy 249	Tel: (281) 955-7445		

17314 State Hwy. 249 Houston, TX 77064 Tel: (281) 955-7445 Fax: (281) 539-2728



## **U.S. Distributors**

**Future Electronics** 

27489 West Agoura Rd.

Agoura Hills, CA 91301

Tel: (818) 865-0040

Tel: (800) 876-6008

Fax: (818) 865-1340

Tel: (714) 250-4141

Tel: (800) 950-2147

Fax: (714) 453-1226

Tel: (619) 625-2800

Fax: (619) 625-2810

Tel: (818) 757-2000

Fax: (818) 708-7436

Tel: (619) 691-0141

Fax: (619) 691-0172

Tel: (909) 980-2105

Tel: (619) 453-8211

Fax: (619) 535-9883

Tel: (562) 929-9722

Fax: (562) 864-7110

Tel: (805) 449-1480

Fax: (805) 449-1460

Tel: (714) 470-1011

Fax: (714) 470-1104

Tel: (619) 576-0088 Fax: (619) 576-0990

Tel: (805) 370-1515

Fax: (805) 370-1525

Tel: (303) 428-2400

Fax: (303) 428-3007

Tel: (303) 255-2180

Fax: (303) 255-2226

Tel: (303) 237-1400

Fax: (303) 232-2009

Tel: (303) 373-4540

Fax: (303) 373-0648

Rancho Cucamonga, CA 91730 Fax: (909) 980-9270

Suite 300

Suite 200

Suite 220

25B Technology

Irvine, CA 92618

5151 Shoreham Pl.

San Diego, CA 92122

6925 Canby, Bldg. 109

Reseda, CA 91335

Newark Electronics

Chula Vista, CA 91910

660 Bay Blvd

9045 Haven Ave.

9444 Waples St.

San Diego, CA 92121

325 East Hillcrest Dr.

13900 Alton Pkwy.

4360 View Ridge Ave.

San Diego, CA 92123

Thousand Oaks, CA 91361

850 Hampshire Rd.

Irvine, CA 92618

12631 East Imperial Hwy.

Santa Fe Springs, CA 90670

Thousand Oaks, CA 91360

Nu Horizons Electronics Corp.

Suite 102

Bldg. F

Suite 123

Suite B

Suite R

Suite 308

Suite B150

FAI

1333 West 120th Ave.

Westminster, CO 80234

12600 West Colfax Ave.

Lakewood, CO 80215

Newark Electronics

Denver, CO 80239

CONNECTICUT

4725 Paris St.

Jan Devices Incorporated

### D

DIE DISTRIBUTION				
<b>Chip Supply, Inc.</b> 7725 Orange Blossom Trail Orlando, FL 32810			298-7100 290-0164	
PACKAGED DEVICES				
ALABAMA				
Bell Industries Suite 140 8215 Hwy. 20 West Madison, AL 35758	Tel: Fax:	(205) (205)	464-8646 464-8655	
EBV Electronics Suite 16 4835 University Square Huntsville, AL 35816			721-8720 721-8725	
Future Electronics Suite 400 A 6767 Old Madison Pike Huntsville, AL 35806			971-2010 922-0004	
<b>Newark Electronics</b> 150 West Park Loop Huntsville, AL 35806			837-9091 837-1288	
Nu Horizons Electronics Corp. Suite 10 4835 University Square Huntsville, AL 35816	Tel:		722-9330 722-9348	
ARIZONA				
Bell Industries Suite 500 7025 East Greenway Pkwy Scottsdale, AZ 85254			905-2355 905-2356	
	i ux.	· /		
FAI Suite 245 4636 East University Dr. Phoenix, AZ 85034	Tel:	(602)	731-4661 731-9866	
FAI Suite 245 4636 East University Dr.	Tel: Fax: Tel:	(602) (602) (602)		
FAI Suite 245 4636 East University Dr. Phoenix, AZ 85034 Future Electronics Suite 245 4636 East University Dr.	Tel: Fax: Tel: Fax: Tel:	(602) (602) (602) (602) (602)	731-9866 968-7140	
FAI Suite 245 4636 East University Dr. Phoenix, AZ 85034 Future Electronics Suite 245 4636 East University Dr. Phoenix, AZ 85034 Newark Electronics 1600 West Broadway Rd.	Tel: Fax: Tel: Fax: Tel:	(602) (602) (602) (602) (602)	731-9866 968-7140 968-0334 966-6340	
FAI Suite 245 4636 East University Dr. Phoenix, AZ 85034 Future Electronics Suite 245 4636 East University Dr. Phoenix, AZ 85034 Newark Electronics 1600 West Broadway Rd. Tempe, AZ 85282	Tel: Fax: Tel: Fax: Tel: Fax: Tel: Tel:	(602) (602) (602) (602) (602) (602) (602)	731-9866 968-7140 968-0334 966-6340	
FAI Suite 245 4636 East University Dr. Phoenix, AZ 85034 Future Electronics Suite 245 4636 East University Dr. Phoenix, AZ 85034 Newark Electronics 1600 West Broadway Rd. Tempe, AZ 85282 ARKANSAS Newark Electronics 10816 Executive Center Dr.	Tel: Fax: Tel: Fax: Tel: Fax: Tel: Tel:	(602) (602) (602) (602) (602) (602) (602)	731-9866 968-7140 968-0334 966-6340 966-8146 225-8130	
FAI Suite 245 4636 East University Dr. Phoenix, AZ 85034 Future Electronics Suite 245 4636 East University Dr. Phoenix, AZ 85034 Newark Electronics 1600 West Broadway Rd. Tempe, AZ 85282 ARKANSAS Newark Electronics 10816 Executive Center Dr. Little Rock, AR 72211	Tel: Fax: Tel: Fax: Tel: Fax: Tel: Fax:	(602) (602) (602) (602) (602) (602) (501) (501) (501) (916) (916)	731-9866 968-7140 968-0334 966-6340 966-8146 225-8130	

### Δ

### в

### Т

### С

3001 D	bugias	Biva.
Rosevil	le, CA	95661

### 1161 North Fairoaks Ave.

### Sunnyvale, CA 94089 **EBV Electronics**

1295 Oakmead Pkwy. Sunnyvale, CA 94086

7) 290-0104	2220 C San Jo
	<b>Future</b> Suite 2 3009 D Rosevi
5) 464-8646 5) 464-8655	2220 C San Jo
5) 721-8720 5) 721-8725	<b>Newar</b> 3600 V Palo Al
5,721-0725	2020 H

Suite 215 3009 Douglas Blvd. Roseville, CA 95661

FAI

'Toole Ave. se, CA 95131

Electronics 210 ouglas Blvd. ille, CA 95661

O'Toole Ave. se, CA 95131

k Electronics Vest Bayshore Rd. Ito, CA 94303

lurley Way Sacramento, CA 95825

**Nu Horizons Electonics** 2070 Ringwood Ave. San Jose, CA 95131

### CALIFORNIA (SOUTH

### **Bell Industries**

2201 East El Segundo Blv El Segundo, CA 90245 Suite 100 220 Technology Dr. Irvine, CA 92618 Suite 300 6835 Flanders Dr. San Diego, CA 92121 Suite 110

125 Auburn Ct. Westlake Village, CA 913

### **EBV Electronics**

Suite 450 2 Ventura Plaza Irvine, CA 92618

Suite 250 6405 Mira Mesa Blvd. San Diego, CA 92121

Suite 107 123 Hodencamp Rd. Thousand Oaks, CA 91360

FΔI Suite 310 27489 West Agoura Rd. Agoura Hills, CA 91301

Suite 200 25B Technology Irvine, CA 92718

Tel: (408) 734-8570

Fax: (408) 734-8875

Tel: (408) 522-9599

Fax: (408) 522-9590

Suite 220 5151 Shoreham Pl. San Diego, CA 92122

	Tel: Fax:		783-7877 783-7988
			434-1122 433-0822
	Tel: Fax:		812-6300 812-6333
			565-1760 565-1279
Corp.			434-0800 434-0935
IERN)			
vd.			563-2300 289-2355 777-7715
			727-4500 453-4610
			457-7545 457-9750
62			373-5600 496-7340
	Tel: Fax:	(714) (714)	727-0201 727-0210
	Tel: Fax:		638-9444 638-9454

