

Chapter 4

Transients

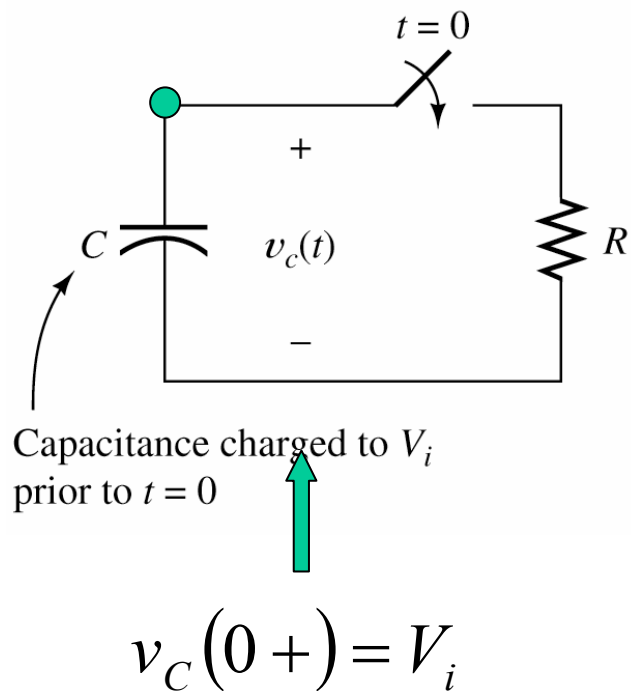
*The time-varying currents and voltages resulting from the sudden application of sources, usually due to switching, are called **transients**.*

Goal

- 1. First-order RC or RL Circuits.**
- 2. Concepts of Transient Response and Steady-State Response.**
- 3. Transient Response of First-Order Circuits to Time Constant.**
- 4. RLC Circuits in DC Steady-State Conditions.**
- 5. Second-Order Circuits.**
- 6. Step Response of a Second-Order System to its Natural Frequency and Damping Ratio.**

First-Order RC Circuits

Discharge of a Capacitance through a Resistance



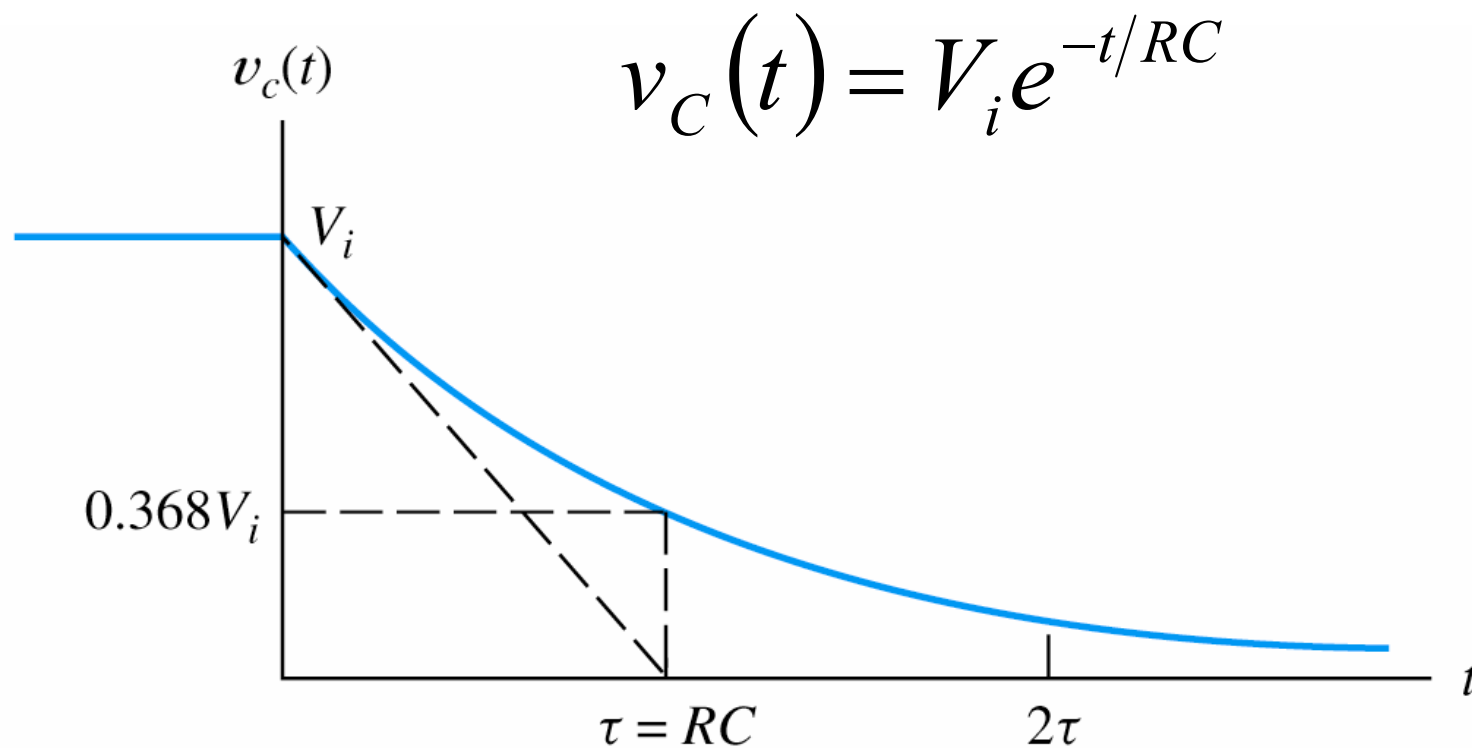
KCL at Node $C \frac{dv_C(t)}{dt} + \frac{v_C(t)}{R} = 0$

$$RC \frac{dv_C(t)}{dt} + v_C(t) = 0 \quad \Rightarrow \quad v_C(t) = Ke^{st}$$

$$RCKse^{st} + Ke^{st} = 0 \quad \Rightarrow \quad s = \frac{-1}{RC}$$

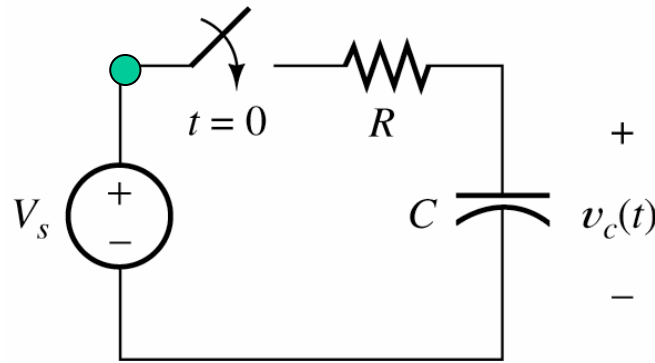
$$v_C(t) = Ke^{-t/RC}$$

$$v_C(t) = V_i e^{-t/RC}$$



The time interval $\tau = RC$ is called the time constant of the circuit
 In one time Constant, Voltage decays by factor $1/e$

Charging Capacitance from DC Source through a Resistance



$$\text{KCL at Node } C \frac{dv_C(t)}{dt} + \frac{v_C(t) - v_s}{R} = 0$$

$$RC \frac{dv_C(t)}{dt} + v_C(t) = v_s \quad \longrightarrow \quad v_C(t) = K_1 + K_2 e^{st}$$

$$\text{I.C. } v_C(0+) = v_C(0-) = 0$$

$$(1 + RCs)K_2 e^{st} + K_1 = v_s \quad \longrightarrow \quad s = \frac{-1}{RC} \quad \longrightarrow \quad K_1 = v_s$$

