

a) Common Mode voltage gain: (single-ended)

$$A_{cm} = \frac{V_o}{V_{cm}} = \frac{V_{o2}}{V_{s1}} \Big|_{V_{s2}=V_{s1}} = -g_{m2} \tau_{D2} [1 + g_{m1} \tau_s - g_{m1} \tau_s] \frac{1}{\Delta}$$

$$\left| A_{cm} = -\frac{g_m \tau_D}{1 + 2g_m \tau_s} = -\frac{1}{2} \frac{\tau_D}{\tau_s \left(1 + \frac{1}{2g_m \tau_s}\right)} \right| \quad \frac{-g_m \tau_D}{2\tau_s g_m + 1}$$

b) Differential Mode voltage gain: (single-ended)

$$A_d = \frac{V_o}{V_d} = \frac{V_{o2}}{V_{s1}} \Big|_{V_{s2}=0} = g_{m1} \tau_s g_{m2} \tau_{D2} \frac{1}{\Delta}$$

$$\left| A_d \cong \frac{g_m \tau_s g_m \tau_D}{1 + 2g_m \tau_s} = \frac{1}{2} \frac{g_m \tau_D}{\left(1 + \frac{1}{2g_m \tau_s}\right)} \right|$$

c) Common Mode Rejection Ratio:

$$\left| CMRR = \frac{|A_d|}{|A_{cm}|} \cong g_m \tau_s \right|$$

Numerical Example

$$\tau_D = 39 \text{ k}\Omega$$

$$\tau_s = 18 \text{ k}\Omega$$

$$g_m = 4 \times 10^{-4} \frac{\text{A}}{\text{V}}$$

\Rightarrow

$$\left| \begin{array}{l} A_{cm} \cong -1.01 \\ A_d \cong 7.29 \\ CMRR \cong 7.2 \end{array} \right|$$

Conclusion: To improve both A_d and $CMRR$ we have to replace τ_D and τ_s by current sources! \rightarrow active Loads