Tel: (916) 782-7882

Fax: (916) 782-9388

Tel: (408) 434-0369

(: (805) 638-945

Tel: (818) 879-1234 Tel: (800) 274-0818 Fax: (818) 879-5200

#### Tel: (619) 623-2888 Fax: (619) 623-2891

**Bell Industries** 781 Highland Ave. Cheshire, CT 06410 FAI Westgate Office Center

700 West Johnson Ave.

Cheshire, CT 06410

Tel: (203) 250-0900 Fax: (203) 699-3892 Tel: (203) 250-1319

Fax: (203) 250-0081

COLORADO **Bell Industries** Suite 260 8787 Turnpike Dr. Westminster, CO 80030 **EBV Electronics** 

Tel: (805) 777-0045 Fax: (805) 777-0047

Tel: (714) 753-4778 Tel: (800) 967-0350 Fax: (714) 753-1183

Newark Electronics 34 Jerome Ave. Bloomfield, CT 06002	Tel: (860) 243-1731 Fax: (860) 242-3949
Nu Horizons Electronics Corp. Building I Corporate Place, Hwy. 128 107 Audubon Rd. Wakefield, MA 01880	Tel: (203) 265-0162 Fax: (203) 791-3801
FLORIDA	
Bell Industries Suite 400 650 South North Lake Blvd. Altamonte Springs, FL 32701	Tel: (407) 339-0078 Fax: (407) 339-0139
EBV Electronics Suite 130 600 South North Lake Blvd. Altamonte Springs, FL 32701	Tel: (407) 767-6974 Fax: (407) 767-9667
Suite 525 17757 U.S. Hwy. 19 North Clearwater, FL 33764	Tel: (813) 536-8800 Fax: (813) 536-8810
Suite 204 500 Fairway Dr. Deerfield Beach, FL 33442	Tel: (954) 418-0065 Fax: (954) 418-9080
FAI Suite 307 237 South Westmonte Dr. Altamonte Springs, FL 32701	Tel: (407) 685-7900 Tel: (800) 333-9719 Fax: (407) 865-5969
Suite 200 1400 East Newport Center Dr. Deerfield Beach, FL 33442	Tel: (954) 626-4043 Tel: (800) 305-8181 Fax: (954) 426-9477
Suite 108 2200 Tall Pines Dr. Largo, FL 34641	Tel: (813) 530-1665 Fax: (813) 538-9598
Future Electronics Suite 307 237 South Westmonte Dr. Altamonte Springs, FL 32714	Tel: (407) 865-7900 Tel: (800) 950-0168 Fax: (407) 865-7660
Suite 200 1400 East Newport Center Dr. Deerfield Beach, FL 33442	Tel: (954) 426-4043 Tel: (800) 305-2343 Fax: (954) 426-3939
Newark Electronics 3230 West Commercial Blvd. Ft. Lauderdale, FL 33309	Tel: (954) 486-1151 Fax: (954) 486-9929
4040 Woodcock Dr. Jacksonville, FL 32207	Tel: (904) 399-5041 Fax: (904) 399-5047
1080 Woodcock Rd. Orlando, FL 32803	Tel: (407) 896-8350 Fax: (407) 896-7348
5601 Mariner St. Tampa, FL 33609	Tel: (813) 287-1578 Fax: (813) 286-2572
Nu Horizons Electronics Corp. Suite 270 600 South North Lake Blvd. Altamonte Springs, FL 32701	Tel: (407) 831-8008 Fax: (407) 831-8862
3421 Northwest 55th St. Ft. Lauderdale, FL 33309	Tel: (954) 735-2555 Fax: (954) 735-2880
GEORGIA	
Bell Industries Suite 115 3000 Northwoods Pkwy. Norcross, GA 30071	Tel: (770) 446-9777 Fax: (770) 446-1186
EBV Electronics Suite 2700 6855 Jimmy Carter Blvd. Norcross, GA 30071	Tel: (770) 441-7878 Fax: (770) 441-1001
FAI Suite 130 3150 Holcomb Bridge Rd. Norcross, GA 30071	Tel: (404) 441-7676

### **Future Electronics** Suite 130 3150 Holcomb Bridge Rd. Norcross, GA 30071 Newark Electronics 520 Guthridge Ct. Tel: (770) 448-1300 Norcross, GA 30092 Nu Horizons Electronics Corp. Suite 155 100 Pinnacle Way Norcross, GA 30071 **IDAHO Future Electronics** 12301 West Explorer Dr. Boise, ID 83713 ILLINOIS Active Electronics 1776 West Golf Rd. Mount Prospect, IL 60056 Bell Industries 175 West Central Rd. Schaumburg, IL 60195 Fax: (847) 202-5849 **EBV Electronics** Suite 4610 3660 North Lake Shore Dr. Chicago, IL 60613 Fax: (773) 975-2110 FAI Suite 115 3100 West Higgins Rd. Hoffman Estates, IL 60195 **Future Electronics** Suite 200 3150 West Higgins Rd. Hoffman Estates, IL 60195 Newark Electronics 4801 North Ravenswood Chicago, IL 60640 Suite A320 1919 South Highland Ave. Lombard, IL 60148 110 South Alpine Rd. Rockford, IL 61108 1012 North St. Springfield, IL 62704 INDIANA Bell Industries 525 Airport North Office Park Fort Wayne, IN 46825 Suite B 5605 Fortune Cir. South Indianapolis, IN 46241 6982 Hillsdale Ct Indianapolis, IN 46250 FAI Suite 170 8425 Woodfield Crossing Indianapolis, IN 46240 **Future Electronics** Suite 170 8425 Woodfield Crossing Indianapolis, IN 46240 Newark Electronics 4410 Executive Blvd. Fort Wayne, IN 46808

50 East 91st St. Indianapolis, IN 46240

## Tel: (404) 441-7676 Fax: (404) 441-7580

Fax: (770) 448-7843 Tel: (770) 416-8666

```
Fax: (770) 416-9060
```

```
Tel: (208) 376-8080
```

Tel: (847) 640-7713 Tel: (847) 202-6400

Tel: (773) 883-5593

Tel: (847) 843-0034 Tel: (800) 283-1899 Fax: (847) 843-1163

Tel: (847) 882-1255 Tel: (800) 490-9290 Fax: (847) 490-9290

```
Tel: (773) 784-5100
Fax: (773) 907-5217
```

Tel: (630) 317-1000 Fax: (630) 424-8048 Tel: (815) 229-0225

Fax: (815) 229-2587 Tel: (217) 787-9972 Fax: (217) 787-7740

Tel: (219) 490-2104 Fax: (219) 490-2100

Tel: (317) 842-4244 Fax: (317) 570-1344 Tel: (317) 842-4244 Fax: (317) 570-1344

Tel: (317) 469-0441 Fax: (317) 469-0446

Tel: (317) 469-0447 Fax: (317) 469-0448 Tel: (219) 484-0766 Fax: (219) 482-4751

Tel: (317) 844-0047 Fax: (317) 844-0165

### IOWA

Newark Electronics 2550 Middle Rd Tel: (319) 359-3711 Bettendorf, IA 52722 Fax: (319) 359-5638

### KANSAS

**Bell Industries** Suite 313 6400 Glenwood Overland Park, KS 66202

FAI Suite 210 10977 Granada Ln. Overland Park, KS 66211

Future Electronics Suite 210 10977 Granada Ln. Overland Park, KS 66211

Newark Electronics 6811 West 63rd St. Overland Park, KS 66202

### KENTUCKY

MARYLAND

**Bell Industries** 

6460 Dobbin Rd

FAI

Suite 101

Columbia, MD 21045

Newark Electronics 1313 Lvndon Ln. Louisville, KY 40222

LOUISIANA

Newark Electronics 3525 North Causeway Blvd. Metairie, LA 70002

### Tel: (504) 838-9771 Fax: (504) 833-9461

Tel: (913) 236-8800

Fax: (913) 384-6825

Tel: (913) 338-4400

Fax: (913) 338-3412

Tel: (913) 498-1531

Fax: (913) 498-1786

Tel: (913) 677-0727

Fax: (913) 677-2725

Tel: (502) 423-0280

Fax: (502) 425-3741

Tel: (410) 730-6119 Fax: (410) 730-8940

**EBV Electronics** Suite 118 10010 Junction Dr. Tel: (301) 617-0200 Annapolis Junction, MD 20701 Fax: (301) 617-0202

6716 Alexander Bell Dr. Tel: (410) 312-0833 Columbia, MD 21046 Fax: (410) 312-0877

### **Future Electronics** International Tower, 2nd Floor 857 Elkridge Landing Rd. Linthicum Heights, MD 21090

Newark Electronics 7272 Park Circle Dr. Hanover, MD 21076

Nu Horizons Electronics Corp. Suite 160 8965 Guilford Rd.