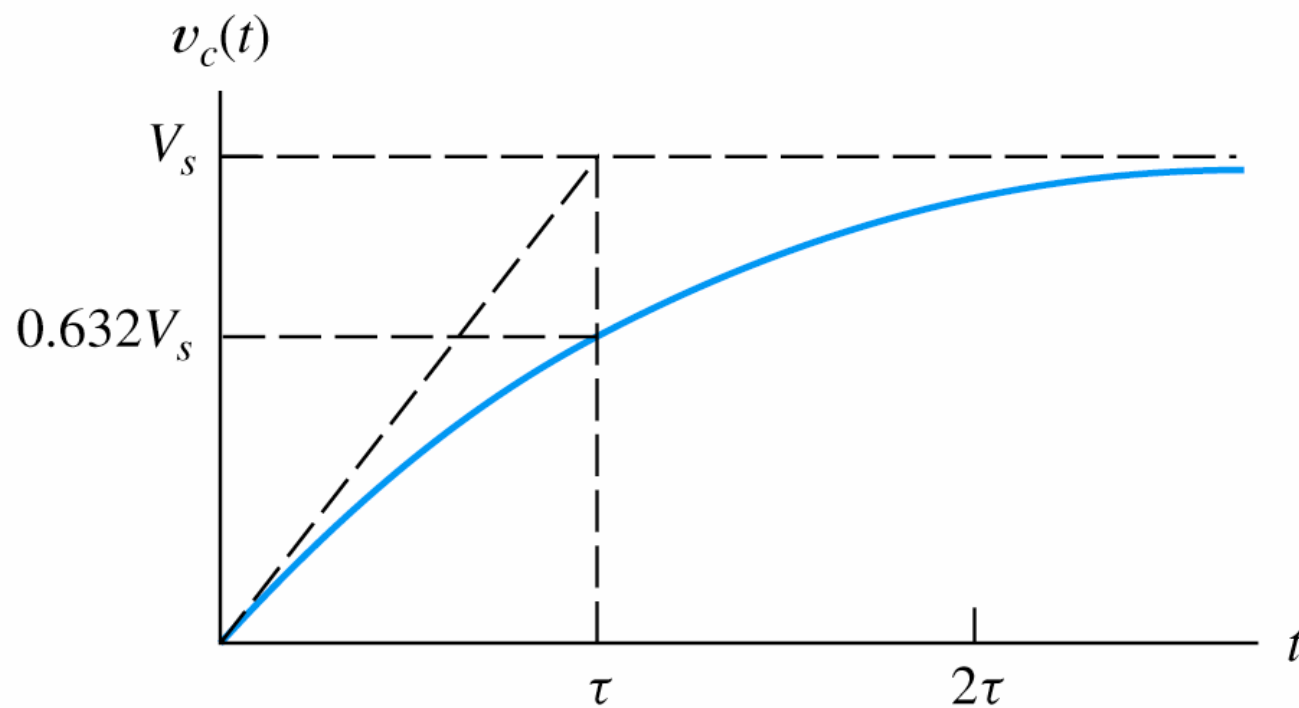
$$v_C(t) = v_s + K_2 e^{-t/RC} \quad \longrightarrow \quad K_2 = -v_s \quad \tau = RC$$

$$v_C(t) = v_s - v_s e^{-t/\tau}$$

v_s : Steady State Response (Forces Response)

$v_s e^{-t/\tau}$: Transient Response

$$v_C(t) = v_s - v_s e^{-t/\tau}$$



DC STEADY STATE

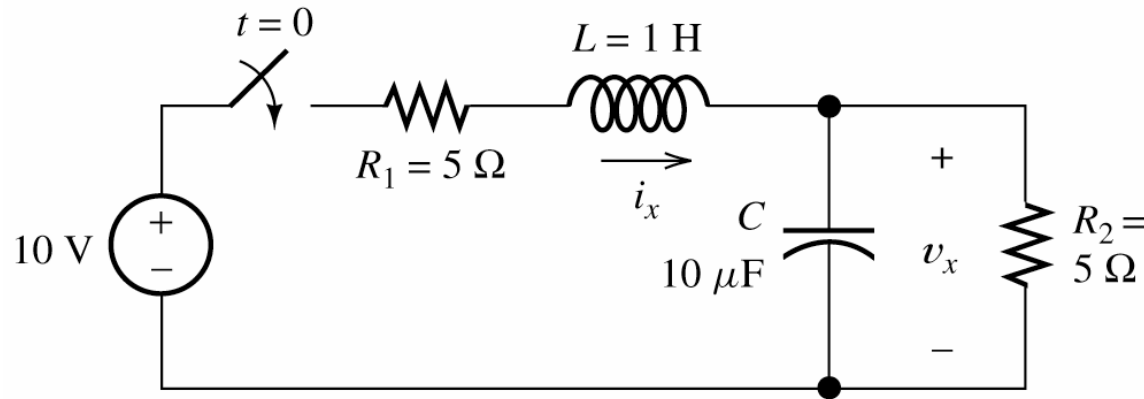
At Steady State of DC Circuit,

- Voltage is Constant $i_c(t) = C \frac{dv_c(t)}{dt} = 0$
- Current is Constant $v_L(t) = L \frac{di_L(t)}{dt} = 0$

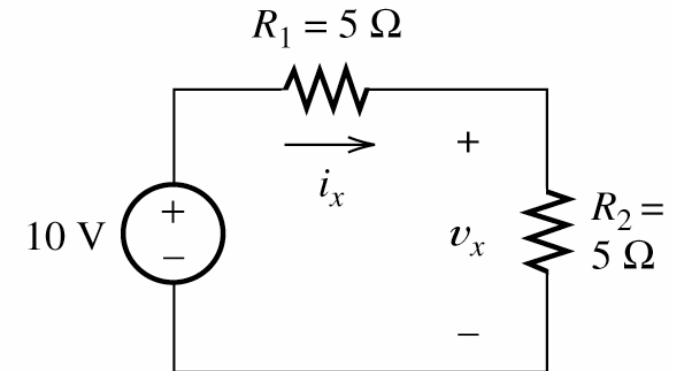
Steady State (Forced) Response for *RLC* circuits with DC sources are:

1. Replace Capacitances with open circuits.
2. Replace Inductances with short circuits.
3. Solve the remaining circuit.

Example of DC STEADY STATE



(a) Original circuit



(b) Equivalent circuit for steady state

If Time is Sufficiently Large, Steady State becomes.

$$i_x = \frac{v_s}{R_1 + R_2} = \frac{10}{5 + 5} = 1A$$

$$v_x = R_2 i_x = 5V$$

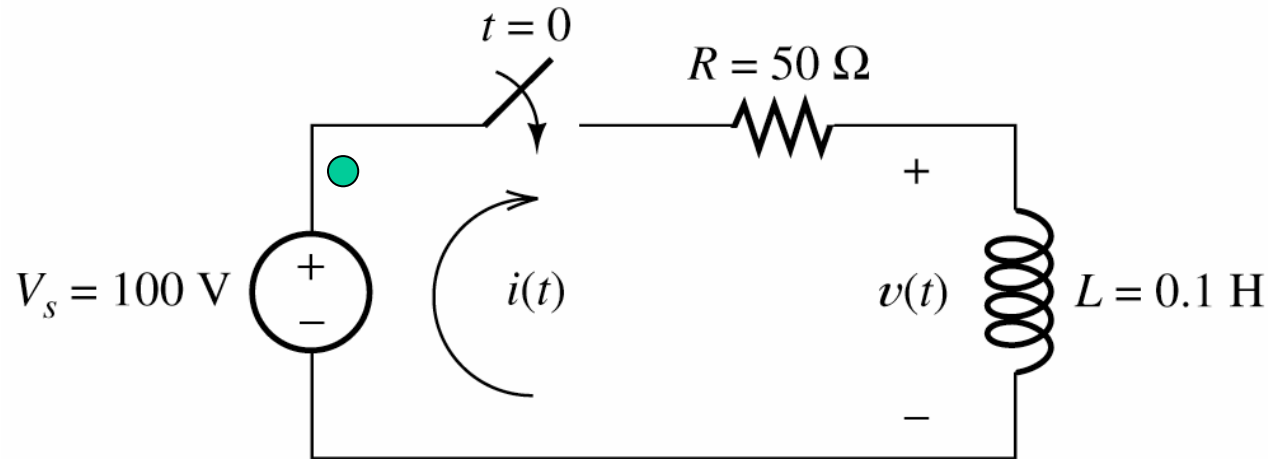
RL Circuits

To solve circuits with DC sources, Resistances, & One energy-storage element (Inductance or Capacitance) are:

1. Apply KCL & KVL to write the Circuit Equation.
2. If Integrals, Differentiate to Differential Equation.
3. Assume a Solution form $K_1 + K_2 e^{st}$.
4. Substitute Solution into Differential equation to determine K_1 and s
5. Use the initial conditions to determine the value of K_2 .
6. Write the final solution.

