

Solution for \bar{I}_D :

$$\left\| \begin{aligned} \bar{I}_{D1} = \bar{I}_{D2} &\approx \frac{1}{8k\bar{r}_s^2} \left[1 + 4k\bar{r}_s (V_{CM} + V_{SS} - V_t) \pm \sqrt{1 + 8k\bar{r}_s (V_{CM} + V_{SS} - V_t)} \right] \\ \text{where } k &= \frac{1}{2} \frac{W}{L} \mu C_{ox} \end{aligned} \right\|$$

physically not possible
since $V_{GS} < V_t$

$$\text{and } \left\| V_{DS1} = V_{DS2} \approx V_{DD} + V_{SS} - \bar{I}_D (\bar{r}_D + 2\bar{r}_s) \right\|$$

Numerical Example

$$V_{DD} = V_{SS} = 5V$$

$$\bar{r}_s = 18k\Omega$$

$$\bar{r}_D = 39k\Omega$$

$$V_t = 0.9V$$

$$k = 4 \times 10^{-4} \frac{A}{V^2}$$

$$V_{DSsat} \approx (V_{GS} - V_t)$$

$$\text{p.g. } \left| \begin{aligned} \mu_n &= 5 \times 10^{-2} \frac{m^2}{Vs} \\ C_{ox} &= 8 \times 10^{-4} \frac{F}{m^2} \end{aligned} \right| \quad \left| \frac{W}{L} = \frac{100\mu m}{5\mu m} = 20 \right|$$

Case A

$$V_{CM} = 0$$

$$\bar{I}_D \approx 100\mu A$$

$$V_{DS} \approx 4.3V$$

$$V_{DSsat} \approx 0.50V$$

$$g_m \approx 4 \times 10^{-4} \frac{A}{V}$$

Case B

$$V_{CM} = -1V$$

$$\bar{I}_D \approx 74\mu A$$

$$V_{DS} \approx 5.8V$$

$$V_{DSsat} \approx 0.43V$$

$$g_m \approx 3.4 \times 10^{-4} \frac{A}{V}$$

Case C

$$V_{CM} = 1V$$

$$\bar{I}_D \approx 131\mu A$$

$$V_{DS} \approx 2.5V$$

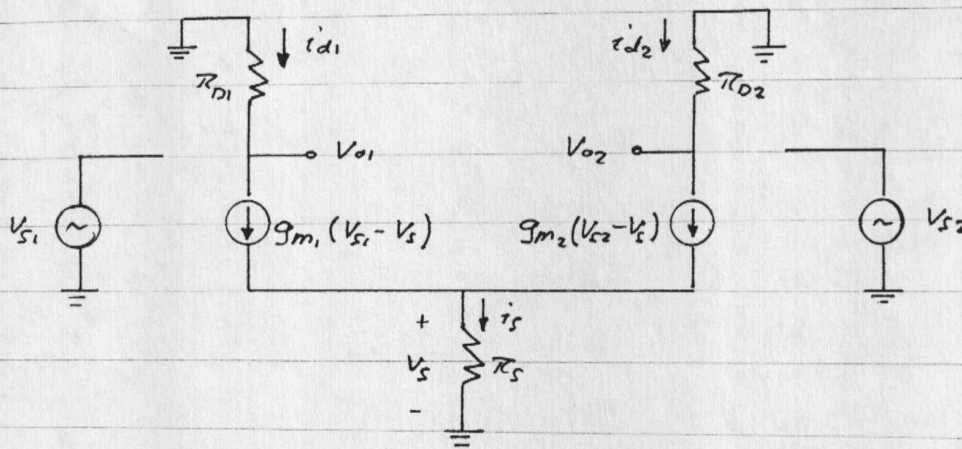
$$V_{DSsat} \approx 0.57V$$

$$g_m \approx 4.6 \times 10^{-4} \frac{A}{V}$$

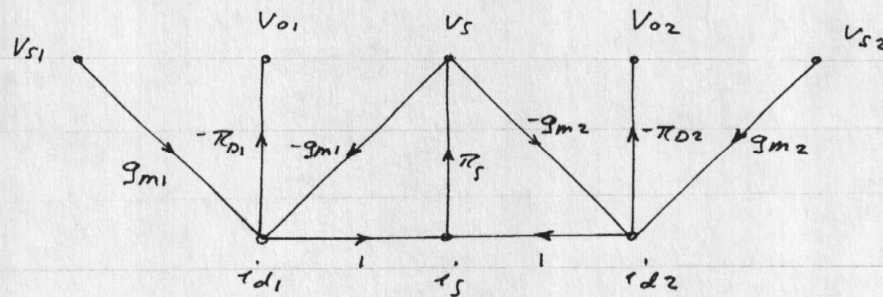
We note again that the common mode input voltage influences the operating point and thus the ac performance (g_m !) of the differential gain stage. To remedy this situation we can again apply a current source biasing scheme!

4.2.2 AC Considerations

linear equivalent circuit (y-parameter model)



SFG



$$\Delta = 1 + g_{m1} R_S + g_{m2} R_S$$

If transistors are perfectly matched we obtain

$$|\Delta = 1 + 2 g_m R_S|$$

$$\frac{V_{o1}}{V_{s1}} = -g_m R_D \left(\frac{1 + g_m R_S}{1 + 2 g_m R_S} \right)$$

$$V_{o1} = \frac{V_{s1} (-g_m R_D) - V_{s1} (g_m R_S g_m R_D)}{1 + g_m R_S + g_m R_S}$$