Tel: (410) 995-6330 Tel: (301) 621-8244 Fax: (410) 995-6332

Tel: (781) 932-0050

Tel: (978) 623-3200

Fax: (978) 474-8902

Tel: (978) 657-5900

Fax: (978) 658-7989

Tel: (410) 314-1111

Fax: (410) 314-1110

Tel: (410) 712-6922

Fax: (410) 712-6932

### MASSACHUSETTS

Columbia, MD 21046

Active Electronics 11 Cummings Park Woburn, MA 01801

**Bell Industries** Suite G-01 100 Burtt Rd. Andover, MA 01810

187 Ballardvale St. Wilmington, MA 01887

**EBV Electronics** 131 Middlesex Turnpike Burlington, MA 01803

Tel: (617) 229-0047 Fax: (617) 229-0031

### 0

FAI 41 Main St. Bolton, MA 01740			779-3111 779-3199
Future Electronics 41 Main St.			779-3000
Bolton, MA 01740	Fax:	(978)	779-3050
Newark Electronics 59 Composite Way Lowell, MA 01851			551-4300 551-4329
65 Boston Post Rd. West Marlborough, MA 01752			229-2200 229-2222
Nu Horizons Electronics Corp. 19 Corporate Pl., Bldg. 1 107 Audubon Rd. Wakefield, MA 01880			246-4442 246-4462
MICHIGAN			
Future Electronics Suite 280 4595 Broadmoor, SE			698-6800
Grand Rapids, MI 49512 Suite 106	Fax:	(616)	698-6821
35200 Schoolcraft Rd. Livonia, MI 48150			261-5270 261-8175
Newark Electronics 900 East Paris Ave., SE Grand Rapids, MI 49546		· /	954-6700 954-6713
4600 Fashion Square Blvd. Saginaw, MI 48604			799-0480 799-7722
550 Stephenson Hwy. Troy, MI 48083			583-2899 583-1092
MINNESOTA			
Bell Industries Suite 232 9555 James Ave. South Bloomington, MN 55431			888-7747 888-7757
FAI Suite 198 10025 Valley View Rd. Eden Prairie, MN 55344			974-0909 944-2520
Future Electronics Suite 196			
10025 Valley View Rd. Eden Prairie, MN 55344			944-2200 944-2520
Newark Electronics 2021 Hennipin Ave. Minneapolis, MN 55413			331-6350 331-1504
Nu Horizons Electronics Corp. 10907 Valley View Rd. Eden Prairie, MN 55344			942-9030 942-9144
MISSISSIPPI			
<b>Newark Electronics</b> 795 Woodlands Pkwy. Ridgeland, MS 39157			956-3834 957-1240
MISSOURI			
FAI Suite 220 12125 Woodcrest Executive Dr. St. Louis, MO 63141			542-9922 542-9655
Future Electronics Suite 220 12125 Woodcrest Executive Dr. St. Louis, MO 63141			469-6805 469-7226
Newark Electronics 2258 Schuetz Rd. St. Louis, MO 63146	Tel: Fax:	(314) (314)	991-0400 991-6945

### NEBRASKA

Newark Electronics Tel: (402) 59 11128 John Galt Blvd. Omaha, NE 68137 Fax: (402) 59 NEW JERSEY Active Electronics Heritage Square 1871 Route 70 Cherryhill, NJ 08034 Tel: (609) 424 **Bell Industries** Suite F202-203 271 Route 46 West Tel: (973) 22 Fairfield, NJ 07004 Fax: (973) 22 Suite 110 158 Gaither Dr. Tel: (609) 43 Mt. Laurel, NJ 08054 Fax: (609) 43 **EBV Electronics** Suite A104 530 Fellowship Rd. Tel: (609) 23 Mt. Laurel, NJ 08054 Fax: (609) 23 FAI Suite 130 12 East Stow Rd. Tel: (609) 98 Marlton, NJ 08053 Fax: (609) 98 Future Electronics Suite 200 12 East Stow Rd. Tel: (609) 59 Marlton, NJ 08053 Fax: (609) 59 1259 Route 46 East Tel: (973) 29 Parsippany, NJ 07054 Fax: (973) 299 Newark Electronics Tel: (732) 93 197 Hwy. 18 South East Brunswick, NJ 08816 Fax: (732) 93 Nu Horizons Electronics Corp. Suite 200 18000 Horizon Way Tel: (609) 23 Mt. Laurel, NJ 08054 Fax: (609) 23 39 U.S. Route 46 Tel: (973) 88 Pine Brook, NJ 07058 Fax: (973) 88 NEW MEXICO **Newark Electronics** Tel: (505) 828 8205 Spain, NE Albuquerque, NM 87109 Fax: (505) 82 NEW YORK Active Electronics 3075 Veteran's Memorial Ronkonkoma, NY 11779 Tel: (516) 47 **Bell Industries** 77 Schmitt Blvd. Tel: (516) 42 Farmingdale, NY 11735 Fax: (516) 75 1 Corporate PI. Suite 200 1170 Pittsford Victor Rd. Tel: (716) 38 Pittsford, NY 14534 Fax: (716) 38 **EBV Electronics** 1373-40 Veterans Memorial Hwy. Tel: (516) 76 Hauppauge, NY 11788 Fax: (516) 76 FAI 801 Motor Pkwy. Tel: (516) 34 Hauppauge, NY 11788 Fax: (516) 34 300 Linden Oaks Tel: (716) 38 Rochester, NY 14625 Suite 150 200 Salina Meadows Pkwy. Tel: (315) 45 Syracuse, NY 13212 Fax: (315) 45

				_
92-2423	Future Electronics 801 Motor Pkwy. Hauppauge, NY 11788		234-4000 234-6183	
92-2423 92-0508	300 Linden Oaks Rochester, NY 14625		387-9550 387-9563	
	Suite 200 200 Salina Meadows Pkwy. Syracuse, NY 13212		451-2371 451-7258	
24-7070	Newark Electronics 3 Marcus Blvd. Albany, NY 12205	· ·	489-1963 489-1989	
27-6060 27-2626	75 Orville Dr. Bohemia, NY 11716		567-4200 567-4235	
39-8860	7449 Morgan Rd. Liverpool, NY 13090		457-4873 457-6096	
39-9009	1151 Pittsford-Victor Rd. Pittsford, NY 14534		381-4244 381-2632	
35-7474 35-4992	15 Myers Corners Rd. Wappingers Falls, NY 12590	· ·	298-2810 298-2823	
50 <del>1</del> 552	5500 Main St. Williamsville, NY 14221	· ·	631-2311 631-4049	
38-1500 38-9231	Nu Horizons Electronics Corp. 70 Maxess Rd. Melville, NY 11747		396-5000 396-5050	
96-4080 96-4266	333 Metro Park Rochester, NY 14623		292-0777 292-0750	
99-0400	NORTH CAROLINA			
99-1377	Bell Industries Suite 800			
37-6600 37-6667	3100 Smoketree Ct. Raleigh, NC 27604		874-0011 874-0013	
31-0900 31-9510	EBV Electronics Suite 575 8000 Regency Pkwy. Cary, NC 27511		468-3580 462-0891	
82-8300 82-8398	Future Electronics Suite 108 8401 University Executive Park Charlotte, NC 28262		547-1107 547-9650	
8) 1878 28-9761	Suite 314 Smith Towers Charlotte Motor Speedway P.O. Box 600 Concord, NC 28026	· ·	455-9030 455-9173	
	1 North Commerce Center 5225 Capital Blvd. Raleigh, NC 27604		876-0088 790-9022	
71-5400 20-9800	Newark Electronics 5501 Executive Center Dr. Charlotte, NC 28212		535-5650 537-3914	
52-9870	1701 Pinecroft Rd. Greensboro, NC 27407		292-7240 292-9575	
81-9700 81-9495	Nu Horizons Electronics Corp. Suite 125 2920 Highwood Blvd. Raleigh, NC 27604		954-0500 954-0545	
61-1500 61-1510	ОНІО			
48-3700 48-3793	Bell Industries 8149 Washington Church Road Dayton, OH 45458		428-7300 428-7359	
87-9600	6557-A Cochran Rd. Solon, OH 44139	· ·	542-3700 542-3710	
51-4405 51-2621	Bell Industries (Military) 8149 Washington Church Road Dayton, OH 45458		428-7330 428-7358	