(Alternatively, we can determine K_1 *by solving the circuit in steady state*)

RL Transient Analysis (Series & Switch On)



Initial Condition

$$i(t) = 0 \quad t < 0$$

Step 1. Apply KCL & KVL to write the circuit equation (No Step 2)

$$Ri(t) + L \frac{di(t)}{dt} = v_s$$

Step 3. Assume a solution of the form $K_1 + K_2 e^{st}$.

$$i(t) = K_1 + K_2 e^{st}$$

Step 4. Substitute the solution into the differential equation

$$\underbrace{RK_1}_{=v_s} + \underbrace{(RK_2 + sLK_2)e^{st}}_{=Zero} = v_s$$

$$K_1 = \frac{v_s}{R} \quad s = \frac{-R}{L} \quad \Rightarrow \quad i(t) = v_s / R + K_2 e^{-tR/L}$$

Step 5. Use the initial conditions to determine the value of K_2 .

$$i(0+) = v_s / R + K_2 = 0 \quad \Rightarrow \quad i(t) = v_s / R (1 - e^{-tR/L})$$

$$\text{Time constant is } \tau = \frac{L}{R}$$

Step 6. Write the final solution.

$$\frac{v_s}{R} = \frac{100}{50} = 2 \quad \tau = \frac{L}{R} = \frac{0.1}{50} = 2ms \quad \Rightarrow \quad i(t) = 2(1 - e^{-t/\tau})$$

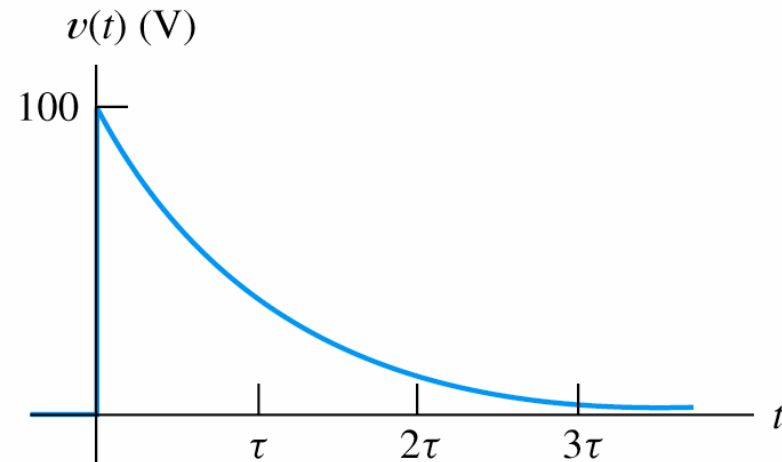
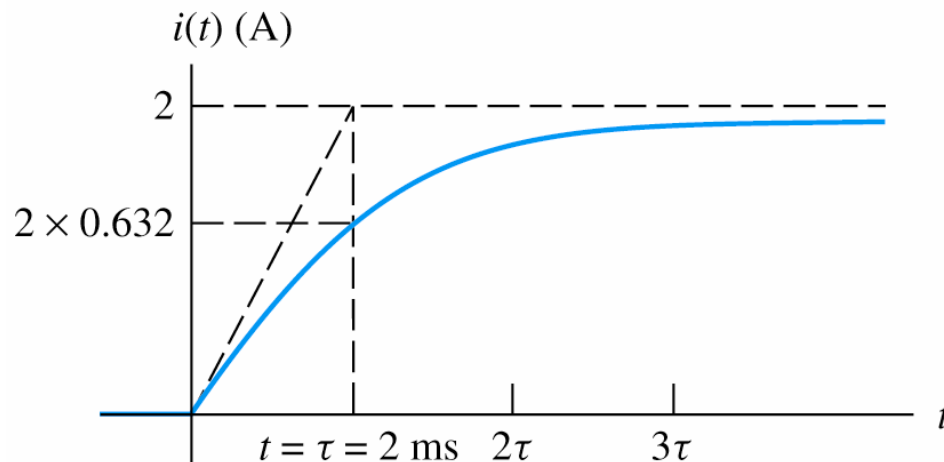
Using $v_L(t) = L \frac{di_L(t)}{dt}$

$$i(t) = v_s / R (1 - e^{-tR/L}) \quad \longrightarrow \quad v_L(t) = v_s e^{-tR/L}$$

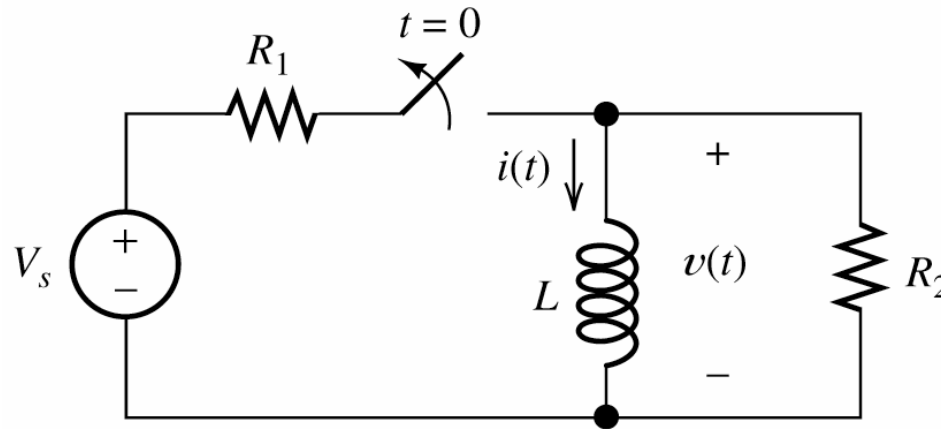
In given Circuit Condition, $R=100\Omega$, $L=0.1\text{H}$

$$i(t) = 2(1 - e^{-t/\tau})$$

$$v_L(t) = 100e^{-t/\tau}$$



RL Transient Analysis (Parallel & Switch Off)



Initial Condition

$$i(t) = \frac{V_s}{R_1} \quad \& \quad v(t) = 0 \quad t < 0$$

Before Switch Off, Current Circulates through R_1 , V_s & Inductor

After Switch Off, Current from V_s disappear

Current flows through inductor return to R_2

→ Voltage appears across R_2 & Inductor, causing to Current to decay

→ Steady-State Solution becomes Zero State

Step 1. Apply KCL & KVL \rightarrow Circuit equation (No Step 2)

$$Ri(t) + L \frac{di(t)}{dt} = v_s$$

Step 3&4. Assume Solution form $K_1 + K_2 e^{st}$ $i(t) = K_1 + K_2 e^{st}$

Steady State is Zero State : $K_1 = 0$ $i(t) = K_2 e^{st}$

$$i(t) = K_2 e^{-t/\tau} \quad \tau = \frac{L}{R_2}$$

Step 5. Use the initial conditions to determine the value of K_2 .

$$i(0+) = v_s / R_1 = K_2 \quad \rightarrow$$

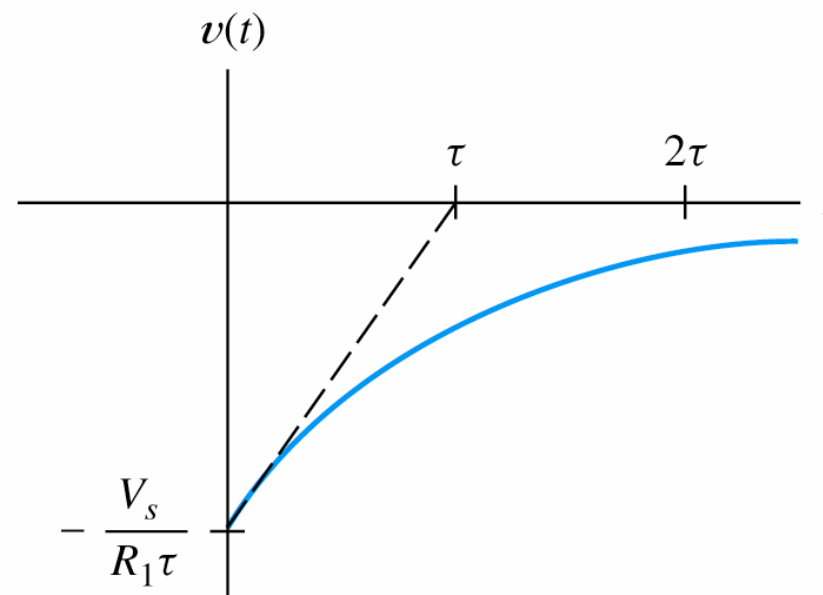
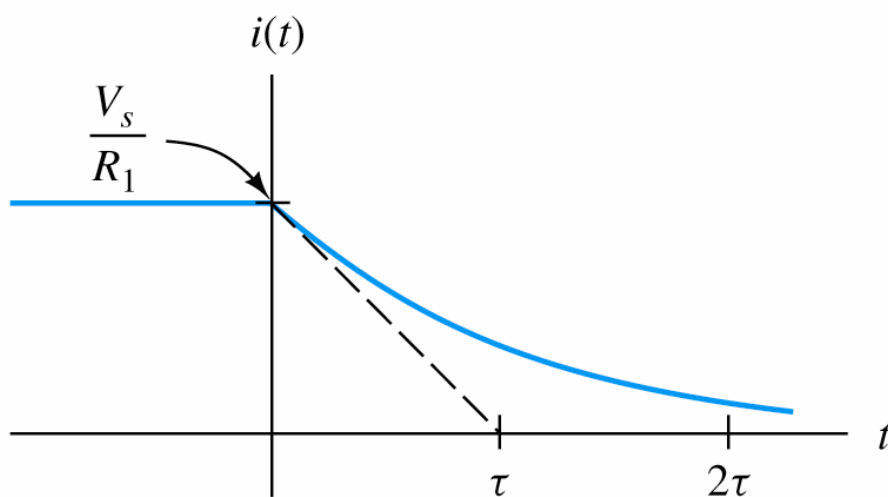
$$i(t) = v_s / R_1 e^{-t/\tau}$$

$$v(t) = 0 \quad t < 0$$

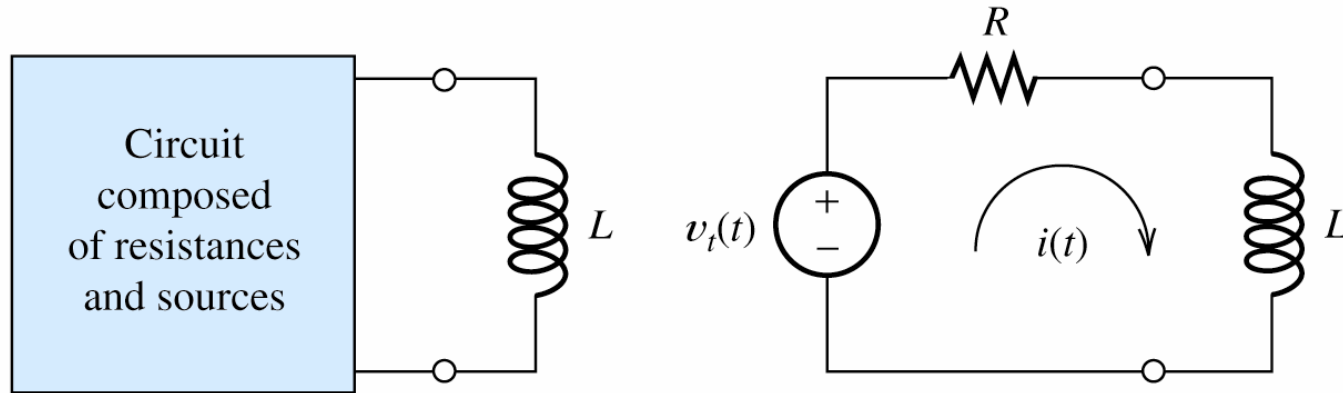
$$v_L(t) = L \frac{di_L(t)}{dt} \quad \rightarrow \quad v(t) = -\frac{Lv_s}{R_1 \tau} e^{-t/\tau} \quad t > 0$$

$$i(t) = v_s / R_1 e^{-t/\tau} \quad v_L(t) = L \frac{di_L(t)}{dt} \quad \Rightarrow \quad v(t) = 0 \quad t < 0$$

$$v(t) = -\frac{Lv_s}{R_1\tau} e^{-t/\tau} \quad t > 0$$



RC & RL Circuits with General Sources



When Inductor is Linked with General Source

→ Using Thévenin Theorem → Voltage Source + Resistor

Note : *Voltage Source & Current are varying with time*

KVL

$$L \frac{di_L(t)}{dt} + Ri(t) = v_t(t) \quad \longrightarrow \quad \frac{L}{R} \frac{di_L(t)}{dt} + i(t) = \frac{v_t(t)}{R}$$

Generally $\tau \frac{dx(t)}{dt} + x(t) = f(t)$ τ : Time Constant
 $f(t)$: Forcing function

Solution of 1st Order Differential Equation

$$y' + p(t)y = r(t) \quad \longrightarrow \quad y = \underbrace{e^{-\int p(t)dt} \int e^{\int p(t)dt} r(t)dt}_{\text{Appendix}} + C \underbrace{e^{-\int p(t)dt}}_{\text{Appendix}}$$

The particular solution (called the forced response) is any expression that satisfies the equation.

The complementary solution (called the natural response) is obtained by solving the homogeneous equation.

$$\tau \frac{dx(t)}{dt} + x(t) = f(t) \quad \longrightarrow \quad x(t) = x_p(t) + x_c(t)$$

$$\frac{dx(t)}{dt} + \frac{1}{\tau} x(t) = \frac{1}{\tau} f(t) \quad \longrightarrow \quad p(t) = \frac{1}{\tau} \quad \& \quad r(t) = \frac{1}{\tau} f(t)$$

$$y = e^{-\int \frac{1}{\tau} dt} \int e^{\int \frac{1}{\tau} dt} \frac{1}{\tau} f(t) dt + C e^{-\int \frac{1}{\tau} dt} = e^{-\frac{t}{\tau}} \int e^{\frac{t}{\tau}} \frac{1}{\tau} f(t) dt + C e^{-\frac{t}{\tau}}$$

$$\frac{dx_c(t)}{dt} + \frac{1}{\tau} x_c(t) = 0 \quad \frac{dx_c(t)/dt}{x_c(t)} = -\frac{1}{\tau} \quad \ln x_c(t) = -\frac{t}{\tau} + c \quad \uparrow \quad x_c(t) = K e^{-\frac{t}{\tau}}$$

Step-by-Step Solution

Circuits with a resistance, a source, and an inductance (or a capacitance)

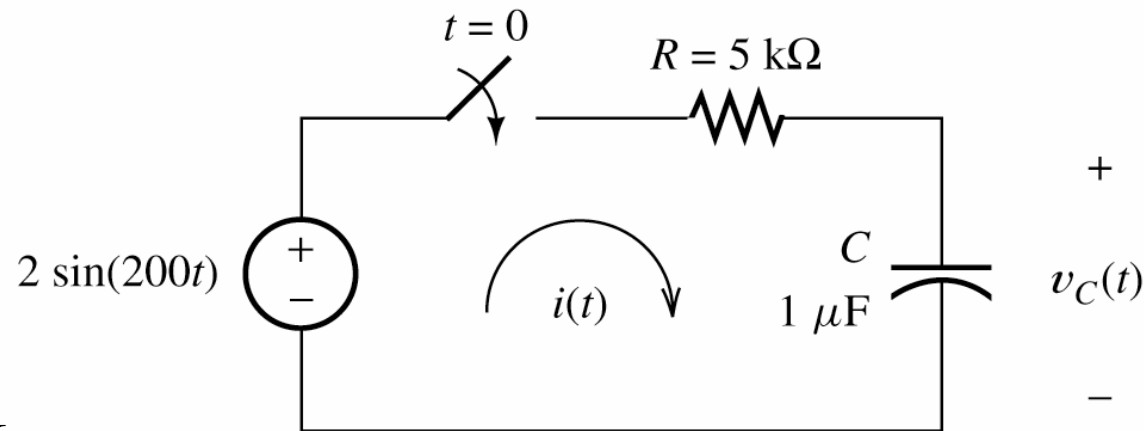
1. Write *Circuit Equation* as *1st Order* Differential Equation.

2. Find a *Particular Solution*.

The details of this step depend on the form of the forcing function.

3. Obtain the *Complete Solution* by adding the particular solution to the *Complementary Solution*

4. Use *Initial Conditions* to find the value of K .



Use KVL

$$Ri(t) + \frac{1}{C} \int_0^t i(t) dt + v_C(0) - 2 \sin(200t) = 0 \quad v_C(0) = 1 \text{ V}$$

Step 1. Write Circuit Equation as 1st-Order Differential Equation.

$$R \frac{di(t)}{dt} + \frac{1}{C} i(t) = 400 \cos(200t) \quad \longrightarrow \quad RC \frac{di(t)}{dt} + i(t) = 400C \cos(200t)$$

Step 2. Find a particular solution.

Using General Solution or
Guessing from Math.

$$\longrightarrow i_p(t) = A \cos(200t) + B \sin(200t)$$

$$5 \times 10^{-3} \frac{di(t)}{dt} + i(t) = 400 \times 10^{-6} \cos(200t) \quad \longrightarrow \quad i_p(t) = 200 \cos(200t) + 200 \sin(200t) \mu A$$

$$A = B = 200 \mu A$$

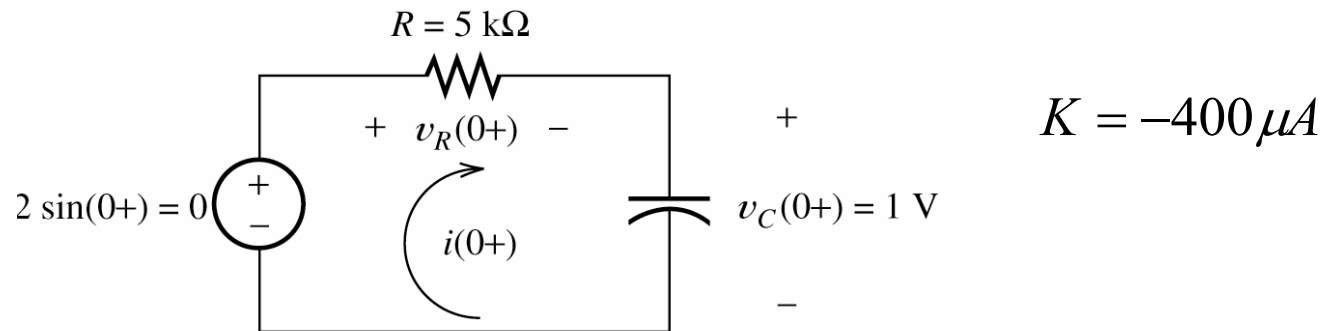
Step 3. Obtain the Complete Solution

$$RC \frac{di(t)}{dt} + i(t) = 0 \quad \longrightarrow \quad i_c(t) = Ke^{-\frac{t}{RC}} = Ke^{-\frac{t}{\tau}}$$

$$i(t) = 200 \cos(200t) + 200 \sin(200t) \mu A + Ke^{-\frac{t}{RC}}$$

Step 4. Use initial conditions to find the value of K .