FAI Suite 203 1430 Oak Ct.	Tel: (513) 427-6090 Fax: (216) 449-8987
Beavercreek, OH 45430 Future Electronics	Fax. (210) 449-0907
Suite 203 1430 Oak Ct. Beavercreek, OH 45430	Tel (513) 426-0090 Fax: (513) 426-8490
6009 East Landerhaven Dr. Mayfield Heights, OH 44124	Tel: (440) 449-6996 Fax: (440) 449-8987
Newark Electronics 498 Circle Freeway Dr. Cincinnati, OH 45246	Tel: (513) 942-8700 Fax: (513) 942-8770
4614 Prospect Ave. Cleveland, OH 44103	Tel: (216) 391-9300 Fax: (216) 391-2811
5025 Arlington Centre Blvd. Columbus, OH 43220	Tel: (614) 326-0352 Fax: (614) 326-0231
3033 Kettering Blvd. Dayton, OH 45439	Tel: (937) 294-8980 Fax: (937) 294-2517
5660 Southwyck Blvd. Toledo, OH 43614	Tel: (419) 866-0404 Fax: (419) 866-9204
Nu Horizons Electronics Cor 2208 Enterprise E. Pkwy. Twinsburg, OH 44087	<b>p.</b> Tel: (216) 963-9933 Fax: (216) 963-9944
OKLAHOMA	
Newark Electronics 3524 Northwest 56th St. Oklahoma City, OK 73112	Tel: (405) 943-3700 Fax: (405) 943-6403
OREGON	
Bell Industries Suite 100 8705 Southwest Nimbus Ave. Beaverton, OR 97008	Tel: (503) 644-3444 Fax: (503) 520-1948
EBV Electronics Suite 360 8196 Southwest Hall Blvd. Beaverton, OR 97008	Tel: (503) 574-2255 Fax: (503) 574-2266
Future Electronics Suite 800	
7204 Southwest Durham Rd. Portland, OR 97224	Tel: (503) 645-9454 Fax: (503) 645-1559
Newark Electronics 4850 Southwest Scholls Ferry Portland, OR 97225	Rd. Tel: (503) 297-1984 Fax: (503) 297-1925
PENNSYLVANIA	
Bell Industries Suite 110	
158 Gaither Dr. Mt. Laurel, NJ 08054	Tel: (215) 557-6450 Fax: (609) 231-9510
EBV Electronics Suite A104 520 Fellowship Rd. Mt. Laurel, NJ 08054	Tel: (609) 235-7474 Fax: (609) 235-4992
Future Electronics Suite 200 12 East Stow Rd. Marlton, NJ 08053	Tel: (609) 596-4080 Fax: (609) 596-4266
Newark Electronics 1503 North Cedar Crest Blvd. Allentown, PA 18104	Phone: (610) 434-7171 Fax: (610) 432-3390
501 Office Center Dr. Fort Washington, PA 19034	Tel: (215) 654-1434 Fax: (215) 654-1460
100 Hightower Blvd. Pittsburgh, PA 15205	Tel: (412) 788-4790 Fax: (412) 788-1566
Nu Horizons Electronics Cor	р.
Suite 200 18000 Horizon Way	Tel: (215) 557-6450

Mt. Laurel, NJ 08054

~	~	~		•••	•••	-	_	•

Fax: (609) 231-9510

SOUTH CAROLINA			
Newark Electronics 150 Executive Center Dr. Greenville, SC 29615			288-9610 297-3558
TENNESSEE			
Newark Electronics 5401-A Kingston Pike Knoxville, TN 37919			588-6493 588-6041
2600 Nonconnah Blvd. Memphis, TN 38132			396-7970 396-7955
TEXAS			
Bell Industries			
Suite 103 11824 Jollyville Rd. Austin, TX 78759			331-9961 331-1070
Suite 170 14110 North Dallas Pkwy. Dallas, TX 75240			458-0047 404-0267
Suite 310 12000 Richmond Ave. Houston, TX 77082			870-8101 870-8122
EBV Electronics Suite 215			
11500 Metric Blvd. Austin, TX 78758			491-9340 491-9345
Suite 320 1778 Plano Rd. Richardson, TX 75081			783-8322 783-8774
FAI Northpoint Center Bldg. II			
Suite 320 6850 Austin Center Blvd. Austin, TX 78731	Tel: Fax:	(512) (512)	346-6426 346-6781
Suite 126 800 East Campbell Richardson, TX 75081	Tel:	(800)	231-7195 272-0694 231-2508
Suite 137E 6800 Park Ten Blvd. San Antonio, TX 78213			738-3330 738-0511
Future Electronics Northpoint Center Bldg. II			
Suite 320 6850 Austin Center Blvd. Austin, TX 78731			502-0991 502-0740
Suite 970 10333 Richmond Ave. Houston, TX 77042	Tel:	(203)	952-7088 250-0083 952-7098
Suite 130			437-2437
800 East Campbell Richardson, TX 75081	Tel:	(203)	250-0083 669-2347
Newark Electronics 3737 Executive Center Dr. Austin, TX 78731			338-0287 345-2702
12880 Hillcrest Rd. Dallas, TX 75230			458-2528 458-2530
Suite 292 7500 Viscount El Paso, TX 79925			772-6367 772-3192
8203 Willow PI. South Houston, TX 77070			894-9334 894-7919
Nu Horizons Electronics Corp. Suite 100 2404 Rutland Dr.	Tel:		873-9300 47-NUHO
Austin, TX 78758			873-9800
Suite 200 1313 Valwood Pkwy. Carrollton, TX 75006	Tel:	(800)	488-2255 200-1586 488-2265

### UTAH

Bell Industries Suite 110 310 East 4500 South Murray, UT 84107 **EBV Electronics** Suite 131 825 East 4800 South Murray, UT 84107 FAI Suite 301

Tel: (801) 261-2999

Fax: (801) 261-0880

Tel: (801) 261-1088

Fax: (801) 261-1442

Tel: (801) 467-9696

Fax: (801) 467-9755

Tel: (801) 467-4448

Fax: (801) 467-3604

Tel: (801) 261-5660

Fax: (801) 261-5675

Tel: (804) 984-5022

Fax: (804) 984-5422

Tel: (703) 707-9010

Fax: (703) 707-9203

Tel: (804) 282-5671

Fax: (804) 282-3109

Tel: (206) 881-8191

Tel: (425) 486-2124

Fax: (425) 487-1927

Tel: (206) 485-6616

Fax: (206) 483-6109

Tel: (206) 489-3400

Fax: (206) 489-3411

Tel: (425) 814-6230

Fax: (425) 814-9190

Tel: (509) 327-1935

Fax: (509) 328-8658

Tel: (414) 793-9778

Fax: (414) 792-9779

Tel: (414) 879-0244

Fax: (414) 879-0250

3450 South Highland Dr. Salt Lake City, UT 84106

**Future Electronics** Suite 301 3450 South Highland Dr. Salt Lake City, UT 84106

Newark Electronics 4424 South 700 East Salt Lake City, UT 84107

### VIRGINIA

FAI Suite 202 660 Hunters PI. Charlottesville, VA 22911

Newark Electronics 131 Elden St. Herndon, VA 22070

1504 Santa Rosa Rd. Richmond, VA 23229

#### WASHINGTON

Active Electronics 13107 Northup Way 20th St., NE Bellevue WA 98005

**Bell Industries** Suite 102 19119 North Creek Pkwy. Bothell, WA 98011

FAI North Creek Corporate Center Suite 118 19102 North Creek Pkwy Bothell, WA 98011