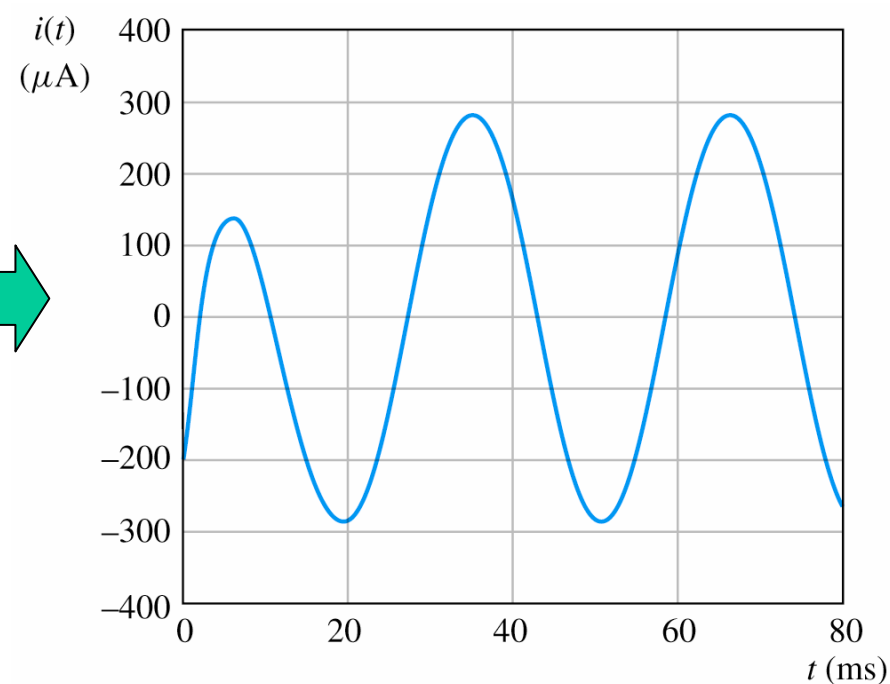
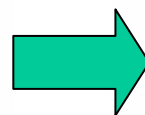
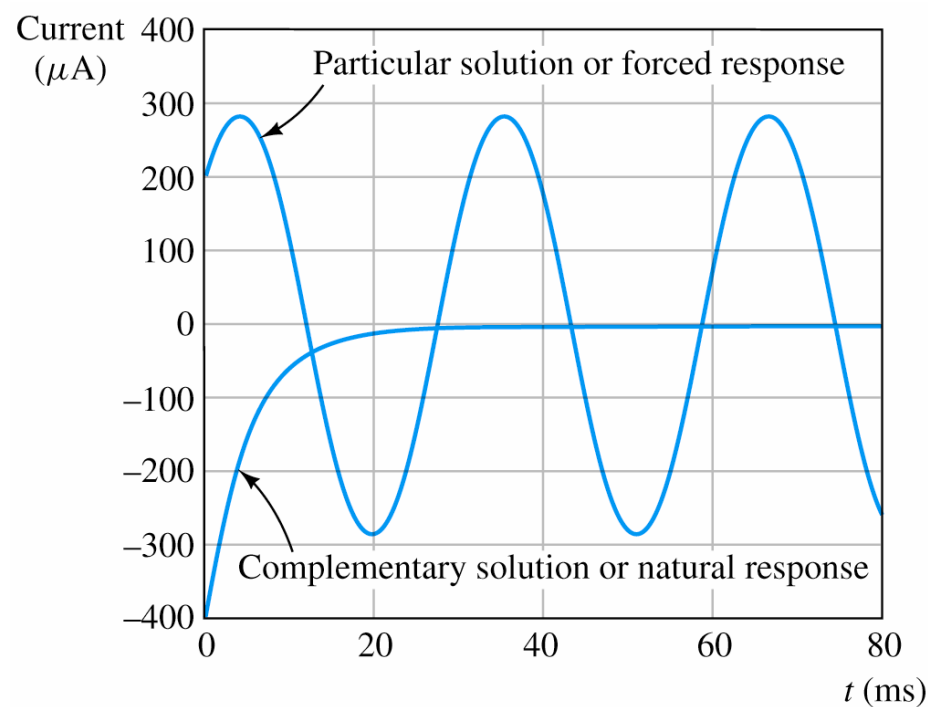
$$i(0+) = \frac{v_R(0+)}{R} = \frac{-1}{5000} = -200 \mu A = (200 + K) \mu A$$



$$i(t) = 200 \cos(200t) + 200 \sin(200t) \mu A - 400 e^{-\frac{t}{RC}} \mu A$$

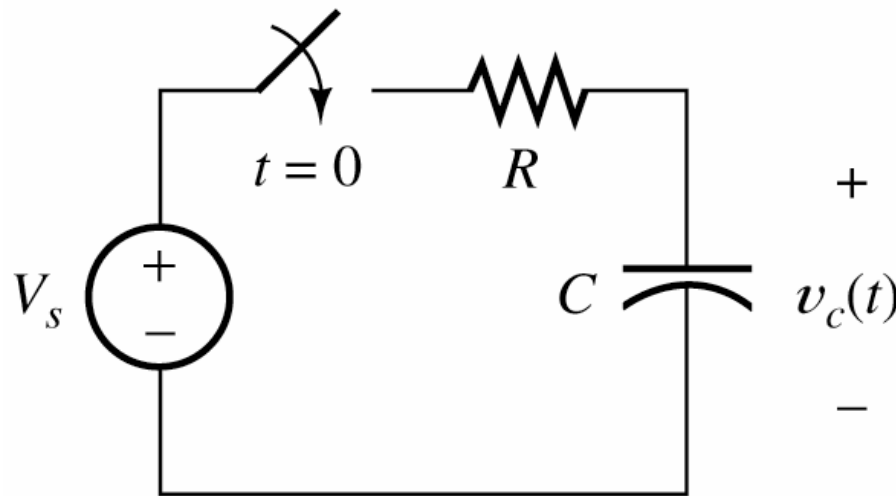
$$\tau = RC = 25 ms$$

$$i(t) = 200 \cos(200t) + 200 \sin(200t) \mu A - 400 e^{-\frac{t}{RC}} \mu A$$



Summary of 1st Order Diff. Equation

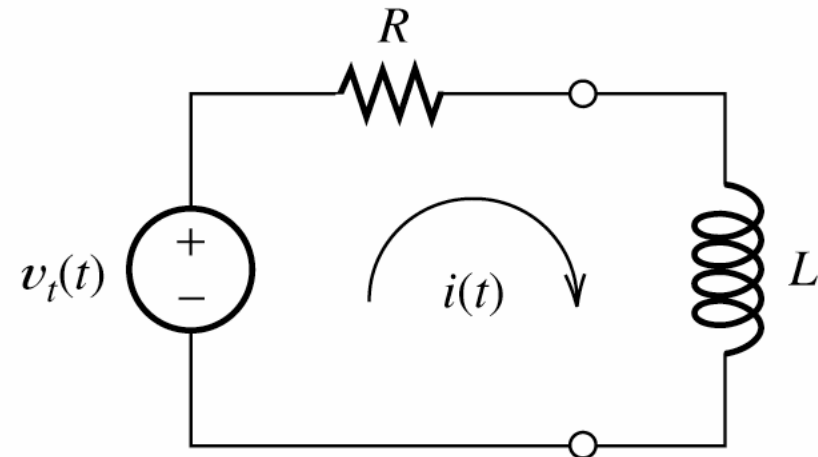
$$i(t) = e^{-\frac{t}{\tau}} \int e^{\frac{t}{\tau}} \frac{1}{\tau} f(t) dt + C e^{-\frac{t}{\tau}}$$



Constant Voltage Source (DC)

$$i(t) = e^{-\frac{t}{\tau}} \int e^{\frac{t}{\tau}} \frac{1}{\tau} K dt + C e^{-\frac{t}{\tau}}$$

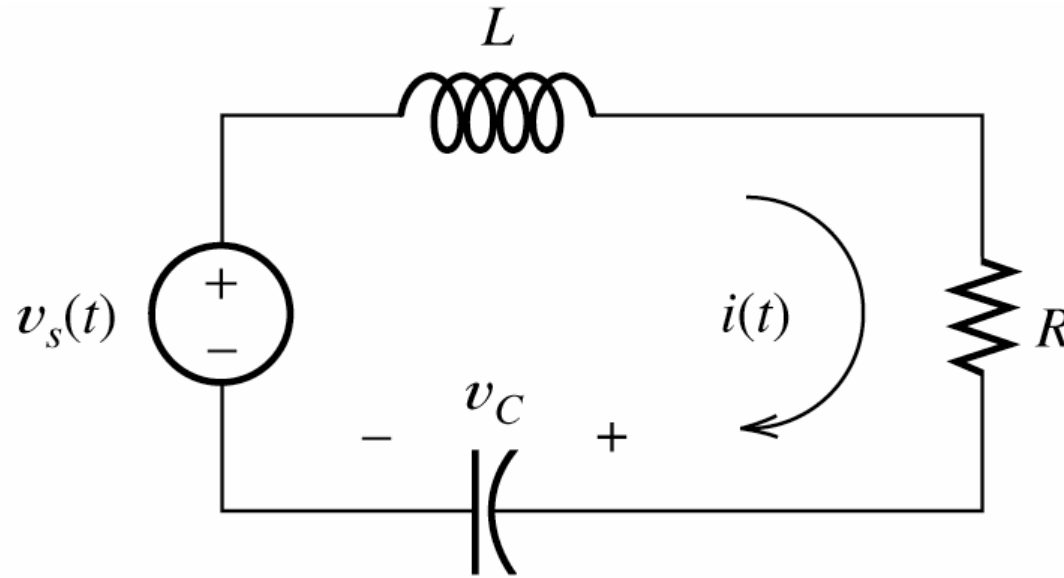
$$= K_1 + K_2 e^{st}$$



General Voltage Source

$$i(t) = e^{-\frac{t}{\tau}} \int e^{\frac{t}{\tau}} \frac{1}{\tau} f(t) dt + C e^{-\frac{t}{\tau}}$$

Second-Order Circuits



Using KVL

$$L \frac{di(t)}{dt} + Ri(t) + \frac{1}{C} \int_0^t i(t) dt + v_C(0) = v_s(t)$$

Taking Derivative & Divide by L

$$\frac{d^2 i(t)}{dt^2} + \frac{R}{L} \frac{di(t)}{dt} + \frac{1}{LC} i(t) = \frac{1}{L} \frac{dv_s(t)}{dt}$$

$$\alpha = \frac{R}{2L} \quad : \text{Damping Coefficient}$$

$$\omega_0 = \frac{1}{\sqrt{LC}} \quad : \text{Undamped Resonant Frequency}$$

$$f(t) = \frac{1}{L} \frac{dv_s(t)}{dt} \quad : \text{Forcing function}$$

$$\frac{d^2 i(t)}{dt^2} + 2\alpha \frac{di(t)}{dt} + \omega_0^2 i(t) = f(t)$$

➡ Linear 2nd Order Differential Equation

Here We know that $x(t) = x_p(t) + x_c(t)$

$$x_p(t) : \frac{d^2 x_p(t)}{dt^2} + 2\alpha \frac{dx_p(t)}{dt} + \omega_0^2 x_p(t) = f(t) \quad : \text{Particular Solution}$$

$$x_c(t) : \frac{d^2 x_c(t)}{dt^2} + 2\alpha \frac{dx_c(t)}{dt} + \omega_0^2 x_c(t) = 0 \quad : \text{Complementary Solution}$$

$$\boxed{x_p(t)} : \text{Particular Solution} : \frac{d^2 x_p(t)}{dt^2} + 2\alpha \frac{dx_p(t)}{dt} + \omega_0^2 x_p(t) = f(t)$$

In Electric Circuit, forcing function is Primarily DC & Sinusoidal Sources

DC Source : Steady State Solution

Can be obtained by Replacing Inductor to Short Circuit & Capacitor to Open Circuit

Sinusoidal Source : Complex Number Analysis (Chapter 5)

$$\boxed{x_c(t)} : \text{Complementary Solution} : \frac{d^2 x_c(t)}{dt^2} + 2\alpha \frac{dx_c(t)}{dt} + \omega_0^2 x_c(t) = 0$$

$$\text{Let } x_c(t) = Ke^{st} \longrightarrow (s^2 + 2\alpha s + \omega_0^2)Ke^{st} = 0$$

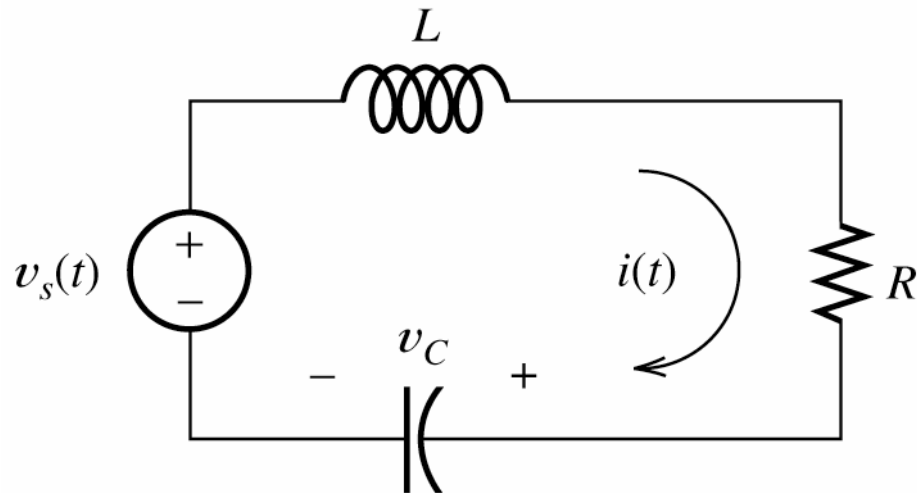
$$\text{Generally } s^2 + 2\alpha s + \omega_0^2 = 0 : \text{Characteristic Equation}$$

$$\text{Two Solutions : } s_1 = -\alpha + \sqrt{\alpha^2 - \omega_0^2}$$

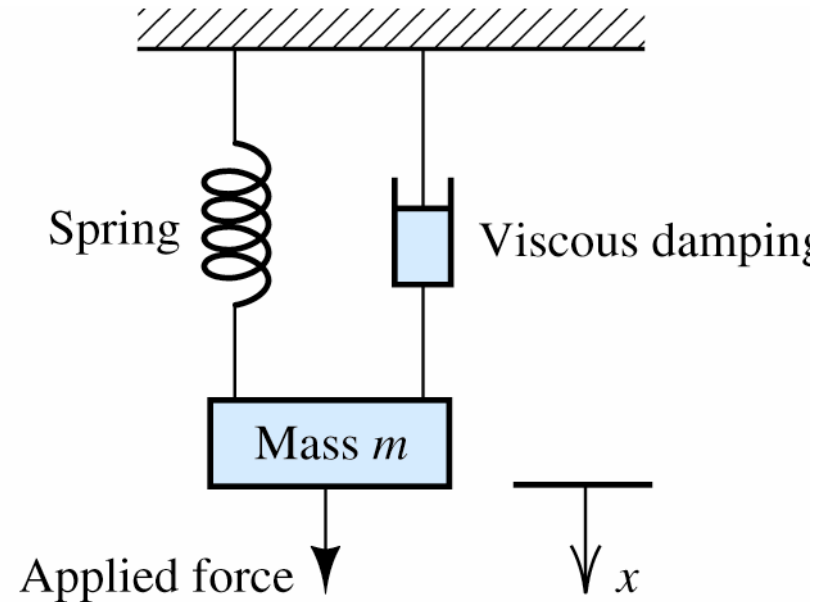
$$s_2 = -\alpha - \sqrt{\alpha^2 - \omega_0^2}$$

$$\zeta = \frac{\alpha}{\omega_0} : \text{Damping Ratio}$$

2nd Order Circuit Analogy



(a) Electrical circuit



(b) Mechanical analog

$$\frac{d^2 i(t)}{dt^2} + \frac{R}{L} \frac{di(t)}{dt} + \frac{1}{LC} i(t) = \frac{1}{L} \frac{dv_s(t)}{dt}$$

$$\frac{d^2 x(t)}{dt^2} + \frac{C}{m} \frac{dx(t)}{dt} + \frac{k}{m} x(t) = \frac{1}{m} f(t)$$