Future Electronics North Creek Corporate Center Suite 118 19102 North Creek Pkwy. Bothell, WA 98011

Newark Electronics 12015 115th Ave., NE Kirkland, WA 98034

West 222 Mission Ave. Spokane, WA 99201

### WISCONSIN

**Bell Industries** W 226 N 900 Eastmound Dr. Tel: (414) 547-8879 Waukesha, WI 53186 Fax: (414) 547-6547 FΔI

Suite 170 250 North Patrick Blvd. Brookfield, WI 53045

**Future Electronics** Suite 170 250 North Patrick Blvd. Brookfield, WI 53045

**Newark Electronics** 6400 Enterprise Ln. Madison, WI 53719

Wauwatosa, WI 53226

2525 North Mavfair Rd.

Tel: (608) 278-0177 Fax: (608) 278-0166 Tel: (414) 453-9100 Fax: (414) 453-2238

Section 5: Data Sheets

### Designing With LDO Regulators



## **International Sales Representatives and Distributors**

Micrel Semiconductor sales indicated by [Micrel]. Synergy Semiconductor sales indicated by [Synergy].

### NORTH AMERICA-DIE DISTRIBUTION ONLY

Chip Supply, Inc. [Micrel] 7725 Orange Blossom Trail Tel: +1 (407) 298-7100

Fax: +1 (407) 290-0164 Orlando El USA 32810-2696

### EUROPE-DIE DISTRIBUTION ONLY

336627
) 260380

### Eltek Semiconductor, Ltd. [Micrel]

Nelson Road Industrial Est	tate	
Dartmouth	Tel:	+ 44 (1803) 834455
Devon TQ6 9LA	Fax:	+ 44 (1803) 833011
United Kingdom		

### INTERNATIONAL—PACKAGED DEVICES

### AUSTRALIA

Future Electronics <sup>[Synergy]</sup> 2nd Floor 1013 Whitehorse Rd.	Tel: (613) 98997944
Box Hill, Victoria 3128	Fax: (613) 98909632
KC Electronics [Synergy] (Rep.)	
KC Electronics <sup>[Synergy]</sup> (Rep.) 152 Highbury Road	Tel: (613) 92453253
,	Tel: (613) 92453253 Fax: (613) 92453288

### BELGIUM

	<sup>[Synergy]</sup> ( <i>Stocking Rep.)</i> [el: + 32 (3) 458 30 33 ax: + 32 (3) 458 31 26
	el: + 31 (20) 504 14 35 x: + 31 (20) 642 39 48
BRAZIL	
	<b>ar Ltda.</b> <sup>[Micrel]</sup> el: + 55 (11) 231-0277 x: + 55 (11) 255-0511
CANADA—ALBERTA	
Microwe Electronics Corporati	on <sup>[Micrel-Synergy]</sup> (Rep.)
2333 18th Avenue NE Calgary, AB T2E 8T6	Tel: (403) 250-7577 Fax: (403) 250-7867
Active Electronics <sup>[Micrel-Synergy]</sup> Unit 1	
2015 32nd Ave., NE Calgary, AB T2E 6Z3	Tel: (403) 291-5626 Fax: (403) 291-5444
Future Active Industrial [Micrel-Syr Unit 1	nergy]

Unit 1 2015 32nd Ave., NE Calgary, AB_T2E 6Z3	Tel: (403) 291-5333 Fax: (403) 291-5444
6029 103rd St. Edmonton, AB T6H 2H3	Tel: (403) 438-5888 Fax: (403) 436-1874
Future Electronics <sup>[Micrel-Synergy]</sup> 3833 - 29th St., NE Calgary, AB T1Y 6B5	Tel: (403) 250-5550 Fax: (403) 291-7054

6029 103rd St. Edmonton, AB T6H 2H3 CANADA-BRITISH COLUMBIA Microwe Electronics Corporation [Micrel-Synergy] (Rep.) 8394-208th St. Langley, BC V2Y 2B4

#### Bell Industries [Micrel] Suite B201 4185 Still Creek Dr. Tel: (604) 291-0044 Burnaby, BC V5C 6G9 Fax: (604) 291-9939 Future Active Industrial [Micrel-Synergy] Tel: (604) 654-1050 200-3689 East 1st. Avenue Vancouver, BC V5M 1C2 Fax: (604) 294-3170 Future Electronics [Micrel-Synergy]

Tel: (403) 438-2858

Fax: (403) 434-0812

Tel: (604) 882-4667

Fax: (604) 882-4668

1695 Boundary Road Vancouver, BC V5K 4X7 Tel: (604) 294-1166

### CANADA—MANITOBA

Future Active Industrial [Micrel-Syn	nergy]	
504-1780 Wellington Ave.	Tel:	(204) 786-3075
Winnipeg, MB R3H 1B2	Fax:	(204) 783-8133
Future Electronics [Micrel-Synergy]		
Future Electronics [Micrel-Synergy] 504-1780 Wellington Ave.	Tel:	(204) 944-1446

### CANADA-ONTARIO

Kaltron Technologies Ltd. Micrel P.O. Box 1214 261 Williams St. Almonte, ON K0A 1A0	<sup>-Synergy]</sup> ( <i>Rep.)</i> Tel: (613) 256-5278 Fax: (613) 256-4757
147 Lloydalex Cres. RR#3 Carp., ON K0A 1L0	Tel: (613) 860-0627 Fax: (905) 831-3475
200-5925 Airport Rd. Mississauga, ON L4V 1W1	Tel: (905) 405-6276 Fax: (905) 405-6274
Active Electronics <sup>[Micrei-Synergy]</sup> Unit 2 1350 Matheson Blvd. Mississauga, ON L4W 4M1	Tel: (905) 238-8825 Fax: (905) 238-2817
1023 Merivale Road Ottawa, ON K1Z 6A6	Tel: (613) 728-7900 Fax: (613) 728-3586
Bell Industries <sup>[Micrel]</sup> 2783 Thamesgate Dr. Mississauga, ON L4T 1G5	Tel: (905) 678-0958 Fax: (905) 678-1213
Future Active Industrial [Micrel-Syr Suite 205/210	nergy]
5935 Airport Rd. Mississauga, ON L4V 1W5	Tel: (613) 820-8244 Fax: (613) 820-8046
Future Electronics [Micrel-Synergy] Suite 210	
1101 Price of Wales Dr. Ottawa, ON K2C 3W7	Tel: (613) 820-8313 Fax: (613) 820-3271
Newark Electronics <sup>[Micrel]</sup> 569 Consortium Ct. London, ON N6E 2S8	Tel: (519) 685-4280 Fax: (519) 685-7104
6200 Dixie Rd. Mississauga, ON L5T 2E1	Tel: (905) 670-2888 Fax: (905) 670-1019