Solution Case of 2nd Order Equation

1. Overdamped case : $\zeta > 1$ or $\alpha > \omega_0$: Real & Distinct Two Roots

$$x_c(t) = K_1 e^{s_1 t} + K_2 e^{s_2 t}$$

2. Critically damped case : $\zeta = 1$ $\alpha = \omega_0$: Real & Equal Roots.

$$x_c(t) = K_1 e^{s_1 t} + K_2 t e^{s_1 t}$$

3. Underdamped case : $\zeta < 1$ or $\alpha < \omega_0$: Complex Roots

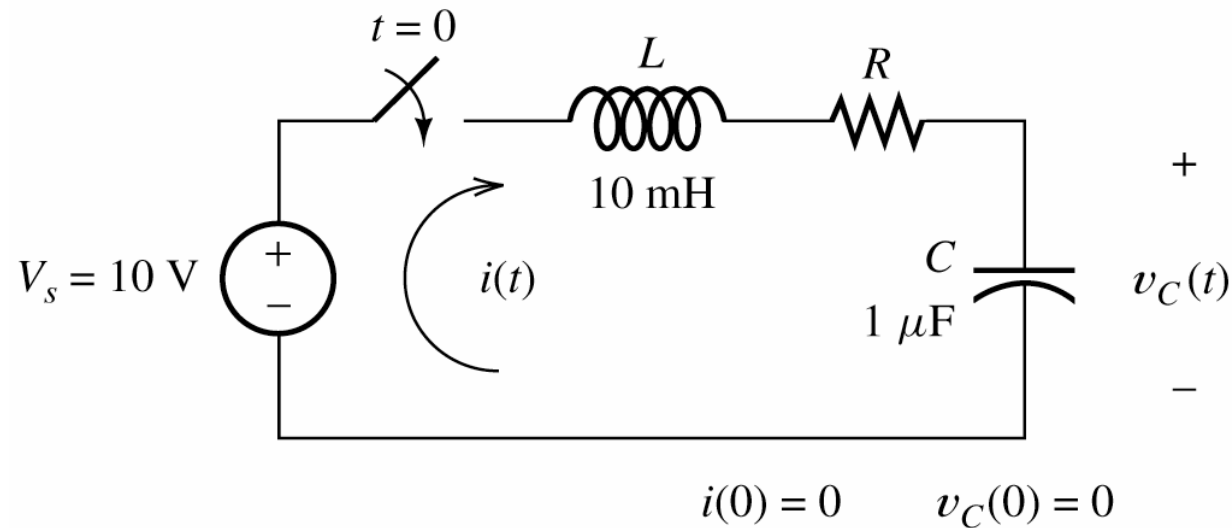
$$s_1 = -\alpha + j\omega_n \text{ \& } s_2 = -\alpha - j\omega_n$$

Natural frequency is given by $\omega_n = \sqrt{\omega_0^2 - \alpha^2}$

$$x_c(t) = K_1 e^{-\alpha t} \cos(\omega_n t) + K_2 e^{-\alpha t} \sin(\omega_n t)$$

In electrical engineering, we use j rather than i to stand for square root of -1, because of i for current.

Analysis of 2nd Order Circuit with DC Source

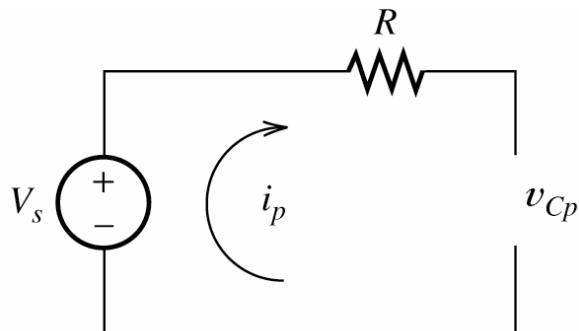


$$\text{KVL : } L \frac{di(t)}{dt} + Ri(t) + v_C(t) = V_s \quad \leftarrow \quad i(t) = C \frac{dv_C(t)}{dt}$$

$$LC \frac{d^2 v_C(t)}{dt^2} + RC \frac{dv_C(t)}{dt} + v_C(t) = V_s \quad \Rightarrow \quad \frac{d^2 v_C(t)}{dt^2} + \frac{R}{L} \frac{dv_C(t)}{dt} + \frac{1}{LC} v_C(t) = \frac{V_s}{LC}$$

$$\frac{d^2 v_C(t)}{dt^2} + 2\alpha \frac{dv_C(t)}{dt} + \omega_o^2 v_C(t) = \frac{V_s}{LC} \quad \begin{aligned} \alpha &= \frac{R}{2L} \\ \omega_o &= \frac{1}{\sqrt{LC}} \end{aligned}$$

Particular Solution



Set Inductor as Short Circuit
Capacitor as Open Circuit

$$\Rightarrow v_{cp}(t) = V_s$$

Complementary Solution

$$\omega_0 = \frac{1}{\sqrt{LC}} = 10^4$$

$$R=300\Omega \quad \alpha = 1.5 \times 10^4 \quad \& \quad \zeta = 1.5 \quad s_1 = -2.618 \times 10^4 \quad s_2 = -0.382 \times 10^4$$

$$v_c(t) = 10 + 1.708e^{s_1 t} - 11.708e^{s_2 t}$$

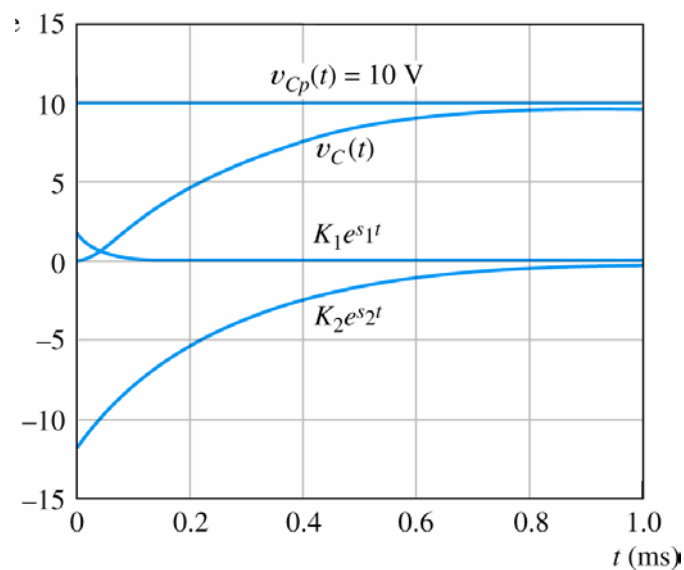
$$R=200\Omega \quad \alpha = 10^4 \quad \& \quad \zeta = 1 \quad s_1 = s_2 = -10^4$$

$$v_c(t) = 10 - 10e^{s_1 t} - 10^5 t e^{s_2 t}$$

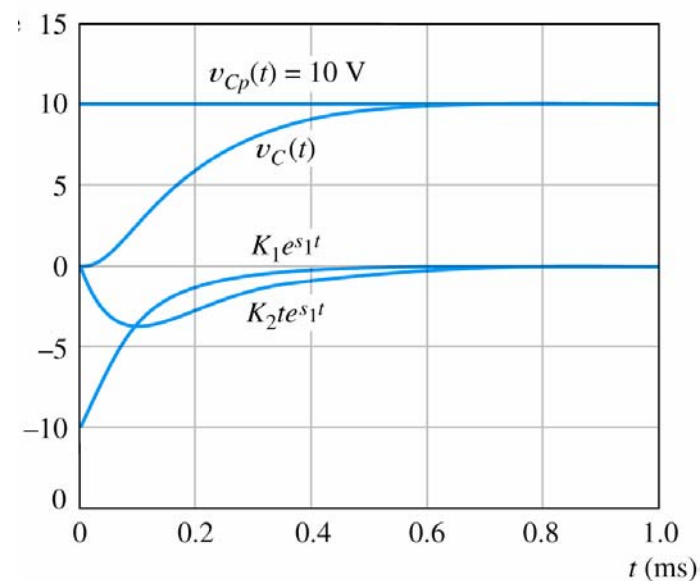
$$R=100\Omega \quad \alpha = 0.5 \times 10^4 \quad \& \quad \zeta = 0.5 \quad \omega_n = 8660$$

$$v_c(t) = 10 - 10e^{-\alpha t} \cos(\omega_n t) - 5.774e^{-\alpha t} \sin(\omega_n t)$$