### CANADA-QUEBEC

Kaltron Technologies Ltd. 224 Forest Rd. Beaconsfield, PQ H9W 2N2			630-7238
Active Electronics [Micrel-Syner	rgy]		
Suite 190 1990 Boul. Charest Ouest Ste. Foy, PQ G1N 4K8			682-5775 682-6282
Bell Industries [Micrel]			
Suite 209 6600 Trans Canada Hwy. Pointe Claire, PQ H9R 4S2			426-5900 526-5836
Future Active Industrial [Mic	rel-Synergy]		
5651 Ferrier St. Montreal, PQ H4P 1N1			731-7444 731-0129
6080 Metropolitan Blvd. Montreal, PQ H1S 1A9			256-7538 256-4890
Future Electronics [Micrel-Syne	rgy]		
Suite 100 1000 Ave. St. Jean Baptiste Quebec, PQ G2E 5G5			877-6666 877-6671
237 Hymus Blvd.	То	. (514)	694-7710
Pointe Claire, PQ H9R 5C7			695-3707
Newark Electronics <sup>[Micrei]</sup> 4480 Cote De Liesse Mt. Royal, PQ H4N 2R1			738-4488 738-4606
CHINA			
Cytech Technology, Ltd. [S	vnergy] (Po	- )	
Room 302 New High Tech Building No. 19 Zhong Guan Cun Ro Haidian District	ad Tel: +	86 (10)	62546450 62546451
Room 306 Tian Ge Wu Cheng Building Mo Zi Giao Yi Huan Road South Sectior Chengdu 610041	12		) 5532883 ext. 3306 ) 5548808
Room 3-5			
Ke Chuang Building 50 Yu Zhou Road			
Goa Xin Ji Shu Kaifa Qu			
Shi Qiao Pu Chongqing 400039 Te			68608938 68619097
Room 03, 19/F			
Donghuan Tower No. 474 Donghuan Road Guangzhou 510075			87627220 87627227
Room 205 No. 29D Yudao Street Nanjing 210016 T			) 4890188 ) 4892089
Room 804 1583 Zhong Shan Road We Shanghai 200233 Te			64388082 64644953
Unit K, 13/F			
Hangdu Bldg. No. 1006 Huafu Road			53780519 53780516
Galaxy Far East Corp. [Micrel		. ,	
Room 0514			

+ country code (city code) telephone number

Tel: + 86 (21) 64956485

Fax: +86 (21) 64852237

New Caohejing Tower

509 Caobao Road Shanghi

### Lestina International Ltd. [Micrel]

Room 302 New High Tech Building No. 19 Zhong Guan Cun Road Haidian District Tel: + 86 (10) 62546450 Beijing 100080 Tel/Fax: + 86 (10) 62546451 Room 306

Tian Ge Wu Cheng Building Mo Zi Giao Tel: + 86 (28) 5532883 Yi Huan Road South Section 2 ext. 3306 Chengdu 610041 Tel/Fax: + 86 (28) 5548808 Room 3-3 Ke Chuang Building 50 Yu Zhou Road Goa Xin Ji Shu Kaifa Qu Shi Qiao Pu Tel: + 86 (23) 68619099 Chongqing 400039 Tel/Fax: + 86 (23) 68608938 - 02 40/F 00 (00) 07007000

Room 03, 19/F	Tel: + 86 (20) 87627232
Donghuan Tower	Tel: + 86 (20) 87627220
No. 474 Donghuan Road	Tel: + 86 (20) 87627222
Guangzhou 510075	Fax: + 86 (20) 87627227
B	
Room 205	

No. 29D Yudao Street	Tel: + 86 (25) 4890188
Nanjing 210016	Tel/Fax: + 86 (25) 4892089

Room 804 1583 Zhong Shan Road West Tel: + 86 (21) 64388082 Shanghai 200233 Tel/Fax: + 86 (21) 64644953

Unit K, 13/F Hangdu Building No. 1006 Huafu R Shenzhen 518041

oad	Tel: + 86 (755) 3790519
	Tel/Fax: + 86 (755) 3790516

### DENMARK

Future Electronics a/s Micrel-Syn Lille Ostergade 5.3 7500 Holstebro	Tel:	+ 45 96 10 09 75 + 45 96 10 09 62
Micronor a/s <sup>[Synergy]</sup> (Stocking Rep.)		
(blocking it	ep.)	
Trovets 1		+ 45 86 81 65 22

#### **FINLAND**

### Integrated Electronics Oy Ab [Micrel]

Laurinmäenkuja 3 A	Tel: + 358 (9) 2535 4400
00440 Helsinki	Fax: + 358 (9) 2535 4450

P.O. Box 31 00441 Helsinki

Memec Finland Oy [Synergy] (	Stocking Rep.)
Kauppakaare 1	Tel: + 358 (9) 836 2600
00700 Helsinki	Fax: + 358 (9) 836 26027
FRANCE	
Future Electronics [Micrel-Syne	rgy]
Parc Technopolis	
Bat. theta 2 LP854 Les Ulis	
3, avenue du Canada	Tel: + 33 (1) 69.82.11.11
91940 Courtaboeuf cedex	Fax: + 33 (1) 69.82.11.00
LSX S.A.R.L. [Micrel] (Rep.)	5 Tal 00 (4) 40 07 00 00
30, rue du Morvan SILIC 525	$J = 101. \pm 33(1) 40.07.03.30$

94633 Rungis cedex	Fax: + 33 (1) 45.60.07.84
	ng Rep.) Tel: + 33 (2) 99.83.04.40 Fax: + 33 (2) 99.83.04.44
	Rep.) Tel: + 33 (1) 46.87.22.00 Fax: + 33 (1) 46.87.80.49

### Sonepar Electronique [Micrel]

6-8, rue Ambroise Croizat	Tel: + 33 (1) 64.47.29.29
91127 Palaiseau cedex	Fax: + 33 (1) 64.47.00.84

### GERMANY

ActiveComp GmbH [Micrel	l (Rep.)	
Schubertstraße 35	Tel: + 49 (70) 43 93 29 10	
75438 Knittlingen	Fax: + 49 (70) 4 33 34 92	
dacom Electronic Vertriebs GmbH [Micrei]		

Tel: + 49 (89) 9 96 54 90 Freisinger Straße 13 85737 Ismaning Fax: + 49 (89) 96 49 89

Future Electronics Deutschland GmbH [Micrel-Synergy] München Straße 18 Tel: + 49 (89) 95 72 70 85774 Unterföhring Fax: + 49 (89) 95 72 71 73

Retronic GmbH [Synergy] (St	ocking	Rep.)				
Willhoop 1	Tel:	+ 49 (	(89)	40 5	3 97	44
22453 Hamburg	Fax:	+ 49 (	(89)	40 5	3 97	44

### HONG KONG

(Rep.)		
Tel:	+ 852	27350325
Fax:	+ 852	27307538
	Tel:	<i>Rep.)</i> Tel: + 852 Fax: + 852

### Cytech Technology [Synergy] (Rep.)

Room 1803, 18th Floor	
Hom Kwok Jordan Center	
7 Hillwood Road	
Tsimshatsui	Tel: + 852 23782212
Kowloon	Fax: + 852 23757700

### Lestina International Ltd. [Micrel]

14th Floor, Park Tower	
15 Austin Road	Tel: + 852 27351736
Tsimshatsui	Fax: + 852 27305260
Kowloon	Fax: +852 27307538

### INDIA

Hynetic International [Synergy] (Rep.)					
No. 50, 2nd Cross					
Gavipuram Extension	Tel:	+ 91	(80)	620852	
Bangalore - 560019	Fax:	+ 91	(80)	624073	į.
Samura Electronics Pvt. Ltd. [Micrel]					

### Room No 507 W

10011110.007 11						
Navketan Commercial	Complex	Tel:	+ 91	(40)	78065	541
62, S. D. Road	1	el:	+ 91	(40)	78065	542
Secunderabad - 50000	3 F	ax:	+ 91	(40)	78065	542

### IRELAND

Future Electronics [Micrel-Synergy] Post Office Lane Abbey Street Ennis, County Clare	Tel: + 353 (65) 41330 Fax: + 353 (65) 40654
Solid State Supplies Ltd. Micre	<sup>I]</sup> <i>(Stocking Rep.)</i>
2 Wesley Place	Tel: + 353 (67) 34455

Fax: + 353 (67) 34329

ISRAEL

County Tipperary

Nenagh

El-Gev Electronics, Ltd. [Micrel-Synergy]		
11, Ha-avoda Street	Tel: + 972 (3) 9027202	
48017 Rosh Ha-aydin	Fax: + 972 (3) 9027203	
POB 248		