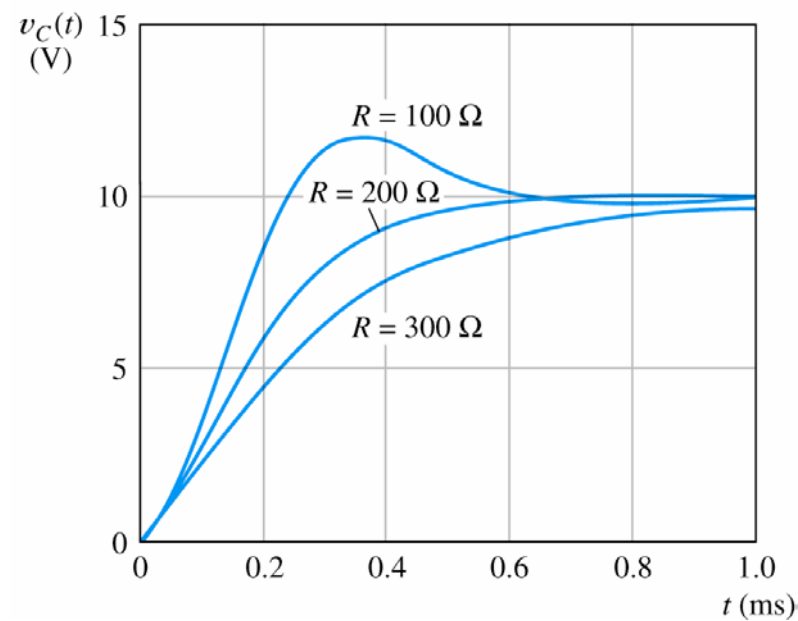
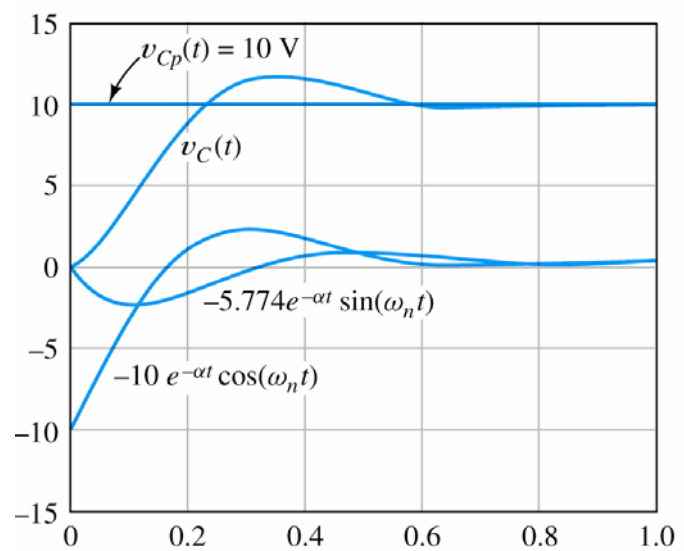
$R=300\Omega$



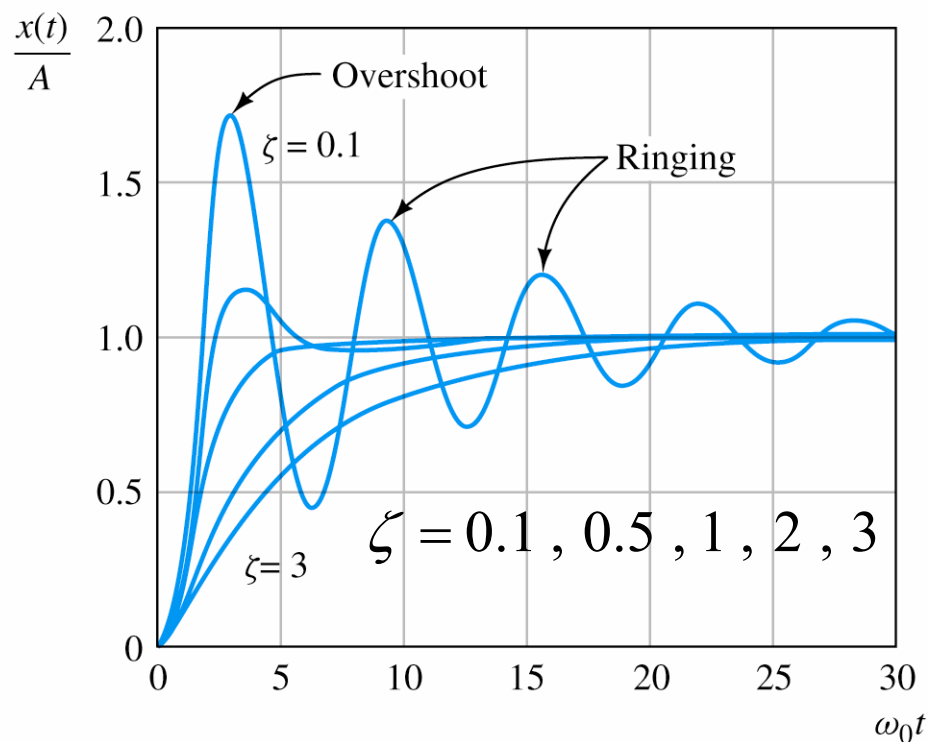
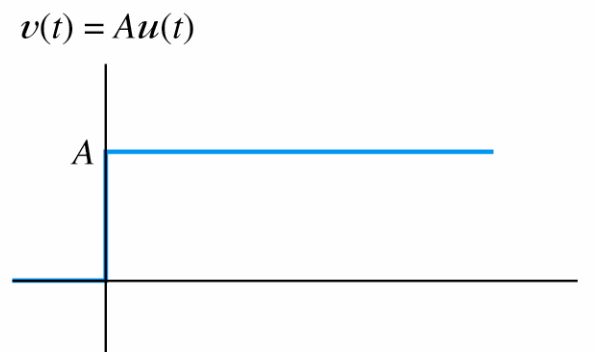
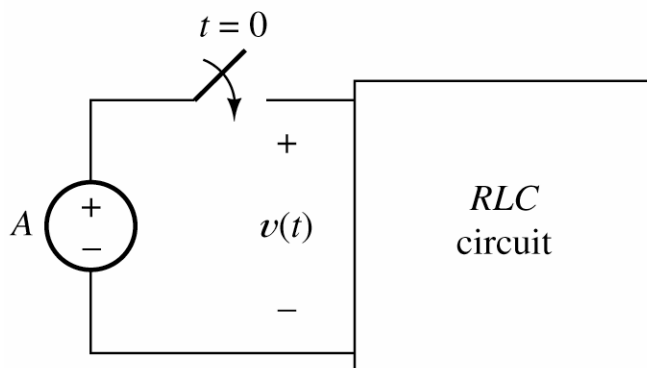
$R=200\Omega$



$R=100\Omega$

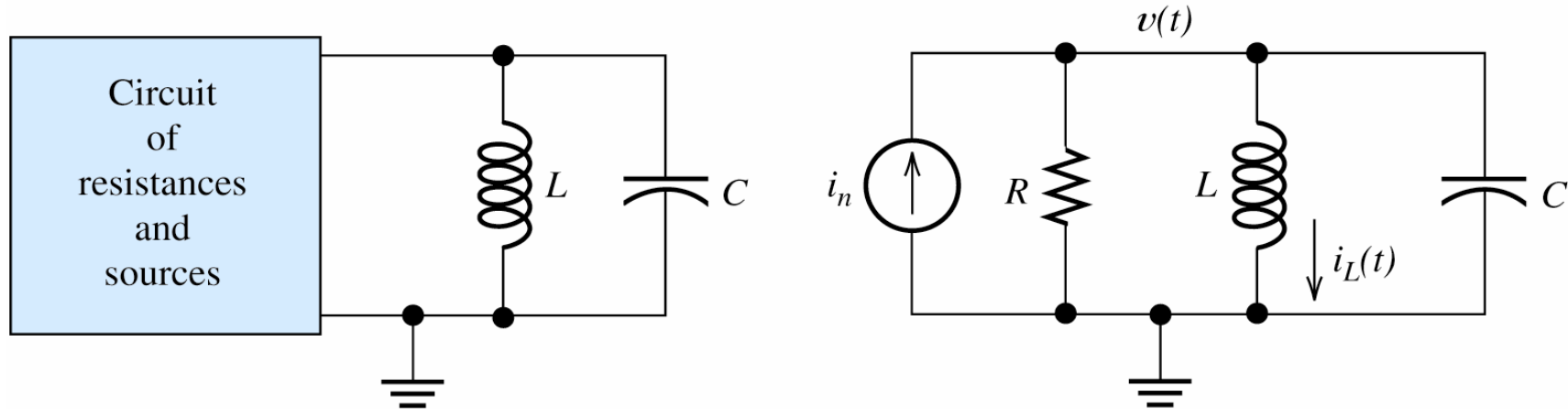


General RLC Circuit with DC Source



To avoid Overshoot,
Design Damping Ratio to 1

RLC Circuit with Parallel L & C



Using KCL

$$C \frac{dv(t)}{dt} + \frac{1}{R} v(t) + \frac{1}{L} \int_0^t v(t) dt + i_L(0) = i_n(t)$$

Taking Derivative & Divide by C

$$\frac{d^2 v(t)}{dt^2} + \frac{1}{RC} \frac{dv(t)}{dt} + \frac{1}{LC} v(t) = \frac{1}{C} \frac{di_n(t)}{dt}$$

$$\alpha = \frac{1}{RC} \quad : \text{Damping Coefficient}$$

$$\omega_0 = \frac{1}{\sqrt{LC}} \quad : \text{Undamped Resonant Frequency}$$

$$f(t) = \frac{1}{C} \frac{di_n(t)}{dt} \quad : \text{Forcing function}$$

$$\frac{d^2 v(t)}{dt^2} + 2\alpha \frac{dv(t)}{dt} + \omega_0^2 v(t) = f(t)$$

➡ Linear 2nd Order Differential Equation

$$x(t) = x_p(t) + x_c(t)$$

All treatments are same as Serial !