### 48101 Rosh Ha-aydin

### ITALY

20139 Milan

Aertronica S.r.I. <sup>[Synergy]</sup> (St Viale Cesare Battisti, 38 20052 Manza (MI)	ocking Rep.) Tel: + 39 (39) 2302240 Fax: + 39 (39) 2302226
Carlo Gavazzi Cefra S.p.A	. [Micrel]
Via G. De Castro, 4	Tel: + 39 (02) 48012355
20144 Milano	Fax: + 39 (02) 48008167
Future Electronics S.r.l. <sup>™</sup> Via Fosse Ardeantine 4 20092 Cinisello Balsamo (N	
Pinnacle Special Technol	ogies, S.r.I. [Micrel]
(Stocking Rep.)	
Via Brembo 21	Tel: + 39 (02) 56810413

### Tel: + 39 (02) 56810413 Fax: + 39 (02) 56810349

## JAPAN

Suite 121

Tempe, AZ

USA 85282

4545 South Wendler Dr.

JAPAN	
Hakuto Co. Ltd. <sup>[Synergy]</sup> ( <i>Rep.</i> ) Nagoya-Seni Bldg. 9-27, Nishiki, 2-chome Naka-ku Nagoya Aichi 460	Tel: + 81 (52) 204-8910 Fax: + 81 (52) 204-8935
292-4, Asouda-machi Matsuyama Ehime 790	Tel: + 81 (89) 931-8910 Fax: + 81 (89) 945-6218
Felix Iwai Bldg. 2-3, Hakataekiminami, 3-chor Hakata-ku Fukoka 812	ne Tel: + 81 (92) 431-5330 Fax: + 81 (89) 431-5265
3-18, Miyanomae, 2-chome, la Hoygo 664	tami Tel: + 81 (72) 784-8910 Fax: + 81 (72) 784-7860
56, Takehanatakenokaido-cho Yamashina-ku Kyoto 607	o Tel: + 81 (75) 593-8910 Fax: + 81 (75) 593-8990
Kamisugikokune Bldg. 4-10, Kamisugi, 1-chome, Aoba-ku Sendai, Miyagi 980	Tel: + 81 (22) 224-8910 Fax: + 81 (22) 224-0645
Micro Summit K.K. <sup>[Micrel]</sup> (Sta Premier K1 Bldg. 1 Kanda Mikura-cho Chiyoda-ku Tokyo 101	cking Rep.) Tel: + 81 (3) 3258-5531 Fax: + 81 (3) 3258-0433
Nippon Imex Corporation M No. 6 Sanjo Bldg., 5F 1-46-9 Matsubara Setagaya-ku Tokyo 156	rrei] Tel: + 81 (3) 3321-8000 Fax: + 81 (3) 3325-0021
KOREA	
GenTech Corporation <sup>[Micrel]</sup> 301, Daewon B/D 67-5, Yangjae-dong Seocho-ku Seoul	(Stocking Rep.) Tel: + 82 (2) 3463-0040 Fax: + 82 (2) 3463-4935
UTO International <sup>[Synergy]</sup> ( <i>Re</i> Suite 801, Union Bldg. 837-11, Yeoksam-dong Kangnam-ku Seoul	p.) Tel: + 82 (2) 566-3745 Fax: + 82 (2) 508-3250
MALAYSIA	
JAG Components Sdn Bhd Room 3B 1st Floor Mutiara I&P 47 Green Hall	[Micrel] Tel: + 604-2634932
10200 Penang	Fax: + 604-2633376
MEXICO	
Harwood Associates Mexico Anguila 3627 Col. Loma Bonita 44590 Zapopan, Jalisco	o <sup>[Micrel]</sup> <i>(Rep.)</i> Tel: + 52 (3) 634-99-27 Fax: + 52 (3) 634-62-56
EBV Electronics <sup>[Synergy]</sup> Prol. Americas 1612 6to Piso Colonia Country Cluby 44610 Guadalajara, Jalisco	Tel: + 52 (3) 678-91-20 Fax: + 52 (3) 678-92-43
Future Electronics Mexico S 5º Piso, Suite 2 Chimalhuacán 3569 Ciudad del Sol 45050 Zapopan, Jalisco	<b>5.A. de C.V.</b> <sup>[Micrei]</sup> Tel: + 52 (3) 122-00-43 Fax: + 52 (3) 122-10-66
Mexican States of Sonora	a and Chihuahua
S & S Technologies [Micrel] Suite 121	

+ country code (city code) telephone number

Tel: +1 (602) 438-7424 Fax: +1 (602) 414-1125

### NETHERLANDS

Alcom Electronics [Synergy] (S	tocking	g Rep.)
Rivium 1 e straat 52	Tel:	+ 31 (10) 288 2500
2909LE Cappelle aan den ljs	ell	
	Fax:	+ 31 (10) 288 2525

### Nijkerk Elektronika B.V. [Micrel]

Drentestraat 7	Tel: + 31 (20) 504 14 35
1083 HK Amsterdam	Fax: + 31 (20) 642 39 48

### NEW ZEALAND

Avnet Pacific Pty. [Micrel]	
274 Church Street	Tel: + 64 (9) 636 7801
Penrose, Auckland	Fax: + 64 (9) 634 4900

P.O. Box 92821 Penrose, Auckland

### NORWAY

ACTE NC Norway AS [Micrel]	
Vestvollveien 10	Tel: + 47 63 89 89 89
2020 Skedsmokorset	Fax: + 47 63 87 59 00

Postboks 84 2020 Skedsmokorset

### Bit Elektronikk AS <sup>[Synergy]</sup> (Stocking Rep.) Smedsvingen 4 Tel: + 47 66 77 65 00

Silleusvillgen 4	Tel. + 47 00 77 05 00
1364 Hvaldstad	Fax: + 47 66 77 65 01

### NORTHERN IRELAND

SEI Bloomer Electronics Ltd	[Synergy] (Stocking Rep.)
9-10 Carn Industrial Estate	Tel: + 44 1762 339818
Craigavon	Fax: + 44 1762 330650
County Armagh BT63 5RH	

### PHILIPPINES

Crystal Semiconductors, Inc Crystal Semiconductors Bldg. Nos. 64-66 Kanlaon St.	[Micrel]	I
Highway Hills Mandaluyong City 1500		+ 63 (2) 531-2336 + 63 (2) 533-4990

### PORTUGAL

Comdist Lda. [Synergy] (Stocking Rep.)		
Edificio turia		
Rua do Entreposto Industrial, 3-2		
Andar Sala-E, Qta Grande	Tel: + 351 (1) 472 5190	
2720, Alfrgaide Lisbon	Fax: + 351 (1) 472 5199	

### SINGAPORE

JAG Components (Pte.) Ltd.	[Micrel]
Ruby Industrial Complex	
Genting Block	
80 Genting Lane, #11-06A	Tel: + 65 749 56 63
Singapore 349565	Fax: + 65 749 56 62

Microtronics Associates [Synergy] (Stocking Rep.)

8, Lorong Bakar Batu 03-01 Kolam Ayer Industrial Park Singapore 348743 Fax: + 65 748 18 35 Fax: + 65 743 30 65

### SOUTH AFRICA

Integrated Circuit Technologies [Micrel]		
(Stocking Rep.)		
66 Third St.	Tel: + 27 (11) 444 3386	
Marlboro, Sandton	Fax: + 27 (11) 444 3389	
Johannesburg		

MB Silicon Systems (Pty.) Ltd. [Micrel]		
P.O. Box 2292	Tel: + 27 (11) 728 4757	
Houghton 2041	Fax: + 27 (11) 728 4979	
Johannesburg		

### SPAIN

Comelta Distribution S.L. <sup>[Syr</sup> Ctra de Fuencarral Km 15,700 Edifico Europa I a pl-1 28108 Alcobendas, Madrid	(	
Avgnda Parc Technologic 4 08200, Cerdanyola del valles Barcelona	Tel: + 34 (3) 582 1991 Fax: + 34 (3) 582 1992	
Unitronics Componentes, S.A. [Micrel]		
Pza. Espana, 18. PL9	Tel: + 34 91 304 3043	
28008 Madrid	Fax: + 34 91 327 2472	
SWEDEN		

Memec Scandinavia AB [Syner	<sup>gy]</sup> (Sto	cking Rep.)
Sehistedtsgaten 6	Tel:	+ 46 (8) 459 7900
11528 Stockholm	Fax:	+ 46 (8) 459 7999
Pelcon Electronics AB [Micrel]		

46 (8) 795 98 70
46 (8) 760 76 85
46 (8) 621 03 35
46 (8) 621 02 99

### SWITZERLAND

Computer Controls AG	[Synergy] (Stocking Rep.)
P.O. Box C14	Tel: + 41 (1) 308 66 66
8057 Zurich	Fax: + 41 (1) 308 66 55

Electronitel SA [Micrel] (Stoc	cking Rep.)
Ch. du Grand-Clos 1	
BP 142	Tel: + 41 (26) 401 00 60

B.P. 142	Tel: + 41 (26) 401 00 60
1752 Villars-sur-Glâne 1	Fax: + 41 (26) 401 00 70

### TAIWAN, R.O.C.

Galaxy Far East Corp. <sup>[Micr</sup> 1F, No. 15 Alley 20 Lane.54	44
Sec. 1, Kuang Fu Road Hsinchu	Tel: + 886 (3) 578-6766 Fax: + 886 (3) 577-4795
7F-A3, 29 Hai-Pien Road Kaohsiung	Tel: + 886 (7) 338-0559 Fax: + 886 (7) 338-1343
8F-6, No. 390, Section 1 Fu Hsing South Road Taipei	Tel: + 886 (2) 2705-7266 Fax: + 886 (2) 2708-7901
Prohubs International Con 20F-4, 79, Section 1	
Hsin Tai Wu Road	Tel: + 886 (2) 2698-9801

### THAILAND

Hs-Chih, Taipei Hsien

JAG Components Thailand Co. Ltd. [Micrel]									
48/157 Moo 1									
Ramkhamhaeng Road									
Sapansoong	Tel: + 662-7294245/6								
Buengkum BangKok 10240	Fax: + 662-7293030								

Fax: + 886 (2) 2698-9802

### UNITED KINGDOM

Berksh

Focus Electronics Distribu	tion Ltd. <sup>[Synergy]</sup>
(Stocking Rep.)	
Suite 1	
Sovereign House	
82 West Street	Tel: + 44 1702 542301
Rochford Essex SS4 1AS	Fax: + 44 1702 542302
Future Electronics Ltd. [Micro	al-Synergy]

Future House	
Poyle Road	
Colnbrook	Tel: + 44 (1753)

Juau	
ook	Tel: + 44 (1753) 763000
ire SL3 0EZ	Fax: + 44 (1753) 689100

Silicon Concepts Ltd. [Micrel]	<sup>1</sup> (Stocking Rep.)
PEC Lynchborough Road	
Passfield, Lipphook	Tel: + 44 (1428) 751617
Hampshire GU30 7SB	Fax: + 44 (1428) 751603

### Solid State Supplies Ltd. <sup>[Micrel]</sup> (Stocking Rep.) Unit 2, Eastlands Lane

Unit 2, Eastlands Lane	
Paddock Wood	Tel: + 44 (1892) 836836
Kent TN12 6BU	Fax: + 44 (1892) 837837

											П	ТТ	Т		П	П	Т		П	ТТ								П	
													-			++													++
										-		++	+			++			++			++		_					+
				_						_		++	_	++		$\left  \right $			$\square$			++		_		+	+		++
										-			+			++			++					+					
										-		++	+			++			$\square$			++							+
				_						_			_	++		$\left  \right $								_		+ $+$ $+$	+ +		++'
										-		+	-			++													++
$\left  + + + \right $		-++	++	++	++	++	+	+	+	_	++	++	+	$\left  \right $	$\left  \right $	$\left  \right $	++	+	$\left  \right $	++	++	++	+	_	$\left  \cdot \right $	+	$\left  \cdot \right $	++	++
			$\pm \pm$																										
				$\square$			$\square$		$\square$			$\square$	+					+										$ \top$	$+\top$
		+	+		++	++	+		+	+	+	+	+	++	+	++	+	++	+	+	+	++	+	_	$\vdash$	++	+	++	++
$\left  + + + \right $			++	++	++	++	+	+	+	+	+	++	+	++	+	++	++	+	++	+	++	++	++	_	$\left  \cdot \right $	+	+	++	++
										-		+	-			++													+++
				_	+					-	++	++	+		++	$\left  \right $	++		$\left  \right $			++		_					
										+	++	++	+			++			++			++		+					+
				_						-		++	-			++			++			++		-					++
										_		++	_		$\square$	$\left  \right $	++		$\square$			++		_					
												+	+			++			++					-					
		-+	++	++	++	++	+	+	+	+	++	++	+	++	++	++	++	+	++	++	++	++	++	+	+	++	$\left  \right $	++	++
			+	+	++	++	+		+		+	++	+	++	$\square$	$\left  \right $	++	+	$\left  \right $	++	+	+	+	_	$\left  \right $		$\left  \right $	++	++
			$\square$		+ +	$+\top$	$\square$		$\square$		$+ \top$	$+ \overline{+}$	-	$+ \overline{+}$	$+ \overline{+}$	$+\top$	$+\top$	+	$ \top$	$+\top$	$+ \overline{+}$	+	+				$\square$	$ \top$	$+ \Box$
		$\rightarrow$	++		++	++	+	+	+	+	++	++	+	++	++	++	++	++	++	++	++	+	++	+	++	++	+	++	++
												$\downarrow \downarrow$					$\downarrow \downarrow$		$ \uparrow $	$\downarrow \downarrow$									$\mp$
$\left  + + + \right $		+	+		++	++	+		+	-	+	++	+	++	++	++	++	++	$\left  \right $	++	++	++	+	_	$\left  \cdot \right $	+	$\left  \right $	++	++
													$\pm$																
			+	++	+	++	+	+]	+	+	+	+	+	++		$\left  \right ^{-}$	++	++		+	+	+	+	+	$\square$	+	++	++	++
		++	++		++	++	+	+	++	+	+	++	+	++	++	++	++	++	++	++	++	++	++	+	++	++	++	++	++
						$\parallel$						$\downarrow \downarrow$	$\mp$																
		++	++	++	++	++	+	+	+	+	++	++	+	++	++	++	++	++	$\left  \cdot \right $	++	++	++	++	+	$\left  \cdot \right $	++	++	++	++
			+		++	++	+		+		+	++	+	$\square$			$\square$		Ц					1	$\square$		$\square$		++
		++	++		++	++	+	+	+	+	++	++	+	$\left[ + \right]$	2-							FI			H				$\vdash$
														Π															
																									4	-			

	+ $+$ $+$ $+$ $+$ $+$ $+$	++++++++		+ + + + + + + + + + + + + + + + + + +	┟┼┼┼┼┼┼┼┼┼┼┼┼
	+ + + + + + + +	++++++++		+ + + + + + + + + + + + + + + + + + +	
	+ + + + + + + +	+++++++++		+ + + + + + + + + + + + + + + + + + +	
+ + + + +	+ $+$ $+$ $+$ $+$ $+$ $+$	+++++++++		+ + + + + + + + + + + + + + + + + + +	┟┼┼┼┼┼┼┼┼┼┼┼┼
+ + + + + -	+ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$	+++++++		+ + + + + + + + + + + + + + + + + + +	
+++++	+ + + + + + + +	+++++++++		+ + + + + + + + + + + + + + + + + + +	
+++++	+ + + + + + + +	+++++++++		+ + + + + + + + + + + + + + + + + + +	┟┼┼┼┼┼┼┼┼┼┼┼┼
+ + + + + +	+ + + + + + + +	+++++++++		+ + + + + + + + + + + + + + + + + + +	┟┼┼┼┼┼┼┼┼┼┼┼┼┼
	+ + + + + + + +			+ + + + + + + + + + + + + + + + + + +	┟┼┼┼┼┼┼┼┼┼┼┼┼
+++++	+ + + + + + + +	+++++++++		+ + + + + + + + + + + + + + + + + + +	┟┼┼┼┼┼┼┼┼┼┼┼┼┼
++++	+++++	+++++++	++++++		
<u>.</u>					